



HYPERSONIC RESEARCH ENGINE/AEROTHERMODYNAMIC INTEGRATION MODEL - EXPERIMENTAL RESULTS -- VOLUME IV: MACH 5 COMPONENT INTEGRATION AND PERFORMANCE

LANGLEY RESEARCH CENTER HAMPTON, VA

**APR 76** 



NASA TECHNICAL

## NASA TM X- 72824

HYPERSONIC RESEARCH ENGINE/AEROTHERMODYNAMIC

INTEGRATION MODEL - EXPERIMENTAL RESULTS

Volume IV - Mach 5 Component Integration and Performance

by

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(Contract No. NAS1-6666)

April 1976

(NASA-TM-X-72824) HYPERSONIC RESEARCH N76-21209 ENGINE/AEROTHERMODYNAMIC INTEGRATION MODEL, EXPERIMENTAL RESULTS. VOLUME 4: MACH 5 COMPONENT INTEGRATION AND PERFORMANCE (NASA) Unclas 526 p HC \$13.00 CSCL 21E G3/07 25232

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INFORMATION SERVICE
SPRINGFIELD, VA 22161



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1. Report No. NASA TM X-72824	2. Government Access	ion No.	3. Rec	pient's Catalog No.	
4. Title and Subtitle HYPERSONIC RESEARCH ENGI	NF/AFROTHERMODYNAI	MIC		ort Date ^il 1976	
INTEGRATION MODEL - EXPE Volume IV - Mach 5 Compo	RIMENTAL RESULTS			orming Organization Cod	le
7. Author(s) Earl H. Andrews, Jr.; Ern Engineering Staff, AiRe	est A. Mackley; a	nd	8 Perf	orming Organization Rep	ert No.
Performing Organization Name and Addr			10. Wor 505	k Unit No. 1-05-41-03	
NASA Langley Research Ce Hampton, VA 23665	enter		ı	tract or Grant No.	
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12. Sponsoring Agency Name and Address				hnical Memoran	
National Aeronautics and Washington, D.C. 20546	Space Administra	tion	<u> </u>	nsoring Agency Code	
15. Supplementary Notes					
Special technical inform	ation release, no	t planned	for formal N	ASA Publicatio	n
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16. Abstract					
The NASA Hypersonic for the purpose of advan hypersonic flight. A la development program was gram was culminated in 1 87 in. long) HRE concept in the NASA Lewis Resear at Mach numbers of 5, 6, results have been previo analysis results of the is included in the four or different interpretat computer program results Program results are cont subtitles:  Volume I - Mach 6 C Volume II - Mach 6 Volume III - Mach 7	cing the technologinge component (in encompassed by the 974 with the tests, designated the Ach Center, Plum Brand 7. AIM tests usly documented. AIM experimental ereports to enable ion of the AIM data for Mach 5 componained in three additional encomponent Integrate Performance	gy of air let, combe project of a function o	breathing probustor, and note. The component of the component in the control of t	pulsion for zzle) and structent development in. diameter cogration Model c Tunnel Facilities and and computer programough informatind/or additionationance tes	t pro- owl and (AIM), ity alysis ram ion al presents
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17. Key Words (Suggested by Author(s))		18. Distribut	ion Statement		
<u>Propulsion</u> Scramjets					
Engine Performance	•		Unclassified	- Unlimited	
Hypersonic Propulsion Hydrogen Fuel					
19. Security Classif. (of this report)	20. Security Classif. (of this	page)	21. No. of Pages	22 Price*	
Unclassified	Unclassified		526	1	

## HYPERSONIC RESEARCH ENGINE/AEROTHERMODYNAMIC INTEGRATION MODEL - EXPERIMENTAL RESULTS

Volume IV - Mach 5 Component Integration and Performance

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#### SUMMARY

An extensive aerothermodynamic development program for the purpose of advancing the technology of airbreathing propulsion for hypersonic flight has been conducted by NASA in the form of the Hypersonic Research Engine (HRE) Project. The engine components (inlet, combustor, and nozzle) aerothermodynamic development program culminated in the testing of an engine which integrated these components and allowed assessment of engine performance at Mach numbers of 5, 6, and 7. This engine was termed the Aerothermodynamic Integration Model (AIM) and was a water-cooled, hydrogen-fueled, full-scale configuration of the HRE design concept, 18 inches in diameter at the cowl lip and 87 inches long.

Descriptions of the AIM tests and a computer program used in the engine performance analyses, as well as data results and analyses, have been previously documented. All of the results of the engine performance computer program, including enough information to enable additional analysis or interpretation of the data, are reported in four volumes. Volume I presents Mach 6 component integration results that were obtained with supersonic combustion. During the integration tests, inlet unstart limits were determined for fuel injection from the first stage fuel injectors only and for multi-stage fuel injection. Optimization of the fuel injector combination that would yield the best combustion and engine performance was attempted. Volume II presents Mach 6 engine performance results during supersonic and subsonic combustion modes. Combustion mode transition was successfully performed, exit surveys made, and effects of altitude, angle of attack, and inlet spike position were determined during these tests. Volume III presents Mach 7 component integration and engine performance results with supersonic combustion modes. Fuel injector optimization was again attempted, exit surveys made, and the effects of low free-stream total temperature, free-stream oxygen content, and angle of attack were studied during these tests. Volume IV (present report) presents Mach 5 component integration and engine performance results with supersonic and subsonic combustion modes. Combustion mode transition was successfully demonstrated, exit surveys made, and effects of free-stream total temperature, free-stream oxygen content, and angle of attack were investigated during these tests.

### INTRODUCTION

The NASA Hypersonic Research Engine (HRE) Project was undertaken to design, develop, and construct a hypersonic research ramjet engine for high performance and to flight test the developed concept on the X-15-2A airplane over the speed range from Mach 3 to 8. It should be emphasized that from the beginning the design was specified to be a research ramjet engine to conduct meaningful experiments and was in no sense intended to be a small-scale prototype of a propulsion system for any particular mission.

About one year after the development phase of the HRE program was underway, the X-15 program was phased out; as a result, adjustments to the project plan and scope were necessitated, which were, however, effected without detriment to achievement of the basic project objectives. The result of the adjustment was that ground testing became the major experimental effort for the HRE program. Engine aerothermodynamic components (inlet, combustor, and nozzle) were developed in separate ground-test programs. Results of the development tests are documented in references 1 through 3. Regeneratively cooled engine structures were also included in the ground-testing program. Tests of the hydrogen-cooled engine structure progressed from small panels and problem area components in laboratory setups to wind-tunnel tests at Mach 6.7 of a full-scale, flight-weight engine termed the Structure Assembly Model (SAM). Results of this program, which was completed in May 1971, are reported in reference 4. Culmination of all the HRE development testing was the engine tests of what was termed the Aerothermodynamic Integration Model (AIM). The purpose of the tests of this full-scale, watercooled, hydrogen-fueled engine was to integrate the aerothermodynamic components and to assess the engine performance at Mach numbers of 5, 6, and 7. Successful tests of the AIM were completed in April 1974.

The AIM employed the HRE design concept of an axisymmetric engine, 18 inches in diameter at the cowl lip and 87 inches long. Versatility was incorporated into the AIM to allow: (1) inlet spike translation for optimum air flow and inlet internal contraction ratio variation; and (2) hydrogen fuel injection for tailored fuel distribution for proper heat release in a diverging combustor, and to change the mode of combustion from supersonic to subsonic or vice versa. The AIM tests are reported in reference 5 and data results of the tests have been analyzed in terms of engine performance by use of a computer program (ref. 6) generated during the HRE program. Results of these analyses are reported in references 7 through 9.

The purpose of the present reports (herein and refs. 10 to 12) is to present experimental engine performance results obtained from computer program analyses of the test data. These results contain the free-stream conditions, pressure distributions, fuel injection configuration and rate, etc., that should enable additional analysis or interpretation of results other than those previously reported. It

should be noted that all units are in U.S. Customary Units because the data results from the HRE contracts, which were initiated in May 1965 with a follow-on effort in February 1967, were under that system. Because of the cost that would have been incurred if the contractors had been required to change to the metric system, the U.S. Customary Units were retained through the HRE contractual effort; this procedure is consistent with the guidelines for conversion established by NASA.

#### SYMBOLS

All units are in U.S. Customary Units because of the reason noted above.

A area, ft.<sup>2</sup>

M Mach number

P or p pressure, psia

r radius, in.

 $R_{C1}$  cowl lip radius at 12<sup>0</sup> tangent point (see table 3), in.

x longitudinal distance from inlet spike virtual tip (see table 3), in.

CL longitudinal distance from inlet spike virtual tip to the cowl lip 120 tangent point (see table 3), in.

 $\Delta x$  longitudinal distance inlet centerbody moved from inlet physical close-off, in.

 $\Delta\Delta x$  difference between an actual  $x_{CL}$  value and the Mach 6  $x_{CL}$  value of 34.884 in., in.

T temperature, OR

 $\alpha$  angle of attack, deg.

fuel equivalence ratio; value of unity is for stoichiometric combustion (subscript symbols or notations, such as  $\phi_{1A}$  or ERIA, represent the values for the designated fuel injector (e.g., IA), EROA is the sum of all  $\phi$ -values).

#### Subscripts:

0 free stream

ref. reference condition

th throat

T total

### **APPARATUS**

## Experimental Tests

Experimental tests of the HRE/AIM were conducted in the Plum Brook Hypersonic Tunnel Facility (HTF) (figs. 1(a) and 1(b)) at nominal Mach numbers of 5, 6, and 7. The AIM is shown partially installed in the HTF in the photographs of figures 1(c) and 1(d). During the tests the engine was nearly completely enshrouded except for an 11-inch gap between the facility nozzle exit and the front of the shroud as depicted in the schematic of figure 1(e). This test configuration was suggested by results of a subscale tunnel starting investigation reported in reference 13.

A description of the facility and the results of calibration tests are presented in reference 14. The test facility used an induction-heated, drilled-core graphite storage bed to raise the temperature of nitrogen to a nominal  $4960^{\rm O}$  R at a maximum design pressure of 1200 psia. The nitrogen was mixed with ambient-temperature oxygen to produce synthetic air. Diluent nitrogen was added with the oxygen in the mixture at tunnel Mach numbers below 7 to control free-stream total temperature and to supply the correct weight flow. Because of facility heater deterioration and a lack of time to implement necessary repairs, true temperature simulation of  $3700^{\rm O}$  R at Mach 7 was not achieved; a maximum temperature of about  $3100^{\rm O}$  R was obtained.

The original test plan is summarized in table 1. Because of testing problems and limitations in facility schedule, the test plan was altered to provide a maximum of data to meet the test objectives. Details of the AIM tests are described in reference 5. General test conditions, results, and remarks of the AIM tests were tabulated in references 5 and 9 and are presented herein as table 2. All tests (reading numbers in second column) are listed including the tests that were aborted because of tunnel starting or other problems. Run numbers were assigned to AIM reading numbers or groups of AIM reading numbers with the same test objective (some readings represent zero success, partial success, or are reruns of others) to provide a means for a cross-check with the original plan.

#### Model

The HRE/AIM was a full-scale (18 inches in diameter at the cowl and 87 inches long), water-cooled, hydrogen-fueled research engine. Details of the design and fabrication of the AIM have been reported in references 16 through 29. The design is described generally in references 5 and 9, and some difficulties encountered with the AIM during the tests are discussed in reference 5.

A schematic of the AIM is presented in figure 2 and the coordinates are listed in table 3. The AIM incorporated a mixed compression inlet with a translating spike that enabled the close-off of the engine (an early HRE program

requirement). The inlet was designed for spike translation to the most open position for Mach 4 to 6 operation with spillage occurring up to Mach 6. At Mach 6 "shock-on-lip" occurred, and from Mach 6 to 8 the spike was designed to translate to maintain shock-on-lip over this Mach number range. An "upsloping throat" was incorporated in the inlet which enabled the inlet to not only maintain shock-on-lip with spike translation for Mach 6 to 8, but also to have increased inlet contraction ratio with increased Mach number. The combustor was designed with diverging walls and the area distribution is shown in figure 3(a) with fuel injector locations indicated. Figure 3(b) presents a sketch of the combustor with the locations of the staged fuel injectors and two sets of ignitors indicated (a third set of ignitors planned for the outerbody at an x-station of 54.38 inches was not installed). The set of ignitors at an x-station of 42.0 inches malfunctioned and use was discontinued (see fig. 3(b)) about midway in the Mach 6 test program (see discussion in ref. 5). Injectors 1A, 1B, 1C, 4, 2A, and 2C were designed to allow optimum distribution of the fuel in the combustor to obtain a fuel equivalence ratio,  $\phi$ , of unity during the supersonic combustion mode. During the supersonic combustion mode, it was desired to inject the maximum amount of fuel from the first-stage injectors (1A and 1B) without unstarting the inlet; all of the fuel was designed to be injected from injectors 1A and 1B at Mach 8. Injectors 3A and 3B were designed for use in the subsonic combustion mode. The locations are tabulated in figure 3(b) for the designed Mach 6 inlet operating position; cowl lip positions other than the Mach 6 position (because of spike translation) result in different x-station values for the injectors and ignitors on the outer wall and also for injector 3B. These changes are accounted for in the performance results presented herein.

#### Instrumentation

Planned instrumentation for the AIM is documented in reference 15. All of the instrumentation planned was not used because of facility instrumentation recording channel limitations or damages to instrumentation in inaccessible places during the AIM final assembly or during AIM repairs at the test site. A list of all planned instrumentation is presented in table 4 (obtained from ref. 5) with notations indicating the items not installed or damaged, the recording channel numbers for each item used, and the ranges of the pressure transducers or thermocouples.

### Method of Calculation

A computer program that incorporated methods described in reference 15 was used in reducing the data from the AIM tests to engineering units. Listings of this program were checked for accuracy and determination of steady-state conditions. Times of interest were selected from each run and the information from the engineering units computer program was used in a performance analysis computer program which incorporated methods described in reference 6. After the erroneous surface pressures were eliminated, the remaining pressures at each station were averaged by the performance computer program which then performed surface-pressure integration by linear interpolation and determined the skinfriction coefficients. Chemical equilibria of the synthetic air and fuel-air mixtures were calculated by the program using methods described in reference 30.

## Description of Performance Program Methods

General.- Several methods were used to establish validity of critical parameters, such as the wind tunnel Mach number. The first method used curves generated from instrumentation rakes installed during calibration of the wind tunnel. The second method used measured values of wind tunnel total pressure and temperature, and pitot pressure at the spike tip along with real-gas, normal-shock solution to calculate the wind tunnel Mach number. The third method used measured values of wind tunnel total temperature, spike-tip pitot pressure, and spike cone surface pressure, along with the real-gas, normal-and conical-shock solutions, to calculate the wind tunnel Mach number. Calculations made utilizing each of the three methods indicated good agreement. After confidence was established in the three methods, the use of the third method was discontinued, since it required excessive computer time. Additional information concerning tunnel Mach number determination is contained in reference 9.

The conditions at the inlet throat were determined by computing the momentum and total enthalpy from the pressure forces and accounting for friction and heat losses incurred on the inlet spike and the internal surfaces. The inlet mass flow ratio and additive drag were determined from theoretical calculations (ref. 31). Pressures used in these calculations were obtained as follows: (1) for conditions where inlet start was obtained ( $M_{th} > 1$ ), the calculated mass-momentum-average static pressure was used, and the measured static pressures at the throat were not used; and (2) for conditions where inlet unstart was experienced ( $M_{th} \le 1$ ), the average of the measured static pressures at the throat was used with the Mach number constrained to unity to calculate spillage and additive drag.

For both cases above, the flow was analytically expanded (isentropically) from the inlet throat conditions to the freestream static pressure in order to determine the hypothetical static enthalpy and associated velocity which are required to compute the inlet kinetic energy efficiency and the inlet process efficiency (as required under the contract statement of work). Also the flow was analytically compressed (isentropically) from the inlet throat conditions until the calculated total enthalpy matched the known total enthalpy after heat loss. For a started inlet, a side calculation was made by isentropically expanding the flow to an area which was arbitrarily set 10 percent larger than the throat area (for flow stability). At this point, the flow was passed through a normal shock. The limiting subsonic pressure recovery for the inlet and the corresponding kinetic energy and process efficiencies were then determined from conditions downstream of the normal shock. These inlet performance parameters were considered of interest as indicators of the overall inlet performance and of flow conditions prior to inlet unstart.

Two methods were used to calculate conditions at the combustor stations: (1) up to the first station where fuel was injected, the mass-momentum-averaged static pressure that satisfied the state, continuity, momentum, and energy equations was calculated; and (2) at stations downstream of the first fuel injector the average of the measured innerbody and outerbody pressures was used, and the combustor efficiency was calculated to satisfy the conservation equations. For these methods it was assumed that the flow area equals the geometric duct

area (no flow separation). The amount of hydrogen required to react in order to satisfy the measured static pressure, the duct area, the heat loss, and the conservation equations is computed by the program. Of the total hydrogen injected or present in the flow at a given station, the amount which reacts has been named "real" hydrogen and is used in the equilibrium chemistry process being completed. The hydrogen which is not reacting has been named "inert" hydrogen. The concept of real and inert hydrogen and the station-wise conversion from inert to real is simply a bookkeeping procedure in the program which simulates or "models" the mixing process. The inert hydrogen is assumed to have the properties of an inert gas, not to react with other species, and not to dissociate.

The combustor throat was defined as the point of minimum-flow area between the struts in the subsonic combustion mode and at the strut exit plane in the supersonic combustion mode. When the computed one-dimensional Mach number at the assumed combustor exit was found to be less than 0.95, the computation was considered to improperly represent the subsonic combustor flow situation in that the flow must have reached a sonic point further downstream. With the area increasing added combustion (heat release) downstream of the assumed combustor exit station is implied. Therefore, a side calculation was made of the combustor efficiency required to produce sonic velocity at the assumed combustor exit station, as if this added heat release occurred prior to the assumed combustor exit station. For this condition, the performance program printout shows results under the heading SONIC THROAT (e.g., reading 94, time 150.342 sec).

The regeneratively cooled combustor performance ("COMBUSTOR REGEN" in the performance program printout) was simulated by recalculating the total enthalpy at the combustor exit as the sum of the free-stream enthalpy of the synthetic air, the enthalpy of the hydrogen fuel at  $50^{\circ}$ R, and the absolute value of the heat loss through all the engine surfaces wetted by the internal flow stream. Using this total enthalpy, the stream total pressure, and the same combustion efficiency, the combustor exit static-state properties were also computed.

Nozzle performance was obtained by isentropically expanding the flow from the actual and regeneratively cooled combustor exits to the nozzle exit area and to ambient pressure ("NOZZLE AE" and "NOZZLE PO" in the performance program printout). The flow was then isentropically expanded from the actual combustor throat to those nozzle stations representing the locations of pressure taps, and the local skin-friction coefficients were calculated using the Spalding-Chi correlation. The nozzle vacuum stream thrust coefficient was also computed. This coefficient is arbitrarily defined in previous HRE documents (e.g., refs. 3 and 15) as the ratio of the actual nozzle exit total momentum (stream thrust) divided by the theoretical nozzle exit total momentum where the flow was isentropically expanded from the combustor exit conditions to the nozzle exit area (512.389 in<sup>2</sup>). The actual nozzle exit total momentum was determined by taking the combustor exit total momentum and adding (or subtracting) the pressure force, the friction force, and one-half of the calculated drag force (onehalf of strut assumed to be charged to the nozzle component). The hypothetical static enthalpy resulting from the computed isentropic expansion from the combustor exit conditions to the free-stream static pressure was used to calculate the nozzle kinetic energy and process efficiencies.

Side calculations were made of a fictitious stagnation combustion process (constant pressure and zero velocity) with 100 percent combustion efficiency and no loss to the walls (denoted in the performance program printout as "FICTIVE COMBUSTOR"), followed by an isentropic expansion to ambient pressure to obtain the combustor effectiveness. Also to obtain the combustor effectiveness, the flow at the combustor exit was expanded to free-stream static pressure and the total momentum at this pressure was determined. The combustor effectiveness (ref. 15) is then the change in total momentum for the actual combustor process from the combustor entrance condition to the expanded (free-stream static pressure) condition divided by the change in total momentum for the fictitious process mentioned above from the combustor entrance condition to the expanded (free-stream static pressure) condition. Side calculations were also made of a fictitious nozzle to determine the static and total conditions ("FICTIVE NOZZLE" in the performance program printout) required to match the actual vacuum specific impulse at the nozzle exit.

Calculation of cooling load distribution. - For the AIM tests, the heat loss distribution was determined from the differences between the skin thermocouples inbedded in the engine surfaces and the cooling water temperatures. Standard heat-transfer equations were used to obtain local heat losses. These losses were then adjusted linearly with the overall heat loss as measured by the overall water temperature rise. The detailed equations and procedures used for these computations are presented in reference 9.

Tare forces.- Purge nitrogen was injected in the AIM cavity between the non-metric "windshield" shroud and the metric outerbody to assure that hot tunnel gases did not enter into this cavity. This method produced a large tare force which was of the same order of magnitude as the engine net thrust. An effort was made to reduce and even control the tare force by suitable control of the pressures in two parts of the cavity. This tare-force control concept was, however, not achieved. Since the thrust is considered the most important measurement in evaluating the engine performance, special tare-force calibration tests were made and the results carefully correlated in order to determine the correction for the measured thrust. The method and procedures are described in detail in references 5 and 9.

<u>External drag.</u> The external drag was calculated from the summation of pressure and friction forces acting on the external metric surfaces of the AIM. The method and procedures are described in reference 9.

Strut force calculation. The performance program was originally programmed to calculate strut force based on a theoretical calculation, assuming uniform flow ahead of the strut. This force should be a drag term since, theoretically, pressures downstream of the maximum strut blockage should be lower than upstream. However, test data indicate that this is only true with subsonic combustion. Upon examination of the test data, it appeared that measured static pressures between struts on both the inner and outer walls (there were no measurements along the strut surfaces) could be used to represent the forces occurring on the strut surface. Thus, a pressure integral was used to determine the strut force and a calculation was also made for strut base pressure as discussed in reference 9.

Performance correction for regeneratively cooled system. The AIM incorporated a water-cooled jacket in which heat was rejected and not recovered. In order to compensate for this heat loss, hydrogen fuel was heated up to  $1500^{\circ}$  R to simulate a regeneratively cooled system. The deficiency of energy in the system in terms of theoretical energy release was less than 10 percent in all cases.

In order to correct this deficiency, the performance computer program (ref. 6) incorporated a side calculation in which the energy deficiency, because of the heat loss through internal surfaces, was added to the stream at the combustor exit with no total pressure change. The flow was then expanded to the nozzle exit with measured nozzle efficiency. The differences between the heat added to fuel and the internal cooling loss are presented for several tests in reference 9 as table 6.6-1.

Performance correction for inlet total temperature.-Because of the facility heater deterioration, the true temperature simulation of  $3700^{\circ}$  R at Mach 7 was not achieved (the test Mach number was generally about 7.25 requiring a simulation temperature of about  $3960^{\circ}$  R). It is known that the effect of decreasing total temperature is to increase the engine performance. Therefore, it is necessary to correct the measured performance for Mach 7 (ref. 12) to properly account for deviations in test conditions. Theoretical calculations indicate that, at Mach 7, a decrease of  $560^{\circ}$  R would increase the thrust coefficient by 5 percent and the specific impulse by 3.5 percent. The accomplishment of this correction in the performance computer program (ref. 6) employed the methods discussed in reference 9.

Determination of tunnel gas composition. The oxygen-to-nitrogen ratio was determined from the flow measurements of oxygen, diluent nitrogen, and nitrogen entering the storage heater, and checked by gas samples taken through two aspirating thermocouple probes  $180^{\circ}$  apart in the facility nozzle entrance prior to each run. The samples were collected in high-pressure bottles and later analyzed on a mass-spectrometer. The measured compositions for each run are presented in reference 9 as table 6.8-1. The one-dimensional performance computer program (ref. 6) used only the N<sub>2</sub> and O<sub>2</sub> values.

## **RESULTS**

Selected points of interest of the HRE/AIM test data have been analyzed by use of the one-dimensional performance analysis computer program (ref. 6). The amount of material generated requires four volumes. Mach 5 component integration and engine performance results are presented herein. Mach 6 component integration results, Mach 6 engine performance results, and Mach 7 component integration and engine performance results are presented in references 10 to 12, respectively. All of these results were used in references 7 through 9 in the discussion of the results of the AIM test program.

## Selected Test Points for Performance Analysis

Details of the AIM tests were discussed in reference 5 which included a list of all the HRE/AIM tests; this list is contained herein as table 1 (included in each volume). The individual AIM tests were recorded as consecutive reading numbers that extended through number 97 for a total operation time of 112 minutes with 41.5 minutes of combustor operations. About 60 successful tests are noted in the first column of table 2.

Reference 5 documented the fuel injection schedules, both planned and measured, for the successful tests. The measured fuel injection schedules for the successful Mach 5 tests are contained herein for convenience in figure 4. Such plots were reviewed and points (run time) of interest were selected for performance analysis. The selected points were listed in reference 9 and are included in tables 5(a) through 5(d) for the results presented in references 10 through 12 and herein, respectively, where the times correspond to the abscissa in figure 4. The first column of table 5 indicates the page number of the initial page of the data for a given test point (specific time of a reading number). Table 5 indicates the general test conditions and fuel injection equivalence ratios,  $\phi$ , for the first-, second-, and third stage injectors and the accumulative  $\phi$ -value. Also, the use of ignitors is indicated and the general purpose of the test is noted.

Vagaries in the test program that should be noted (table 5, last column) are:

- (1) Fuel equivalence ratio values,  $\phi$ , in table 5 for reading 93 are lower than the values indicated by the fuel injection schedule (fig. 4(a)). In preparation for the performance analysis, the tunnel measured oxygen content was found to be about 34 percent instead of the standard 21 percent; therefore, the fuel equivalence ratios were corrected to account for the difference in the available oxygen for combustion.
- (2) Time 235 seconds in reading 90 is for an inlet unstart condition. With an unstart, the captured mass flow is, of course, greatly decreased, and since the fuel flow rate is still high, the  $\phi$ -value would be high as indicated, therefore this time is not very meaningful.
- (3) At Mach 7 the agreement between computed thrust (a function of fpda) and measured thrust was not nearly as favorable as experienced for Mach 6. Examination of the surface static pressure distributions on the outer combustor surface in the vicinity of the pressure rise indicated some pressure instrumentation to be faulty. For reading 89, more reasonable values were substituted for the measured pressures and the performance recomputed. The recomputation was performed for two different times, 316.47 and 327.27 seconds (see table 5(c)), and the results indicate a much more favorable agreement between the computed and measured thrust. The channel numbers in which new pressure values were substituted are noted on the first page of the results for these two times. A more detailed discussion of this exercise is contained in reference 9 (section 7.7.2 Mach 7 Performance).

- (4) Times 264.04, 274.84, and 275.74 seconds of reading 96 had a fuel flow measurement malfunction that indicated no fuel flow from injector 1B. Injector 1B manifold pressure, however, indicated flow to exist at pressure levels about equal to planned pressure levels ( $\phi$ -values about the same as for injector 1A). The performance calculations for these times of reading 96 erroneously used only fuel flow from injector 1A.
- (5) At time 313.54 seconds, also of reading 96, the test chamber pressure was noted to be high, thus yielding unrealistically high pressures on the AIM nozzle shroud and plug that would, of course, contribute erroneously to increased engine thrust.

## Description of Performance Computer Results

The selected points listed in table 5 were analyzed using the performance computer program described in reference 6. As noted in the Method of Computation section, the AIM test data were reduced to engineering units and reviewed for erroneous data. Such data were "coded out" in the performance computer program. Table 6 indicates the channels that were coded out. The COXX indicates the code outs for a reading number, e.g., for reading 33, CO33 is indicated. Channels that are coded out are listed adjacent to the notation KODSEL, e.g., for reading 33 the first and last of 85 coded out channels are 60 and 399, respectively. The locations and type of measurement for the listed channels may be determined by referring to table 4.

Several points (run time) of interest were selected for each run as indicated in table 5. The page numbers indicated in the first column of table 5 are output listings of the performance computer program (ref. 6). For each time of interest there are seven or eight pages of computer output listings. On each of these pages a standard heading exists: READING number (test number); BLOCK number (numbered sequentially and corresponding to recording times of test data); TIME (of data recording, seconds); MACH number (in wind tunnel); PT (total pressure in wind tunnel, psia); TT (total temperature in wind tunnel, OR); and PAGE number.

Station flow parameters.- A summary of flow parameters at each calculation station in the AIM is contained on pages 1, 2, and 3. Each station is headed by a station designator (i.e., WIND TUNNEL, INLET THROAT, COMBUSTOR, etc.), followed by three integers (the zero following the combustor designator is meaningless). The first integer denotes the station number, the second denotes the combustor station, and the third denotes the number of interations required to converge on a solution. The third integer may assume values between 0-21, 100-121, and 200-221. A value of the third integer equal to 21 denotes that the mass flow was too great or the flow area too small to obtain a solution, 121 denotes that the solution for total conditions did not converge in 21 interations and 200-221 denotes that the mass flow was too small or the flow area too large to obtain a solution. When both solutions for static and total conditions have converged, the third integer may assume the values 1-20 or 101-120 depending upon which solution (static or total) required the larger number of interations. Columns 2-8 have two rows of values for each station; total and static conditions in first and second rows, respectively.

Most of the station designators are self-explanatory. The first appearance of the designators WIND TUNNEL and SPIKE TIP NS (NS = NORMAL SHOCK) reports conditions in wind tunnel and upstream of the spike tip based on a wind tunnel Mach number determined from calibration runs. The second appearance of these designators reports these conditions based on a wind-tunnel Mach number calculated from the total and pitot pressures and the total temperature of the synthetic air applied to the normal shock equations. The designators INLET UPNRSK and INLET DNNRSK denote conditions upstream and downstream of a normal shock positioned at a fictitious flow area 1.10 times the flow area at the inlet throat. The designator COMBUSTOR REGEN denotes, for cases with fuel flow, conditions at the combustor throat simulating a regeneratively cooled ramjet. In some cases (e.g., reading 94 time 150.342 sec) the designator SONIC THROAT appears ahead of the COMBUSTOR REGEN. This denotes the results discussed in section entitled "Description of Performance Program Methods." NOZZLE AE and NOZZLE PO report conditions when the flow is expanded isentropically to the nozzle exit area and to the windtunnel static pressure, respectively. NOZZLE AE REGEN and NOZZLE PO REGEN denote, for cases with fuel flow, conditions at the nozzle exit simulating a regeneratively cooled ramjet. FICTIVE COMBUSTOR denotes stagnation combustion conditions (zero velocity and constant pressure) with combustor efficiency equal to unity. FICTIVE NOZZLE reports conditions required to match the actual momentum and nozzle exit area.

Definition and units of parameters in the SUMMARY REPORT, pages 1-3 in the computer listings, are listed below:

P - pressure, psia T - temperature, OR H - enthalpy\*, Btu/lbm GAMMA - specific heat ratio MOLWT - molecular weight SONV - conic velocity, ft/sec MACH - Mach number VEL - flow velocity, ft/sec S - entropy, Btu/lbm-OR W/A - flow rate per unit area, lb<sub>m</sub>/sq in W - flow rate, lb<sub>m</sub>/sec A/AC - mass flow ratio MØMTM - flow momentum, lb<sub>f</sub> Q - dynamic pressure, lb<sub>f</sub>/sq in IVAC - vacuum specific impulse, lb<sub>f</sub>-sec/lb<sub>m</sub> PHI - equivalence ratio (see discussion in Ramjet Performance section) ETAC - combustor efficiency

$$\sum_{i}^{T} \int_{0}^{C_{p,i}dT} C_{p,i}dT \quad \sigma_{i}(T) = \sum_{i}^{\Sigma} H_{f,i}^{298} + \int_{298}^{T} C_{p,i}dT \quad \sigma_{i}(T)$$

$$- \sum_{i}^{\Sigma} H_{f,i}^{298} + \int_{298}^{300} C_{p,i}dT \quad \sigma_{i}(T) + \sum_{i}^{\Sigma} \int_{0}^{C_{p,i}dT} \sigma_{i}(T)$$

where:  $C_{p,j}$  is specific heat at constant pressure,  $Btu/1b_m$  -  $^{O}R$ , and  $\sigma_i(T)$  is the mass fraction of the specie i as a function of temperature and  $H_f$  is fuel enthalpy. 12

<sup>\*</sup>Two values were reported. The first value (column 4) was the JANNAF-based enthalpy. The value in parentheses (column 5) was the enthalpy potential or the sensible enthalpy based on the equation

Cooling and surface-pressure parameters. Surface pressures, cumulative surface-pressure integrals, cumulative cooling losses, cumulative surface area, and pressure ratios for axial distances from the AIM virtual spike tip are listed on pages 4 and 5.

Definitions and units of the parameters are as follows:

```
XABS - axial distance from virtual spike tip, in P-IB - surface pressure on innerbody, psia P-ØB - pressure on cowl inner surface, psia PDA - cumulative surface-pressure integral, \int_{0}^{\chi} ABS_{PdA}, 1b_{f} QØX - cumulative total cooling loss, Btu/sec Q-IB - cumulative cooling loss from innerbody, Btu/sec Q-ØB - cumulative cooling loss from outerbody, Btu/sec CAWALL - cumulative surface area, sq in P-IB/PSØ - innerbody static to wind-tunnel static-pressure ratio PPB/PSØ - outerbody surface static to wind-tunnel static-pressure ratio PØB/PSØ - outerbody surface static to wind-tunnel static-pressure ratio PØB/PTØ - outerbody surface static to wind-tunnel total-pressure ratio
```

Drag and heat-transfer coefficients. Longitudinal values of drag force and drag and heat-transfer coefficients are listed on page 6 (for some cases on page 6 and 7). Definition and units of the parameters are as follows:

```
X - axial distance from spike virtual tip, in DDRAG - incremental frictional drag force, lf_f CDRAG - cumulative frictional drag force, lf_f C_F - friction-drag coefficient HC - heat-transfer coefficient, Btu/(sec-sq\ ft-^{O}R)
```

Ramjet performance.— AIM performance parameters and pertinent information are contained on page 7 (page 8 for some cases). The performance parameters are generally self-explanatory; detailed discussion about the methods of computation are presented in references 6 and 9. Parameters listed below STATIONS are presented since they are related (except for the inlet throat) to the cowl leading-edge station. The NOMINAL COWL LEADING EDGE refers to the  $\chi_{Cl}$  (table 3) value for the Mach 6 design operating position. SPIKE TRANSLATION is the recorded distance between the nominal and the actual  $\chi_{Cl}$  value (this distance is designated as  $\Delta\Delta x$  in symbols and used in figure 3(a)); all dimensions other than those for the inlet spike are corrected by this amount.

The fuel injectors and their corrected stations in inches are shown. A letter in the VALVE column indicates the injectors that were in use during the respective time. Table 5 indicates the general fuel equivalence ratio values for the various injector stages. The actual fuel equivalence ratio, however, for each injector can be determined by noting the step increases in the PHI column on the output, pages 1-3, for the respective time (ignore 0.01 or 0.02 changes); the step difference at the combustor station corresponding to the indicated injector station is the  $\phi\text{-}\text{value}$  for the respective injector.

#### SUMMARY OF TESTS

The Hypersonic Research Engine/Aerothermodynamic Integration Model was tested in the NASA Hypersonic Tunnel Facility at the Plum Brook Station of the NASA Lewis Research Center. Synthetic air (heated nitrogen with proper amount of oxygen added) was delivered by the facility at nominal Mach numbers of 5, 6, and 7. The Mach 5 and 6 tests were conducted at true air temperature while Mach 7 tests were conducted at Mach 6 temperature (3000° R) because of heater deficiency. Changes in total temperature and instream oxygen content at Mach 5 and 7 were also explored. The hydrogen fuel was heated up to 1500° R prior to injection to simulate a regeneratively cooled system.

The engine testing was completed with an accumulated actual running time of about 112 minutes with 41.5 minutes of combustor operation. The important achievements realized from this test program which advanced the state-of-the-art in hypersonic propulsion were discussed in detail in reference 9 and are:

1. Realistic engine performance levels for hypersonic flight were obtained from Mach 5 to 7.

Test Mach No.	Equivalence Ratio	Internal Thrust Coefficient	Internal Specific Impulse
5.1	1.0	0.910	2740
6.0	1.0	0.735	2360
7.25	1.0	0.570	2170

- Engine inlet performance agreed well with theoretical prediction.
   Combustor efficiency of 95 percent was achieved. Nozzle vacuum thrust coefficient was lower than predicted.
- 3. The interaction effects in staged fuel injection were very important in achieving auto-ignition, high combustor efficiency, and overall performance. High supersonic combustor efficiency in a diverging duct was difficult to achieve. The strong stage interaction effects discovered during these tests may be used to great advantage in future designs.
- 4. The "transonic combustion" or "mixed combustion mode" was the most efficient heat addition process in the range of Mach numbers and temperatures tested in this program.
- 5. The effects of ignitors, altitudes, spike translation, fuel schedules, angle of attack, step and struts, inlet gas composition, inlet total temperature, and component interactions were investigated and correlated.

- 6. Stable subsonic and supersonic combustion and convertibility over a range of fuel equivalence ratios at Mach 5 and 6 was demonstrated.
- 7. The overall cooling load and its distribution as compared with theoretical prediction was determined.
- 8. Experience was acquired in free jet testing in a ground test facility with large model blockage and combustion.

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Table 1. - Summary of planned HRE/AIM wind tunnel tests.

## (obtained from ref. 9 and 15)

RUN	H <sub>O</sub>	PTO, PSIA	TTO, °R	'n	FUEL SYSTEMS	FUEL SCHED.	INLET DX, IN.	COMBUSTION MODE	RUN TYPE AND PURPOSE
-	٥	466	1500	٥	-	-	4,23	-	Purge force, nominal case
2	6	466	1500	0	-	-	1.90	-	Purge force, effect of spike position
3	٥	466	1500	3	-	•	4.23	-	Purge force, effect of angle of attack
4	۱۰	466	2000	٥	-		4.23	-	Operation checkout, effect of higher TTO
5	٥	466	3000	٥	•	-	0, 1.71, 2.52 4.23, aft stop	-	Airflow calibration, effect of altitude
•	٥	930	2946	0	•	-	0, 1.71, 2.52 4.23, aft stop	-	Airflow calibration, nominal case
'	•	930	2946	3	•	-	0, 1.71, 2.52 4.23, aft stop	-	Airflow calibration, affect of angle of attack
8	0	930	2946	0	ia, ib	1	4.23	Supersonic	Inlet-combustor performance, ignition and inlet unstart limits
9	٥	930	2946	0	ia, ib, 2a, 2c	2	4.23	Supersonic	Inlet-combustor performance, injector optimization
10	•	930	2946	0	1c, 4, 2a, 2c	2	4.23	Supersonic	Inlet-combustor performance, injector optimization
н	۱۰	930	2946	0	1a, 1b, 1c, 4	3	4.23	Supersonic	Inlet-combustor performance, injector optimization
12	۱	930	2946	0	TBD	TBD	4.23	Supersonic	Inlet-combustor performance, injector optimization
13	6	400	3000	0	la, 16, 2a, 2c	2	4.23	Supersonic	Inter-combustor performance, effect of altitude
14	۱٥	700	3000	0	la. lb, 2a, 2c	2	4.23	Supersonic	Inlet-combustor performance, effect of altitude
15	6	930	2946	0	1a, 1b, 2a, 2c	2	Aft stop	Supersonic	Inlet-combustor performance, effect of spike position
16	۰	930	2946	0	la, lb, 2a, 2c	2	2.52	Supersonic	Inlet-combustor performance, effect of spike position
17	٠	930	2946	0	la, lb, 2a, 2c	2	1.71	Supersonic	Inlet-combustor performance, effect of spike position
18	6	930	2946	0	3a, 3b	4	4.23	Subsonic	Inlet-combustor performance, subsonic combustion
19	٠	930	2946	0	3e, 3b	5	4.23	Subsonic &	Engine performance, subsonic combustion and transition
20	۰	930	2946	٥	la, lb, 2a, 2c	2	4.23	Supersonic	Engine performance, nominal case
21		466	2946		la, lb, 2a, 2c	2	4.23	Supersonic	Engine performance, effect of altitude
22	٠	930	2946	3	la. lb. 2a. 2c	2	4.23	Supersonic	Engine performance, effect of angle of attack
23	,	520	1 500	٥			2.88	-	Purge force
24	7	520	3965	0	<b>.</b> .	-	2.34, 2.88 3.24	•	Airflow calibration, effect of altitude
25	7	1000	3840	٥	•	-	1.98, 2.88 3.24		Airflow calibration, nominal case
26	,	1000	3840	3	•	•	2.34, 2.88 3.24		Airriow calibration, effect of angle of attack
27	,	520 A	3965 3840		la, Ib	6	2.88	Supersonic	Inlet-combustor performance, ignition and inlet unstart limits
28	,	1000	3840	0	la, 16, 2a, 2c	7	2.88	Supersonic	Inlet-combustor performance, injector optimization
29	7	1000	3840	0	1c, 4, 2a, 2c		2.88	Supersonic	Inlet-combustor performance, injector optimization
30	7	1000	3840	0	la, lb, lc, 4	8	2.88	Supersonic	Inlet-combustor performance, injector optimization
31	,	1000	3840	0	TBD	TBD	2.88	Supersonic	Inlet-combustor performance, injector optimization
32	,	522	3965	٥	1a, 1b, 2a, 2c	7	2.88	Supersonic	Inlet-combustor performance, effect of altitude
33	,	700	3965	٥	la, lb, 2a, 2c	7	2.88	Supersonic	Inlet-combustor performance, effect of altitude
34	,	1000	3840	٥	la, 16, 2a, 2c	7	3.24	Supersonic	Inlet-combustor performance, effect of spike position
35	,	1000	3840	0	la, Ib, 2a, 2c	,	2.34	Supersonic	Inlet-combustor performance, effect of spike position
36	,	1000	3840	0	la, lb, 2a, 2c	7	1.98	Supersonic	Inlet-combustor performance, effect of spike position
37	,	1000	3840	0	ia, ib, 2a, 2c	,	2.68	Supersonic	Engine performance, nominel case
38	,	522	3965	ŏ	ta, 1b, 2a, 2c	,	2.88	Supersonic	Engine performance, effect of altitude
39	,	1000	3840	3	la. lb. 2a. 2c	7	2.88	Supersonic	Engine performance, effect of angle of attack
40	5	445	1500	٥	la, lb, 2a, 2c	-	4.23		Purge force
41	5	206		0	la, lb, 2a, 2c	-	4.23		Airflow calibration
42	5	415	2210			9	4.23	Supersonic	
43	5	415		0	la, 16, 2a, 2c	TBD	4.23	Supersonic	
44	5	415			la, lb, 20, 2c	9	4.23	Supersonic	•
45	5	415	2210	0	3e, 3b	10	4.23	Subsonic	Engine performence, subsonic combustion
46	5	415	2210		1a, 1b, 2a, 2c	"	4.23	Subsonic & Supersonic	Engine performance, effect of angle of attack

Table 2. - HRE/AIM Test Run Summary (obtained from ref. 5).

			Data not valid due to mechanical interference between AIM and outer cost body	Test terminated due to cooling system overpressure abort system failure.	Tunnel nozzle started. Inlet started. Strong shocks in test section. Cell pressure - 2.0 psie.	Test aborted due to facility problem (TAFP).	facility shroud extended and washer added to assist tunnel start (TAFP).	TAFP	Mozzia starr and inlet start obtained Cell pressure "1, 2 psis", Weda nozzia pressura changed from 50 to 60 psis, No improvement in cell pressure.	TAFP	Medge nozzle pressure 55 to 90 psig. No tunnel nozzle stert. Nozzle sterted when iniet closed for shutdown.	TAFP	LAFP	First combustion attempt. TAFP	Mozzle start not obtained. TAFP.	nozze star toblatend by cycling inter spike open and closed. Inter start obtained. Fuel remped to equivalence ratio = .25 prior to tunnel unstart and TAFP.	Mozzle start with inlet pertially open. (A x = 0.99). TAFP. No fuel Injected.	No start at \$4 = 0.99. Nozzla started by cycling inlet spike. Combustor III causing tunnel unstart.	Jet pump installed. Test aborted due to freezing of coolent supply system.	Jet pump used for this test. Mozzle start obtained. Unstart experienced when inter was opened. Test aborted manually. Nozzle restart noted during shutdom.	Jat pump and wedge nozzle inlet pressure varied. Nozzle start was not obteined. Use of jet pump did not effect test chember pressures. Seets between AlM support struts and facility shroud blosm out.	Jet pump inactivated. TAFP	TAFP	Hozzle start and engine start obtained. Fuel injected for the second priot to mozzle unstart. Unstart attributed to exessive fuel injected caused by facility walve malfunction.	Nozzle start and inter start obtained. Jet pump inactivated. Full was injected, angine infat unter appartated 12 seconds later. Inter start reatablished and fuel again injected. Inter unterte separtanced 9 seconds later. Test uses amoustly aborted. Coal teading edge assembly separated from the outer body. Cause of the separation was stributed to festive of the start had stributed to festive of the screw heads. The failure was caused by overheating of the screw heads. The failure was caused by overheating of the screw heads are ungestion of turnel amount to this area. Ingestion of turnel amoint was the result of Additional dispoststic introduced may be a shock standing on the Alf comi.	Tunnel configuration same as config. 8 except washer inside diameter changed to 44,5 inches. Tunnel unstart observed 19 seconds after feel introduced. Start resistablished. Test manually aborted 3 seconds later when excessive healing of MELAI coal leading edge assembly mount flangs was noted. Excessive healing of the external skin of the Aliw was noted.
	Obligation of Tax	Ubjective of lest	Pra-run reference No-airflow engine Purge system calibration	Facility and engine checkout	Same as run 2	Establish facility operational procedure	Same as run 4	Same as run &	Same as run &	Same a's run &	Same as run la	Same as run &	Same as run 4	Same as run 4	Some as run &	- Lon 4	Same as run 4	Same as run &	Establish facility operational procedure	Same at run 12 above	Same as run 12 above	Same as run 12 above	Same as run 12 above	Same as run 12 above	Same as run 12 above	Establish facility operational procedure to obtain hyperconic airflow.
П	3 3	×				-			8:	•				•	•				,			•	•		•	
			•	•	٠	•	·	·	•	•	•	•	·	•	•			•	٠	•	•	•	•	•	•	'
#	[ ]	^	•	3	56	\$	•	·	ĕ	•	0)	ž	91	×	8 8	3	13	6	•	22	33	•	•	ç	3	=
	5	£	• •	٠	2	•	•	•	~	٠	-	•	$\overline{}$	•	-  -	-	•	-	•		•	·	·	•		-
*	Tunnel	Contrig.	<	<	٧.	٧	=			10		10		=			<b>.</b>		נו	5	ı	73	8	a	<b>z</b>	82
]	Injectors	9 5	,		•	•		•				•		١, د	ه و	•	•	16. 4	•	•	•	٠		14, 18	•	14, 18
tolet	Position,	∆x.1n.	•	4. 266	4, 266	4.266	4,266	£. 266	4. 266	3.962	3.962	3.962	4. 266	<b>4</b> . 266			0.99/	0.99/ 4.00	0.99/	0.99/ 4.00	0.99/ 4.00	0.99/	0.99/ 0.00/	0.99/ 4.98/	, 66.99 8.39 9.39	0.99/ 4.00
5	1.0°	9		1500/2100	1500	1500	995	1500	1500	2250	2250	2950	2950	2800			2950	2950	3000	3000	0001	3000	000€	000€	9100	3100
Inlet Condition	P. 0.	9		99	466	994	994	466	994	999	994	994	994	99		•	466	466	750	750	750	750	S.	750	ox6	930
=	5	į		•	,	9	•	9	,	9	9	9	9	J	. .		•	۰	٠	•	•	9	9	,	9	9
		-	g/√1/8	10/31/72	1/11	11/3	91/11	91/11	91/11	11/31	12/11	11/51	12/8/72	1/18/73		•	1/1	7/2	£1/51/2	18/2	12/2	1/23	1/13	1/13	7.4	3/16
	Reading	ġ	1 through 5	•	,		6	.01	"	12	£.	16	18	٩	= =	•	61	e R	ű	2	a	74	25	92	23	28
	ā:	ġ	-	~	•	3	\$			9		-	-	•			2	=	2	=	2	~			91	-1

\* see figure 5-9, reference 5

Table 2. - Continued.

																		•	
	Comments	Ne-run of reading 23 with seal repaired. Jet pump did not improve tunnel start,	Shroud inlet washer replaced with cons-cylinder and 15° conical diffuser inlet contraction replaced with 7° cons; tunnel nozzle did not start.	Effect run with fully started tunes! Shroud Inlest cone cylinder replaced with original left in clauser ambier. Immal start obtained with original left in diffuser. Test terminated when target conficient achieved due to listed supply of nitrogen. conficient achieved due to listed supply of nitrogen.	Tumes config. Identical to run 20. Tumes start obtained when inlet spike cycled talces. Test cell pressure of 1.0 psie obtained. Vedge nozzle kes negligible effect on cell pressure.	First successful supersonic combustion run, intentional interustrat when first stage acquivalence ratio reached city. We second stage foul added, Or-Ing between the Outerbody and the coel leading adge extruded.	tunnel start and Inlat start obtained, $\varphi$ of 1.35 art at $P_{\rm P}$ $\varphi$ 150 pairs. Fecility functions and $\varphi$ i.40 set at $P_{\rm P}$ $\varphi$ 95 pairs. Fecility functionary value for injector 18 ostilisted. Ann proved All and tunnel can operate at $\varphi$ > 10. Erosion of zirconium diide coating on outer coat body crossover manifold noted. Erosion caused by carbon dust in turnel flow.	Test was aborted when engine inlet unstart was observed three seconds after inlitation of fuel injection. The angine unitart was result of injecting accessive fuel, caused by maffunction of facility control valve. Inspection of the unit revealed that the control raises in the second the was necessary.	First good run with design injector locations. Auto ignition obtained at 6 n.0.55; first stage did not light until sec ud stage fuel added. Overall 6 respect 0.0 with first stage held date 0.2%.	Tast aborted due to malfunction of the steam elector bystem	interborted when fuller unstated. Meditorition of the facility feel control valve mesolised in injector 2C. 3 small creeks in spite skin in region of spitors found in post tim impaction. Greeks repaired to prevent water thank into combiners.		TAFP	Fuel control problems encountered.	investigating performance improvement due to injecting fuel closers to inies, inies unstanted at overall 4 of .83.		Attempt to determine effect of first steps 6 and thrust on performers. Most taken to be considered to the steps of the ste		Effect of fuel split between 1st and second stage injectors at oversity in a 1st and second stage fuel added from innerbody side (system 2C). Fuel system purges turned to determine effect on combustor wall persure distribution. Found thrust messurement affected by thermal expansion of fuel manifold is, intel unserted at ownsit g of 1.0 with first Exacontered 6.0 Cavity onessure top PAZ repaired for this run. Exacontered fuel control problems.
	Objective of Test	Same as run 17 above				invastigate infet unstert limit with first stage combustion	Checkout AlM and fecility. Fuel rich at $F_{TD} = 750$ psia am 1.0 at $P_{TD} = 930$ psia	Checkout AlM and facility. Design im- jector locations	Demonstrate operation with design injector location and determine auto ignition limit	Determine effect of first stage @ on com- bustor performants	Determine effect of First stage & on com- bustor performance	Purge system calibration test	Combustor optimization	1-	Combustor optimization	Purge system calibration test, Evacuated test cell.	Combus tor optimization	Purga system calibration evacuated test cell	Combustor optimization
T	3 8								93		92		1	8	2		5		•
	Min Sec		•	•					-		•	·	1	-	1.	•	~	•	·
-	Hin Sec	×	9	Σ ·	3	ង	8	25	6		1.4			ž	~	•	ಕ	$\cdot$	
	\$ E	•	-	•	-	-	~	•	~	٠	•		$ \cdot $	~	-		_	•	•
	Config.	5	6	u			w		_	<b>.</b>	3	-	-	-	-	-	_	_	<b></b>
]	Injector	1A, 16	Fuel injec. not plenned	Fuel Injec. not plenned	Fuel injec. not planned	18, 28	и, 16.24. М	1A, 18, 2A, 2C	1A, 18, 2A, 2C	•	14, 18, 24, 20			1A, 19,2A,20	14,18,20,4		1A, 1B, 2A, 2C		
Inlet		 8.99			 8 8	 8.	6.00 4.00	. 0.98/ 8. 0.98/		 88.:3	00°7 /66°0			. 38	 8.3.		 8 8		
,	T 00 .0R	3100	2000	2000	2000		0006	9000	3000	900 1	3000		3000	8 8	3000		88		0006
Infet Condition	.o.	88	32	8%	8,	750	765/ 930	957	950	2,	750		8,	2 2	8%		750		750
[	No.	9	•	•	•	•	9	9	•	•	9		٠		•		<b>30</b>	•	9
	* *	3/22	4/27	g 3	g. }	₹.	5/15/73	8/36/73	42/5	5/30/73	5/30	,	10/4/73	10/5/73	10/10/73	01/01	U/11/01	46/61/01	8/7/11
	Reading No.	50	2	ā	z ·	a a	å	<b>\$</b>	y,	37	βť	gy naya 66	\$	3 5	×	. 8	15	55	95
Γ	ۇ چ	ő	5	2	=	z	2	*	22	2			11		82		62		2

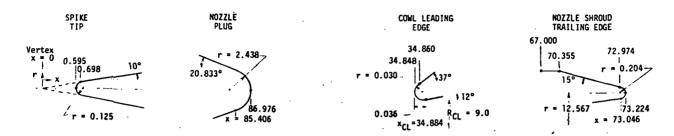
Table 2. - Continued.

	Pasding No.	Dec.	Fe Ch	Inlet Condition PTO: Pale	T <sub>T0</sub> . %	Inlet Spike Position,	Fuel Injectors Used	Tunnel Conf 19.	A P	15 2	Useful Min Sec	Objective of Test	Comments
2		11/2/13		750	3000			-	<u> -</u>	_	1	╀-	
		11/1/11			·	•	•	4	1			Purge system calibration	Determine effect of thermal expansion of fuel manifold 18,
2 S		11/8/73		2 2	8 8	8,8	1A, 18, 2A,	-	. ~	, 3	' ह	Combustor optimization	TARP Overall & held constant while amount of fuel from Innerbody and outerbody injectors varied. Fuel temperature com-
-5		87/81/11	•	85/	8001	0.99/ 1.72/ 2.52	1A, 18, 2A, 2C	_	-	8	2	Datemine effect of spike position on engine performance	possettom account of the second of 0.56 rea by verying the inlast spike position. All well pressure distribution measured with free line surge flow shut off, amounted section of the innerbody seasoly burned and damaged during combustion; damaged section of washing combustion; damaged sections
79		11/20/73	,	930/	3000			-		_	-	Performance test	1.46.9
63		11/21/73	٠	, 33 33	3000	8.8	1A, 18, 2A.		~	8	2 -	Performance test	Tunnel total pressure varied to determine effect of altitude on performance.
<b>3</b>		11/28/11	•	8%	0000	 8	18, 28, 26. 26, 38		_	93.	×	Subsonic-supersonic combestor made transition	Transition from subsonic to supersonic combustion mode demonstrated, inspection of unit reveals decolate was flowing the late the 18 fust amelicia on dutil travels decolate was flowing innerbody had bilstered. Separation at the spike skirt-spike body has progressed to approximately 1.0 inches. Former facing souterbody had progressed to approximately 1.0 inches. Governor facing successful and progressed to approximately to Ginches. Larger fuel matering venturi installed in fuel system E.
99		(1/11/31	•	8%	80	8.4	1A, 18, 2A.	-	-	×	3	Supersonic combustion with instrumentation rig	Instrumentation rake installed. Rake caused tunnel to unstart at a.m. 1.05. Etheust gas sampling date taken.
8	١٦	12/14			·	ŀ		_	•	1.	ŀ	Purge system calibration	TASP
		12/14	·	•	•				•	⊢	•	Purge system calibration	Purge system calibration My purge force calibration with cell evacuated.
9		12/14/73	۰	82	3000				-	-	<u> -</u>		Time of steady state fuel flow increased to 20 seconds to allow gas sampling date to stabilize.
ş		87/M1/21	•	<b>3</b> 7	300	8.4	1A, 18, 2A, 2C	y .	-	02	2 .	Supersonic combustion	One tunnel unstart experienced mear end of run. Several tunnel unstarts prevented by shutting off fuel. Inciplent unstart detected by monitoring luminescent normal shock position in I.V. view of tunnel.
R		2/19/73	•	8%	3000			u u	٠	•	•	Determine affacts of angle of attack	Test terminated premeturely due to frozen want velve.
_		12/19/73	٠	82.	3000	4.00	1A, 18.2A. 2C		٠	35	23		Coal leading adge assembly removed after this run to remove facing step noted after reading oh.
2												Purge system calibration	Calibration with 18 fuel Injector manifold heated test cell evecuated.
73.74.75		1/22/1	,	1000	3200		•		•	•	•	Mach 7 facility chack- out	Test aborted due to facility problems (TAFP)
ĸ		1/23/74	_	1000	3200			•	•		<u>.</u>	-	TAFP
"		1/23/74	7	9001	3200	2.57	,	•	~	,	<u> </u>	Mach 7 facility check-	Attempt to start tunnel at Nuch 7 unsuccessful. Secondary stample agents used; wedge rozzle pressure verled; inlet spike assembly telesiated.
R		1/25/74	,	1000	3500	1.57	•	u	~	-	-	Nach 2 facility check-	Tast aborted while attempting tunnel start. TAFP. Unusual amount of Carbon dust deposited on AIM.
2	T	3/15/76	_	1000	3100	•		5	-	-	ŀ	facility check-out	Ath moved aft 5.5 Inches.
8   ž		2/20/2	,,	98 9	300	2.57	22, 22	5 8	. ~	. 👳		Facility check-out	TAFP (dewer water system frozen). Blomout doors installed in tunnel closure. Tunnel sterted when
									• .	<u> </u>			wedge nozzle pressure reduced. Tunnel unstarted when combustor it. It. Batart not obtained due to change in wedge nozzle inlet pressure.
≈	- [	2/22/2	_	1000	3300		•	<b>C2</b>		Н	Н	Facility check-out	TAFP, Seel around outer coul body support demaged.
20 20	١,	1/22/2	1	900	3300	2.57		3	~			╁┤	1=1
87		2/28/74	1	2001	8 8		14 18 24	3		. 2			TAFP
	1						×	7	╗	g	-	racility chack-but	Tunnel nozzle started. Unstarted at Ø = 0.8

Table 2. - Concluded.

	Comments	First successful Mach 7 run. Tunnel clouwe removed. Diffuser seal repaired. Effect of fuel Injection location investigated. Rea 2 ignitors on. Outer coul body support demaged by carbon particles in tunnel flow due to failure of carbon part in facility heater. Shroud inlet pressure set hit and demaged. Spaired outer coul body support and mater cooled protective wedge installed. Coolent best at the interface of spike shirt and spike body noted at enquier location 270° in addition to leak at 180 degrees noted in Mag 64. Leak at 180° progressed to approximately 1.25 inches. Cool in leading adde tip radiison to leak as proximately 1.25 inches. Cool in leading adde tip radiison to leak spire long by perticles. Demaged areas remorted.	Performance measured with verious fuel injection schemes. Troveried during run. Injectors on. Test terminated prematurely due to failure of transducer in fuel control causing fuel control valve to fully open. Abnormal amount of carbon dust observed in turnel flow. Cowl leading edge tip radius and spike tip again damaged. Tip section repaired.	Second stage fuel injection closer to inlet (injectors IC, 4).	Tunnel start improved at angle of attack. Tunnel started at Pro v 850 psie. 3 Inlet unsterts encountered due to accessive 1st stage fuel. Total coolant leak into combustor estimated to be 5.0 gmm.	Instrumentation rake blockage had adverse effect on tunnel start. Inter spike stroked trucke to start tunnel. Oxygen content of tunnel flow veried while All exheust gas sampling date taken.	First Mach 5 run. Subsonic combustion data obtained, Run terminated prematurely (TAFP).	Subsonic and supersonic combustion and transition demonstrated. Four unsterts experienced, three unstarts attributed to high cell pressure, one to injecting excessive fuel intentionally into the AIM. More carbon in tunnel flow. Cord leading edge and spike tip demagned. Both remorked.	All comments made for Rdg 94 applicable for this run, except combustion was limited to supersonic combustion mode. Four angle unitaris experienced. Three unitaris were attributed to accility conditions and the other to programmed to determine inlet unitarit limit.	Subsonic and supersonic combustion and transition demonstrated at angle of attack. Intentional engine unstart obtained when excessive fuel was injected in supersonic combustion mode.	Combustor exit flow conditions surveyed. Cas sampling date taken, Blockage of instrumentation rake had advarse effect on tunnel operation.
	Objective of Test	Combustion evaluation	Combustor optimization	Combustor optimization	Effect of angle of attack	Combustor performance with instrumentation rake installed,	Facility check-out	Combustor optimization	Combustor optimization .	Evaluate effects of angle of attack	Combustor performance with instrumentation rake installed
	يّن	<u>.</u>	00	91	x	2		6	2		
Time	4		2	-	-	2	•	~	_		
٦	Min Sec	3	•	8.	25	8	88	×	3		
	Ē	~	•	•	2	^	۰	-			
	Tunnel Config.	<b>L</b>	<b>L</b>	ı							<b>I</b>
en en	Injectors Used	1A, 18, 2A, 2C	1A, 18, 2A, 2C, 4	1A.18.1C.	1A, 18, 2C,	1A. 18.2C.	1A, 18, 2A, 3A, 38	X X X X X X X X X X X X X X X X X X X	14, 18, 24, 26, 26, 26, 26, 26, 27, 20, 26, 27, 27, 27, 27, 27, 27, 27, 27, 27, 27	1A, 16, 2A, 3A, 30	2A, 3A, 5B
Inlet Spike	Ax, in.	25.2	2.57	75.57	2.57	15.5	0.4	8 8 8	8 9 9	8 88	0.4
	Tro. OR	3100	3000	3000	3000	2900	2210	3000	3000	2210 3000 2210	2210
Inlet Condition	P <sub>TO</sub> . Ps la	0001	1000	1000	0001	1000	\$15	(e) 415 (b) 300 (c) 206	300 4:5	÷ 88	/ <del>§</del> }₹
1	Nach No.		,	1		1	. 5	~	~	\$	~
	Pate 1 2	2/28	3/15/74	3/8/15	3/12/74	3/18/74	3/27/74	3/28/74	3/29/74	\$1./9	72/19
	Reading No.	88	89	86	91		93	\$	8	8	97
	5 0	æ	83	75	s	38	23	93	8	9	5
	ž ž	· ^		~	~			<u>'-'</u>		ــــــــــــــــــــــــــــــــــــــ	

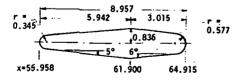
## Table 3. - AIM aerodynamic coordinates (Mach 6 cowl position, $x_{CL}$ = 34.844 in.)



#### a) Centerbody

x, in.	r, in.
0.595	0.0 90°
0.698	0.123\ st. line
18.360	3.237 10°
19.304	3.411
20.443	3.633
21.691	3.885
22.830	4.122
23.850	4.338
25.875	4.782
26.766	4.985
27.900	5.256
28.904	5.518
29.655	5.726
30.360	5.726 \ 15.819°
32.760	6.660
34.080	
37.710	7.140 8.607) 22.0°
38.070	8.734
38.538	8.874
38.826	8.942
39.132	9.000
39.780	9.096
40.500	9.180- 5.645° Throat
42.000	9.318
43.400	9.415
44.000	9.452
45.000	9.518
46.000	9.578
47.000	9.624
47.600	9.650
48.400	9.670
55.760	9.670 End of
55.760	9.406 spike; step )09
61.900	9.406 Thermal throat
65.740	9.406
67.553	9.072 \ 20.000
85.406	9.072 2.278) 20.833°
86.976	0.0 90°

## c) Internal struts (6)



## b) Outerbody

	b) outerbody
x, in.	r, in.
40.894 36.750 36.250 36.000 35.750 35.437	11.611 10.103 9.975 9.808 9.685 9.487 9.487
34.860 34.848 34.884 35.397 35.874 36.171 36.414 36.765 37.494 40.500	9.053
40.894 41.894 42.894 43.894 46.294 55.760 57.000 58.000	9.720 9.810 9.890 9.960 10.132 10.873 10.955 11.000 Internal
58.700 61.900 65.980 66.220 66.740 67.740 68.780 69.740	11.022 -Thermal 11.022 throat 11.042 11.132 11.348 11.572 11.773
70.820 71.660 72.260 72.920 72.980 73.046 73.224 72.974	11.989 12.146 12.249 12.349 12.357 12.365 12.567 90° 12.791 13.491 15° External
70.355 67.000	13. 493 \ 13. 493 \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \

### (d) Cowl lip design positions

	x <sub>CL</sub> . in.	Δx , in.	X <sub>CL</sub> /R <sub>CL</sub>
Close off	39, 150	0.0	4.350
Inlet start	38.160	0.990	4.240
Mach 8	36.990	2.160	4.110
Mach 7	36. 270	2.880	4.030
Mach 4 - 6	34.884	4.266	3.876

# Table 4. - HRE/AIM Instrumentation (obtained from ref. 5).

## (a) Coding for instrumentation list.

The code for the instrumentation listed in the "Identification" column is as follows: Sample, S-P-14.492-0 $^{\circ}$ 11'-90-3 (A-B-C-D-E-F).

"A" designates the component on which the instrumentation is located:

S = inlet spike assembly .

I = innerbody assembly

NP = nozzle plug assembly

CO = cowl leading edge assembly (outside)

C = cowl leading edge assembly (combustor side)

0 = outerbody

N = nozzle shroud (combustor side)

NO = nozzle shroud (outside)

CE = combustor exit

EF = engine airflow-metering duct

F = fluids

"8" designates type of instrumentation

P = pressure

T = temperature

"C" designates the location of the instrumentation in terms of station, with the inlet spike assembly positioned for testing at Mach 6 condition.

"D" designates the angular location in degrees and minutes.

"E" designates position of the pressure pickup with respect to airflow in degrees, or, if the instrument is a temperature sensor, it designates the thermocouple:

CA = chromel alumel

CuC = copper constantan

P/rh = platinum-platinum/rhodium

"F" designates the leg through which the leads are brought out.

An "X" anywhere in the Identification Code indicates that the parameter was not applicable.

xxx/yy in the "Reading No." column indicates the Channel No. (xxx) on which the parameter was recorded, and the rated capacity (yy) of the transducer used.

The "N/U" Code in the "Reading No." Column indicates channels that were not used.

"LeRC Sys" - recorded on separate system, therefore no channel number.

Table 4. - Continued.

(b) Instrumentation list.

٢	5		_		_			_	-	_	_	-	_		_	_	_	-	_		-	-	_	_	_	-	_	_	_	_	_			_	_	_	_	_				-			-		_	_	_	_		_			-	-	_	Ě
	⊢	+	4	-	_	_			_	_	_	_	_	1	_	L	_		L	_			-	L	_	_	_	-	L	_	_	1		4	_	ŀ	_			_	1	_	1	1	1	1	1	_	_	_	_	_			_	_	_	I
	ľ			_	_	_		_	_		_	_	_	4	إ	_	_	_	_		_		إ	_	_	_	_	إ	Ĺ	_		ļ	_	<u>ا</u>	_	_	_	_	_	_	Ļ	_	5	<u>~</u>	<u>~</u>	7	1	_	_	_		_	_	_		_	_	
	٤	_						_	_	_	_			1	138/16	-	_	7133715	<u> </u>		_	_	36/961	}	_		_	110/16	Ì	_	_	ļ		-		<u> </u>	_				L	-	2007	2	<u> </u>	<u> </u>	3	_				_		_	_		_	ĺ
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178   556 - 355 - 667   178		A720 - 40.5 - 178 - (	7 7 3	376/15	H	1		H	H	H	H	H	H	$\prod$			H	Ц				H				• (
A   1   1   1   1   1   1   1   1   1		01 V - 66.2 - 356 - 1	[6-JAJ		+	†	†	$\dagger$	+	+	+	+	+	+	4	T	Į L	4						H	H	1 4
		ATV - 66, 19 - 176 -			H	H	H	H	+	H	+	$\downarrow$	$\perp$	$\downarrow$	-	<u>₹</u>	1	$\downarrow$			T	†	†	$\dagger$	+	
1744 - 15. 35		ATM - 55.6 - 175 - (	773	MOVOTS.	H	$\ $	H	H	H	H	H	H	H	H	Ц	Ì		$\prod$				T	T	t	$\dagger$	
ATH. 72.55 176 Cut-1		4744 - 72.36 - 356 -	71	381/075	+	†	+	+	$\dagger$	+	+	+	+	+	Ť		1					<del> </del>  -	$\parallel$	+	H	
2146 - 66.68 - 176 - Cuc → 1		ATM - 72. % - 176 -	77		H	$\ $	H	H	H	H	H	$\prod$	H	$\prod$	<u>Ř</u>		H	Ц		Π	T	T	†	t	+	
	- 1	AT46 - 66.68 - 176 -	7 3		+	†	+	+	$\dashv$	+	+	+	$ \downarrow $	$\perp$			H	Ц					H	H	Н	1 (

Table 4. - Continued.

(b) Continued

	6	1	1	L	L	1	1	•	1	4	Ľ	L	1	•	1	' '	L	1			_			1		1	1			_					_							_	_	
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	8	Ī	Ī				Ī	Ī					Ì	Ì				Ī				į				ĺ				_	•													
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	69	<u> </u>	ĺ	Ī				Î	1	-	1		3//2	1	185/5mv	7	Į.	- AS/29K							•	T	İ		_		_		-		_	_		_	-				_	
<b>e</b> .	2	T	t	l	<u> </u>	f	-	$\dagger$	+	1	•	1	Î	Î	1		Ì	Î	_			_		1			t	_	-		_			_	_	_	-							
READING NUMBER	3	+	t	-	-	-	1	+	+	1		l		1				†		_	_			†		t	t		_						-	_	-	_	_					
READIN	5	t	$\dagger$	-	-	-	<del> </del>	+	1	1		-		1	+		-	+						$\dagger$		1	+					_			_	-	-					_		
	5	-	$\dagger$	ŀ	-	-	-	ł	1	+		L	-	$\dagger$	1		ŀ	+						+	-	-	+		-		_							_			_	_		-
	2	t	+	-	-	H	-	1	-					1	+		L	+			_		_	+	_	+		_	_		_	_	_			_	_	_	_	_	_	_	_	-
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	až	+	-	H	L			1	-	<u> </u>		ŀ	-		1		H	+						+		<u>~</u>	+	_			_	_		_	_									_
	,	H		L	-	L	$\mid$	1		-	_	L	-	+			L	$\dagger$		_				+		+	+		_		_	_	_			_	_	_	_	_	_		_	
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	├	$\vdash$	-	L	H	L	-		-	+	-	_	-	ļ	+	4	L	7		- !	Visually Monitored	_	H	+		1	+	_	_	_	~-	-			_		_	_	_		_	_	i	4
	F	+	- <u>}</u>	_	Ì	_	- }	[-	_	Ě	_	Ì	-	-	į	_	į	-	_	- <u>'</u>	<u>.</u>	۰	L	1	_	L	Ž.	_	_	•		7	7	1	-	-	_	_	_				=	H
_	<u>۽</u>	L	383/ATSmv	_	384/15m		18t / 15m		-	306/675mv	_	387/ATS.		1000	200		180/1/2				=	*		39./5	-	ž	22	<u> </u>	25/2	258/5	69/5	3	300	ž			?	₹	₹	₹	?	2	21/50	73/51
	Identification		ATS 40.0 - 4 - CuC-3 (	35 - 4/.08 - 35/ - cut-31	7-10-10-10-1	5K - 47.54 - 181 - CuC-47	SM - 50.8 - 358 - CuC-3 (	St - 48.58 - 357 - Cuc-31	4 - 40.8 - 178 - Cut-4 -	1 to ca		16-101 - 000 - 01-00	74 - So.8 - 35t - Cuc-3 -	7P - 66.10 - 176 - CuC-41	74 - 50.8 - 174 - CuC-ts 7	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	) - Y - W - 12 - 19	) -Y- X - NI O H - LY-0		7 - 4 - 10 Oct - 4 - 5 -	P - H_O IN - X - X-4	~	1 - 4 0 - 52.6 - 27 - 04.3	T - H.O - 57.8 - 30 - CA-4	7	PINCE CAVITY PA-1-X - X - X-3	RGE CAVITY PA-2-X - X - X-3	PURGE CAVITY PB-1-X - X - X-3	46E CAVITY P8-2-X - X - X-3	NER BOOY CAV PRES - X - X-4	WER BOOF CAV 1EMP - X-X-CA-	PURGE CAVITY TAI - X - X - CA-	CAVITY TAS .	CAVITY TRE	1							AGE CAVITY	PURGE CAVITY	MGE CAVITY
-Possure-	Mumbe r		7-6															-0			4-0 5-29		1-10					2-6		_	_						2	**	97-6	3-96-			2	

Table 4. - Concluded.

(b) Concluded

| 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 | 1967/15 |

155/75 156/50 156/50 166/75 161/50 161/50 161/50 161/50 161/50 161/50 17

34

Number

Table 5. - Summary of HRE/AIM test points used for analyses.

(a) Mach 6 component integration results.

*		1	т—	T-		T _	_				<del>,</del>	<u>,                                      </u>	,		<del></del>
Page No.	Reading Number	Time	Но	P	To' sia	T <sub>T</sub> OR		K <sub>CL</sub> , in.	α	Inj.1/ø <sub>1</sub>	Inj.2/\$ <sub>2</sub>	Inj.3/ø <sub>3</sub>	φ <sub>τ</sub>	ignitors 1, 2, 3	Purpose & Remarks
-	33**	126.95	6.0		750	300	00	35.2	o°	0	0	0	0	No	No fuel injection
	1	161.15	T	+	Ť		十	T	1	1A,18/.24	0	0	0.24	1,2	ist stage only
		168.0	T	+	†	$\vdash$ †	7	1	11	1A,18/.3	0	0 .	0.30	1	1st stage only
	•	174.65		╅	+	1	$\top$	+	1	1A,1B/.36	0	0	0.36		Max. Ø, engine unstart
57	34	98.15	6.0	$\mp$	750	300	<u></u>	35.2	00	0	0	0	0	1,2	
65	<del>-                                    </del>	104.45	ŤŤ	+	Ť	Ť	+	1	Ť	1A,1B/.20		0	0.20	<del>l í</del>	1st stage only
73		148.55	T	+-	+	T	十	+	H	1A,1B/.23		0	0.81		1st and 2nd stages
81	<del></del>	181.85	$\vdash$	+	+	1 1	十	+	H	<del></del>	2A/.56	3A/.39	1.16	<del>                                     </del>	Max. Ø, 3 stages
89	•	196.25		+	940	1	十	+	1	1A,1B/.15		3A/. 32	0.91	<del>                                     </del>	Max. φ, 3 stages
	36 a	119.18	6.0	$\perp$			<u></u>		-0						
	36 a	124.58	18.0	╫	750 T	300	4	35.2	00	0 .	0	0	0	No	Auto ignition
97	-   a	132.68	++	+-	+-	-	+	+	H	1A,18/.26		<del></del>	0.26	├	
97	<del>                                     </del>	144.38	╁┼	+	+	┥	+	+	H	<del></del>	2A,2C/.34	0	0.59	├-┼-	
106		158.78	╁┼	+	+	H	+	+-	╁	<del>                                     </del>	2A,2C/.49 2A,2C/.69	0	0.73	<del>                                     </del>	<del>                                     </del>
124	-	173.18	╁	+-	+	1	+	╁╴	H	<u> </u>	2A,2C/.75	0	0.92	<del>                                     </del>	
				$\pm$		_	$\pm$								
133	38	96.24	6.0	4	750	300	<u> </u>	35.2	l oo	0	0	0	0	No	
141	ļ	107.05	$\sqcup$	+	1	$\sqcup$	4	4_	Ц	1A,1B/.33	0	0	0.33	<del>                                     </del>	1st stage only
150		113.35	$\sqcup$	4	╀	$\sqcup$	4	↓_	Н	0	2C/.38	0	0.38	<del>                                     </del>	2nd stage only transies
158		116.95	- 1	+-	1	. ₹	+	<u> </u>	1	1A,1B/.18	20/.67		0.85	<b>_</b>	<u>data</u> ر
167	52	165.93	6.0	1	750	300	0	35.2	00	0	0	0	0	No	Ø1A,18 and Ø4,2C
175	1	172.23			$\mathbf{I}$	П	T		П	1A,1B/.24	4,2C/.26	0	0.50		
183		180.33			$\mathbf{L}$				$\coprod$	14,18/.20	4,20/.41	0	0.61	<u> </u>	
191	*	189.33	1	$oxed{\Box}$	Ţ		$\perp$	T	I	1A,18/.20	4,20/.53	0	0.73	•	
199	54	156.46	6.0	+	750	300	<del>,</del>	35.2	00	0	0	0	<del>                                     </del>	No	Constant Ø1A,18, Ø2A,2C
207		185.26	1	+	Ť	1	+	T	T	1A,18/.21	2A,2C/.64	0	0.85		ramped up 3 times
215		200.56		+	+		十	+	H	<del> </del>	2A,2C/.43	0	0.66		
223		222.16	† †	+	+-		十	+	11	<del></del>	2A,2C/.25	0	0.49	<del>-   -   -   -   -   -   -   -   -   -  </del>	
23/	<del>                                     </del>	235.66	t	+	十		十	+	††	1A,18/.24	2A,2C/.52	0	0.76		
239		253.66	T	+	+		1	1	Ħ	1A,1B/.18	2A,2C/.60	0	0.78	1.2	· ·
247	•	280.66		$\top$	+	•	T	+	1	1A,1B/.20	2A,2C/.61	0	0.81	No	
255	57	195.11	6.0	Τ.	750	300	7	35.2	00	0	0	0 ·	0	No	Optimized performance
263	- "	207.71	10.0	┰	<del>/}</del>	700	<del>* </del> -	T	Ť		2A,2C/.73	0	0.94	Ť	operative per formance
27/	<del>}                                    </del>	234.71	╁┼	+	╁	$\vdash$	╅	╁╌	₩	<del></del>	2A,2C/.60	0	0.92		
279	<del>                                     </del>	265.31	1	+	╁	$\vdash$	+	+	╁┼	1A,18/.21	2A,2C/.36	0	0.57	<del>-   -</del>	
287	<del>                                     </del>	287.81	┤┪	+	╁	1	+	+	╁	<del></del>	2A,2C/.54	0	0.74		
				#	_		#		- 6						
295	60	155.69	6.0	4-	750	300	٠.	35.2	100		0	0	0 00	No	Variation of fuel schedule
303		178.19	╁╌╂	+	+-	$\vdash$	+	╀	H	<b>.</b>	2A,2C/.64		0.85		
311	<del>                                     </del>	186.29	╁┼	+	4	$\vdash \vdash$	+	+	H	<u> </u>	2A,2C/.65		0.87		<b></b>
313	$\vdash$	202.49	₩	+	+	⊢┼	+	+	H		2A,2C/.65		0.86	$\vdash$	<del></del>
327	<del>                                     </del>	223.19	ℍ	+	╁	┝╶┼	+	+-	₩	1A/.21	2A,2C/.66		0.87		· · ·
335	$\vdash$	230.39	┤┤	+-	+-	┝┼	+	╁	₩	<del></del>	2A,2C/.67			<del>                                     </del>	
343	<del>                                     </del>	241.19	╁┼	+	+	┥	+	+	₩	18/.19	2A,2C/.68	$\overline{}$	0.87	<del>      -  </del>	
35/	<del>  </del>	249.29	╌┼	+	+-	╁╌╂	+	+	₩	18/.24	2A,2C/.68	$\overline{}$	0.92	<del>     </del>	
359	<del> </del>	258.29	╁┼	+	+	┝╌╂	+	+	₩	0	2A,2C/.76		0.76	<del>                                     </del>	<u> </u>
367		264.59	<u>Lŧ</u>	丄	<u> </u>	<u> </u>	Ц.	1	LŁ	0 .	2A,2C/.80	V	0.80		

<sup>\*</sup>Reference 10
\*\* Because of insufficient valid engine surface pressure measurements, performance results were not obtained.

a Listings not available.

Table 5. - Continued.

### (b) Mach 6 engine performance results.

Number   Time   To   pasia   Na   Na   Na   Na   Na   Na   Na																
### 61 178.86 6.0 750 3000 36.7 0° 0 0 0 0 0 0 No Effect of spike position 6.3 198.66	Page .			M <sub>o</sub>	P.	T <sub>o</sub> '	P <sub>T</sub>	•		a	Inj.1/ø <sub>1</sub>	Inj.2/ø <sub>2</sub>	inj.3/ø <sub>3</sub>	Ø <sub>T</sub>	Ignitors	Purpose & Remarks
198.66		61	178.86	6.0	+		3000	╗┤	36.7	00	0	0	-	0	<u> </u>	Effect of spike position
12, 18			198.66	$\top$	1	Т		7	Ť	T	1A.18/.13	2A.2C/.36	0	0.49	<del>                                     </del>	
1			205.86	1 1	+	t	t	+	_	††	+	<del>+</del>		+	<del>                                     </del>	<del>                                     </del>
20			212.16	11	1	T	1-1	+	_	11	+	<del></del>	+	+	1-1-	<del>  -                                   </del>
108			222.06	† †	+	┢	-	+	+	1 1	<del></del>			-	<del>                                     </del>	
108	-		231.06	11	1			+	37.5	00	1 - : : -	<del> </del>	<del></del>	<del></del>	No	Effect of spike position
17			<del></del>	11	+-	1		+	1	1	<del>+</del>	0	<del> </del>	<del>-</del>	<del>                                     </del>	
126			<del></del>	† †	†	<del>                                     </del>	1	+	+	††	<del>+</del>	<del></del>	<del></del>	+	<del>                                     </del>	<del>                                     </del>
135			<del></del>	11	+	1		7	+	Ħ	<del></del>	+	<del></del>	+	<del>                                     </del>	†
14		<del>                                     </del>		1 1	+	1	-	╅	+	╫	<del></del>	<del></del>	<del></del>	+	<del>                                     </del>	<del>    </del>
153   5   186.15   6.0   930   3000   35.2   0° 0   0   0   0   0   0   No   Effect of altitude     164		•	<del></del>	1 1	1			7	+	1	<del>}</del>		<del></del>	_	1 1 1	, -
161					1	_		1		Ľ	1		<u> </u>		1	·
169		63	<del></del>	6.0	93	30	3000	٥	35.2	00	<del> </del>	ļ <u>.</u>	<del></del>	L	No	Effect of altitude
177			<del></del>	$\sqcup$	$\bot$	L	$\sqcup$	4	4-	11	<del></del>	<del></del>	<del>+</del>	+	<del>                                     </del>	<b></b>
185		<b></b>	216.75	$\sqcup \bot$	╁ '	♥	$\vdash \bot$	4	4	Ш	<del></del>	<del></del>		+	<b> </b>	ļ
193   64   156.11   6.0   750   3000   35.2   0°   0   0   0   0   0   No   Subsonic-supersonic     207				$\sqcup \bot$	<del></del>			$\perp$		Ц	L	<del></del>	0	0	<u>                                   </u>	
201 167.81	185		275.25	1	47	70		4	<u> </u>	1	1A,18/.26	2A,2C/.73	0	0.99	<u> </u>	<u> </u>
201   167.81	193	64	156.11	6.0	75	50	3000	,	35.2	00	0	0	10	0	No	Subsoni c-supersoni c
209	_		167.81			Г		†	T	Т	18/.24	2A,2C/.77	0	1.01	1-7-	<del> </del>
217			202.01	<del>                                      </del>	+	1		†	+-	11	0	<del></del>	3A.38/.85	0.85	<del>††</del>	<del>                                     </del>
18/.24   0   3A,38/.8   1.04			239.81	11	+-	Н		+	+-	H	18/.23	2A.2C/1J1	<del></del>	<del>                                     </del>	<del>                                     </del>	<del>                                     </del>
18/.26   2A,2C/.8   0   1.06				1	+	Н	$\vdash$	+	+-	11	<del></del>		3A.38/.8	<del></del>	<del>                                     </del>	<del>                                     </del>
241 65 164.03 6.0 750 3000 35.2 00 0 0 0 0 0 No Supersonic combustion 12.49   174.83   1		-	<del></del>	1	+-,	-	1	+	+	1	<del></del>	<del> </del>	<del></del>	<del>                                     </del>		
174.83		65		6.0	7,5		3000	,	35.2	00			0		No	Supersonic combustion
180.23		Ī	<del></del>		+		Ť	+	T	T	1A.1B/.23	0	0	0.23	<del>                                     </del>	<del></del>
196.43				╅	+-	Н		$\dagger$	+-	H	<del></del>	2A.2C/.34	0	<del></del>		<del> </del>
273				1	╅─	Н	-	+	+-	1		<del></del>	0	<del></del>		
18.03			<u> </u>	╁┼	+	H	$\vdash$	+	+-	H			<del>↓</del>	<del>-</del>	<del>                                     </del>	
297 69 177.00 6.0 750 3000 35.2 0° 0 0 0 0 0 No Supersonic combustion 305 198.60 1 1A,18/.22 0 0 0 0.22 with instrumentation rig 313 212.10 1 1A,18/.23 2A,2C/.48 0 0.48 gas sampling 321 226.50 1 1A,18/.23 2A,2C/.59 0 0.82 322 256.20 1 1A,18/.23 2A,2C/.59 0 0.82 3337 265.20 1 1A,18/.23 2A,2C/.79 0 1.02 345 71 160.54 6.0 750 3000 35.2 3° 0 0 0 0 0 No Angle of attack perform 353 171.39 1 1A,18/.22 2A,2C/.31 0 0.53 366 174.94 1 1A,18/.22 2A,2C/.59 0 0.83 377 207.34 1 1A,18/.24 2A,2C/.59 0 0.83 377 207.34 1 1A,18/.24 2A,2C/.59 0 0.83 377 207.34 1 1A,18/.24 2A,2C/.59 0 0.83 377 207.34 1 1A,18/.24 2A,2C/.59 0 0.83 377 207.34 1 1A,18/.24 2A,2C/.59 0 0.83 378 207.34 1 1A,18/.24 2A,2C/.59 0 0.83 379 207.34 1 1A,18/.24 2A,2C/.59 0 0.83 389 2066.74 1 0 2A,2C/.33 0 1.33 399 2066.74 1 0 0 2A,2C/.37 0 0.87				╀	+	Н		+	+-	╁			<del></del>		$\vdash$	<del></del>
297 69 177.00 6.0 750 3000 35.2 0° 0 0 0 0 0 0 No Supersonic combustion  305 198.60			<u> </u>	╂	+ ,	$\vdash$	1	+	+-	╁	<b>└</b> ───	<del></del>	<del></del>	<u> </u>	<del>                                     </del>	<u> </u>
198.60					#=			#								
212.10		69		6.0	75	0	3000	4	35.2	00	L				No	
321 226.50			<u> </u>	<del>                                     </del>	1	Ш	$\vdash \downarrow$	4	4	₩	<u> </u>	<del></del>	<del></del>			<del></del>
256.20					4	Ш	$\vdash$	4	$\bot$	Н					<del></del>	gas sampling
345 71 160.54 6.0 750 3000 35.2 3° 0 0 0 0 0 No Angle of attack performance 171.39 1 1A,18/.22 0 0 0 0.22 ance 361 174.94 1 1A,18/.22 2A,2C/.31 0 0.53 1 1A,18/.22 2A,2C/.59 0 0.83 1 1A,18/.24 2A,2C/.59 0 0.83 1 1A,18/.24 2A,2C/.81 0 1.05 1 1A,18/.24 2A,2C/.81 0 1.05 1 1A,18/.24 2A,2C/.33 0 1.33 1 1A,18/.24 2A,2C/.33 0 1.33 1 1A,18/.24 2A,2C/.87 0 0.87 1 1A,18/.24 2A,2C/.87 1 1A,18	32/			$\vdash \vdash$	1	Ш	1	4	┷	$\sqcup$			·		<b></b>	<b></b> _
345 71 160.54 6.0 750 3000 35.2 30 0 0 0 0 No Angle of attack performance				$\sqcup$	4-4	Ш		4	4	Ш			<del></del>	<u> </u>	<b>——</b>	
171.39	337		265.20		┦┛	Ц		+	•	1	1A,18/.23	2A,2C/.79	0	1.02		<u>+</u>
36/     174.94     114.18/.22     2A,2C/.31     0     0.53       36/9     193.84     114.18/.24     2A,2C/.59     0     0.83       37/9     207.34     114.18/.24     2A,2C/.81     0     1.05       38/5     248.74     0     2A,2C/1.33     0     1.33       39/3     266.74     0     2A,2C/.87     0     0.87       40/1     270.34     0     2A,2C/.87     0     0.87	345	71	160.54	6.0	75	0	3000	1	35.2	30					No	Angle of attack perform-
369     193.84     1A,18/.24     2A,2c/.59     0     0.83       377     207.34     1A,18/.24     2A,2c/.81     0     1.05       385     248.74     0     2A,2c/.83     0     1.33       393     266.74     0     2A,2c/.87     0     0.87       401     270.34     0     2A,2c/.87     0     0.87				$\Box$		Ш		$\perp$	$\perp$	Ш			ļ	-		ance
377     207.34     1A,18/.24     2A,2C/.81     0     1.05       385     248.74     0     2A,2C/1.33     0     1.33       393     266.74     0     2A,2C/.87     0     0.87       401     270.34     0     2A,2C/.87     0     0.87			174.94	$\sqcup$		Ш		$\perp$		Ш						
385 248.74 0 2A,2C/1.33 0 1.33 393 266.74 0 2A,2C/.87 0 0.87 0 0.87 0 2A,2C/.87 0 0.87	369		193.84	LL.		$\sqcup$	$\perp$	$\perp$						0.83		
385     248.74     0     2A,2C/1.33     0     1.33       393     266.74     0     2A,2C/.87     0     0.87       401     270.34     0     2A,2C/.87     0     0.87	377		207.34					floor		$\coprod$	14,18/.24					
FOI 270.34 0 2A,2C/.87 0 0.87			248.74					Ι		$\Box$	0	2A,2C/1.33	0	1.33		
<del></del>			266.74				$_{\perp}\Gamma$	Ι			0	2A,2C/.87	0	0.87		
			270.34		П		$\Box$	T			0	2A,2C/.87	0	0.87		
	-09		284.74		П	Π		T	П		O.	2A,2C/.66	0 .	0.66		
17 285.64 0 2A,2C/.66 0 0.66		-	285.64			$\Box$		T	T	1	0	2A,2C/.66	0	0.66		

<sup>\*</sup>Reference 11

Table 5. - Continued.

### (c) Mach 7 component integration and engine performance results.

, a						٦		P		т—	<del></del>				Γ	Τ	<del></del> -
Page*		ding ber	Time	H	ا ،	P <sub>T</sub>	o ia	PT,	in.		(nj.1/ø <sub>1</sub>	inj.2/ø <sub>2</sub>	inj.3/ø <sub>3</sub>	ø <sub>T</sub>	ignitors	Purpose	& Remarks
54	_	38	236.40	7.	25	10	90	3160	36.6	00	0	0	0	0	. 2	Exploratory	run
62			245.40		Π		П	3170	T	┢	1A,18/.30	0	0	0.30			T
70			261.60				П	3250			1A,1B/.42	0	0	0.42			
78			269.70	Г	П	Г	П	3280			1A,18/.55	0	0	0.55			
86			270.60	Г	П			3270		$\Box$	1A,1B/.57	0	0	0.57			
94			271.50					3270			1A,18/.58	0	0	0.58			
102			278.70		Π			3270			14,4/.16	2A,2C/.70	0	0.:86			
111			285.90					3250			14,4/.31	2A,2C/.60	0	0.91			
120			294.00		Г			3200			14,4/.28	2A,2C/.57	0	0.85		•	
129			299.40		Ш			3150	$\perp \perp$		14,4/.45	2A,2C/.46	0	0.91			
138		니	305.70	Ľ	•_	L	Щ	3090		<u> </u>	14,4/.49	2A,2C/.41	0	0.90			<u> </u>
147	-	39	250.77	7.	4	10	00	1790	36.6	00	0	0	0	0	No	Effect of 1	ow T <sub>TO</sub>
155			272.37	7.	25			3180			1A,18/.32	2A,2C/.47	0	0.79	2		
164			283.17		$\Box$			3270			1A,1B/-34	2A,2C/.55	0	0.89			
173			290.37					3270			0	2A,2C/.75	0	0.75			
181			294.87					3310			0	2A,2C/.92	0	0.92			
189			304.77	L	Ц		$\square$	3290			0	2A,2C/.59	0	0.59	<u> </u>		
197		$\sqcup$	310.17	L	Ł	Ш	Ц	3060		<u> </u>	1A,1B/.32	2A,2C/.57	0	0.89			
206, 232		**	316.47	7:	_		Ц	2720	$\perp$	<u> </u>	1A,1B/.29		0	0.83			
215,241		**	327.27	7.		Ц	Н	2410	4		1A,1B/.28		0	0.82		<b> </b>	
224		<b>Y</b>	352.47	7.	25	Н	Ц	3300	_	├—	1A,18/.36	2A,2C/.57	0	0.93		<u> </u>	L
249	9	90	197.22	7.	25	10	00	3000	36.6	o°	0	0	0	0	No	Optimization	n
257		1	206.22	L							1A,18/.48		0	0.48	2	<u> </u>	
265			212.52	L	$oxed{L}$						1A,1B/.49		0	0.54			
273			217.02	L	L	L	Ц	$\Box$			14,18/.48		0	0.82		L	
281		<u> </u>	230.52	L	L				Ш	_	14,18/.26	L	0	0.77	<u> </u>	<b></b>	
289			235.02	L	$\perp$	<u> </u>	$\sqcup$			_	1A,18/.79	10,4/1.19	0	1.98		Inlet u	nstarted
2.97	_	1	246.72	L	┖	_	ļ.,	$\sqcup \! \perp$	$\perp$	<b> </b>	14/.51	0	0	0.51		<b>}</b>	ļ. <del></del>
305			247.62		<u>t</u> .	Ľ	•	1	1	-	1A/.55	0	0	0.55			
313		91	175.65	7.	25	10	000	3100	36.6	3°	1A,18/.39	0	0	0.39	2	Angle of at	tack
321		$\Box$	180.15					$\Box\Box$	$\sqcup \mathbb{L}$		1A,18/.47	0	0	0.47	2		
329	L	$\Box$	186.45	L	$\perp$	ـــ	$\perp$	$\sqcup \sqcup$	$\sqcup \bot$	<b>L</b>	0	0	0	0	No		
337	L	$\sqcup$	190.05	L	$\perp$	<u> </u>	L,	$\sqcup \sqcup$	<del>                                     </del>		14,18/.51	4/.13	0	0.64	2		
345	L_	$\sqcup$	203.55	L		<u> </u>	$\Box$	$\sqcup \sqcup$	$oxed{oxed}$	L_	1A,1B/.52	0	0	0.52	$\vdash \vdash$	ļ	
353	-	$\vdash$	216.15	$\vdash$	₽-	⊢	$\vdash$	$\vdash \vdash \vdash$	⊢-	$\vdash$	18/.27	4,2C/.34	0	0.61	├┼	· ·	
361	├	$\vdash$	224.25	<b> </b> -	$\vdash$	₩-	H	HH	-	├	18/.28	4,20/.50	0.	0.78	<del>  </del>	<b> </b>	
369	-	1-	226.95	$\vdash$	$\vdash$		$\vdash$	$\vdash \!$		<del> </del>	18/.28	4,20/.45	0	0.73	<del>                                     </del>	<del>                                     </del>	<del> </del>
377 385	├	<u>.                                    </u>	229.65	<del> -</del>	L	<del> </del>	L	┝╁┤	<del>-                                    </del>	$\vdash$	18/.33	4,2C/.39 2C/.41	0	0.72	<del>-                                    </del>	<del> </del>	<del></del>
		$\preceq$	235.95	<u>_</u>	_	벋	4				18/.29						
393		92	186.87	-	_	10	00	_	36.6	00	0	0	0	0	No	Supersonic with instru	combustion mentation rig,
401	<u> </u>	$oldsymbol{ol}}}}}}}}}}}}}}}}}}$	205.77	7.	29		Ц	2850	$\perp$	L_	1A,18/.48		0	0.72	2	gas samplin	g and O2
409	L_	1_	227.37	L		_	Ц			_	1A,1B/.50		0	0.93		content eff	ect
417	$\vdash$	+	248.07	Ŀ	<u> </u>	<u> </u>	Н	12000	4	<u> </u>	18/.33	4,20/.58	0	0.91	<del>                                     </del>	<u> </u>	
425	<b> </b>	╁┈┤	290.37	7.			Н	3000		_	1A,1b/.47	4,20/.55	0	0.85	<del></del>	<b> </b>	
433	ட	<b>Y</b>	312.87	<u> </u>	25	L		3000	_±_	<u> </u>	1A,1B/.36	4,2C/.49	لــــــــــــــــــــــــــــــــــــــ	0.05		<u> </u>	<b>!</b>

<sup>\*</sup>Reference 12

<sup>\*\*</sup> Recomputations were made with surface pressure substitutions

Table 5. - Continued.

(d) Mach 5 component integration and engine performance results.

Page*		nding nber	Time	н,		T <sub>o</sub> '	P <sub>T</sub> OR		CL'	·	inj.1/ø <sub>1</sub>	Inj.2/ø <sub>2</sub>	Inj.3/ø <sub>3</sub>	o <sub>T</sub>	igni 1	tors	Purpose &	Remarks	3
54	9	93	134.03	5.1	4	20	210	0 3	5.2	00	0	0	0	0	No		'No fuel injecti	on	1
62		i	142.13	Т	1	Τ	Т	Ť	Τ		0	2A/.29	0	0.29	2		2nd stage only	_	1
70			150.23	$\sqcap$	1	Т	П	$\top$	T	T	0	2A/.31	3A,38/.25	<del></del>			Subsonic combu	stion	1
78			158.33	T	$\top$	1		$\top$	†		0	0	3A,38/.60				and 0, content		1
86			162.83	$\Box$	1	T			$\top$		0	0	3A,38/.71	0.71					1
94			174.53	П	T	Г		$\top$	1		0	0	3A,3B/.49	0.49					1
102			182.63	Į	工	┖			ŧ		0	0	3A,38/.35	0.35	•				1
110	9	4	134.14	5.1	+	20	2230	1 3	5.2	00	0	0	0	0	No	<u> </u>	Subsonic combus	tion.	-
118		<u></u>	140.44	1	+	Ī	T	1	Ť	۳	0	2A/.49	0	0.49	2	,	Subsonie Combas		┨
126			150.34	╁	+	$\vdash$	╁	十	╁	$\vdash$	0	2A/.49	3A,38/.47	0.96	1				1
134	$\vdash$	$\vdash$	157.54	$\vdash \vdash$	+-		-	+	+	$\vdash$	0	0	3A,38/1.03	<del></del>	$\vdash$	•	<del> </del>		1
142	$\vdash$		163.84	┝╌╂	十	H	$\vdash$	+	十	$\vdash$	0	10	3A,38/1.19	+			<del></del>		1
150			180.04	$\vdash \vdash$	T	Н	$\vdash$	†	$\dagger$		0	0	3A,3B/.19	<del></del>			<del>                                     </del>		1
158			214.24	-	1	00	2940	,	十	<del> </del>	0	2A/.53	0	0.53		_	Effect of T <sub>TO</sub>		1
166	-		215.14	╁	+		1	+	╀	<del> </del>	0	2A/.53	0	0.53	$\vdash$	+			١.
174	$\vdash$	$\vdash$	218.74	$\vdash$	+	Н	+	+-	+	٠	0	2A/.54	3A,38/.5	1.04		$\neg f$	High test		
183			231.34	$\vdash \vdash$	+-	╆╢	-+	+-	+	$\vdash$	1A,18/.15	<del></del>	0	0.15	<del>                                     </del>	_	AIM nozz.	pressu	res
191	$\vdash$		233.14	$\vdash$	T	Н	-	╁	T	$\vdash$	1A,18/.25	<del> </del>	0	0.25					1
199	1		234.04	+	1			1	+	М	1A,18/.27	<del></del>	0	0.27					1
	_				Τ,		21.24	1	_	o°		L							7
207	9	•	129.55	5.2	1-3	00	2430	1.	. 2	0	0	0	0	0	No.	•	Supersonic comb	oust: on	4
215			140.35	5.1	+	$\vdash$	3080	-	$\vdash$	<u> </u>	1A,18/.16	<del></del>	0	0.16	2		<del></del>		4
223	-		160.15		+	H	2940 T	4-	H	-		2A,2C/.68		0.86					$\dashv$
23/	—i		169.15	$\dashv$	╂	$\vdash$	+	+	$\vdash$			2A,2C/.83	0	1.02	┝╼┼		<del></del>	<del></del>	┨
239	_		189.85		+	$\vdash$		+-	+	<u> </u>	0	2A,2C/.99		0.99	$\vdash$		<del> </del>		┨
247			196.15	-	+-	$\vdash$	-	+-	H	<u> </u>	0	2A,2C/.86		0.86			<del></del>		┨
255 272	-		204.25	+	+-	1-1	$\dashv$	+	+-	-	0	2A,2C/.71	0	0.71			<del></del>		1
263			211.45		╁	┢┤		+	+	$\vdash$	0	2A,2C/.58 2A,2C/.70		0.58			<b></b>		1
271			217.75		+-	H	+	+	Н		1A,18/.22	<del></del>		0.70	$\vdash$		<del></del>	<del></del>	1
			228.55		+	╁┤	<del></del>	+	H		0	2A,2C/.63	0	0.85	No		<u> </u>		┪
287 295	$\dashv$	-	252.85	+	1	20	2800	+-	Н	$\vdash$	1A,18/.18			0.88	2		<del></del>		┨
303			289.75	+	+ -	0	2890	→-	H		0	2A,2C/.76		0.86	Ϊ́		AIM nozz.	nress	l I
311			310.45	+	+	20	2230		Н		0	2A,2C/.66		0.66	$\vdash$	-	Effect of T <sub>TO</sub>	press,	ווי
311		,	317.65	┪	╄	20	2230	_	H	$\vdash$	0	2A,2C/.51	0	0.51	<del>   </del>		то то		┨
					1	_			#	긐									1
327	90	5		5.1	42	20	2230	35	. 2	3°	0	0	0	0	No		Angle of attack	pertorm-	1
336	_		141.64	<b>ᆜ</b> -	▙	Н	4	+	H		0	2A/.38	0	0.38	2		ance		1
344	_		150.64	-	⊢	∤-∤		↓_	$\sqcup$	_	0	2A/.45	3A,3B/.38	0.83	$\vdash \vdash$				1
352			165.94	-	┡		4	┼	H	_	0	0			$\vdash \downarrow$				1
360			172.24		Ͱ	$\vdash \vdash$	+	+-	H	-	0	0	3A,3B/.59	_	-+				ł
368			180.34	- -	+-		200	+	Н	<u> </u>	0	0	3A,3B/.43	0.43	•				1
376	ļ		244.24		30	-	2925	-	$\vdash$		0	0	0	0	No		B - 1 61		ł
384			264.04	4	42	(0	2230	+-	₽		14,18/.10		0	0.10	2	71	Fuel flow		┨.
392	_		274.84	4	<b> </b>	${oxdot}$		1	Н		1A,1B/.21		0	0.21	2	_}	malfunction		
400			275.74		<u> </u>	$\sqcup$		1	Ц		1A,1B/.20		0	0.20	2	2	flow only	indica	ted 1
408	_		294.64	4	<b> </b> _	$\sqcup$	-	$\perp$	Ц	_	0	0	0	0	No	$\rightarrow$			1
417	Ť	'	313.54	•	I 🖠	1	•	1	•	- 1	0	0 .	3A,3B/.77	0.77	2	- 1	High test	call an	'n

\*Herein

Table 5. - Concluded.

(d) Concluded.

¥				a d	ď	Ļ	L						
Page No.	Reading Number	Time	z°	o psia	_°&	ok in.	ď	lnj.1/φ,	1nj.2/ø <sub>2</sub>	$\ln j \cdot 1/\phi_1 = \ln j \cdot 2/\phi_2 = \ln j \cdot 3/\phi_3$	4	Igni tors	lgnitors Purpose & Remarks
425	6	135.71	5.1	210	$\vdash$	2100 35.2	00	0	0	0	o	N <sub>O</sub>	Subsonic combustion with
433		14.951			2200			0	2A/.51	34,38/.49 0.90	0.90	2	instrumentation rig and
442		160.91						0	24.32	34,38/.24 0.56	0.56		gas sampling probes
451		182.51			_			0	0	34,38/.50 0.50	0.50		
459		14.102						0	0	34,38/.67 0.67	0.67		
467		18.425		•	_			0	0	34,38/.86 0.86	98.0		
476		12.22		420				0	2A/.50	34,38/.43 0.93	0.93		
485		19.1/2			_			0	24/.43	3A,38/.34 0.77	0.77		
484		295.91						0	0	34,38/.74 0.74	0.74		
502		317.51						0	0	34,38/.90 0.90	0.90		
210		322.01						0	0	34,38/1.07 1.07	1.07		High test cell and
5/8		325.61	-	-	<b>→</b>	-	-	0	0	34,38/1.08 1.08	1.08		AIM nozz. pressure

\* Herein

Table 6. - Instrumentation code-outs for HRE/AIM performance computations,

```
0000000 PROCDEF CO33
0000100 KDOSEL 60, 65, 67, 83, 84, 85, 86, 87, 88, 91, 92,123,124,148,154,156,158,160,162,164
0000200 KDOSEL 165,168,168,171,172,174,175,176,180,181,182,183,186,191,205
0000300 KDOSEL 208,212,226,228,230,231,236,239,240,241,244,248,249,290,292
0000300 KDOSEL 305,306,307,308,309,310,311,312,313,314,315,314,317,318,319
0000500 KDOSEL 320,321,322,323,324,325,326,327,328,329,330,331,332,333,334
0000600 KDOSEL 315,336,337,338
0000600 KDOSEL 315,336,337,338
0000700 KDOSEL 315,316,171,1172,174,176,160,181,10XY)-.26552;DISPLAY VAL(11,1NITRO),VAL(11,10XY)
0001000 QUALIFY AINLETT
0000900 AT 3(2);DISPLAY 'IMPUT PSI(1,1), THEN TYPE GO'
0001000 QUALIFY STAPRS
0001100 AT 320(2);DISPLAY 'IMPUT PSI(1,1), THEN TYPE GO'
0000100 PROCDEF CO34
0000100 KDOSEL 166,168,171,172,174,176,160,181,182,183,126,188,134,156,158,160,162,184
0000100 KDOSEL 166,168,171,172,174,176,160,181,182,183,166,191,195,199,201
0000300 KDOSEL 166,168,171,172,174,176,160,181,182,183,166,191,195,199,201
0000300 KDOSEL 206,208,212,226,228,230,231,236,240,241,244,248,249,252,290,292
0000400 KDOSEL 316,337,338
0000600 KDOSEL 316,337,338
0000600 KDOSEL 316,337,338
0000600 KDOSEL 316,337,338
0000600 CMALIFY AINLETT
0000000 AT 3(2);SET VAL(11,1NITRO)-.73448,VAL(11,10XY)-.26552;DISPLAY VAL(11,1NITRO),VAL(11,10XY)
0000000 AT 3(2);SET VAL(11,1NITRO)-.73448,VAL(11,10XY)-.26552;DISPLAY VAL(11,1NITRO),VAL(11,10XY)
0000000 AT 3(2);SET VAL(11,1NITRO)-.73448,VAL(11,10XY)-.26552;DISPLAY VAL(11,1NITRO),VAL(11,10XY)
0000000 AT 3(2);SET VAL(11,1NITRO)-.73448,VAL(11,10XY)-.26552;DISPLAY VAL(11,1NITRO),VAL(11,10XY)
0000000 AT 3(2);SET VAL(11,1NITRO)-.73448,VAL(11,10XY)-.26552;DISPLAY VAL(11,1NITRO),VAL(11,10XY)
0000000 AT 3(2);SET VAL(11,1NITRO)-.73448,VAL(11,10XY)-.26552;DISPLAY VAL(11,1NITRO),VAL(11,10XY)
  CO33
CO33
CO33
  CO33
CO33
CO33
  CO33
CO33
CO33
  CO33
CO33
CO33
  CO34
CO34
CO34
  CO34
CO34
CO34
  CO34
CO34
CO34
  CO 34
CO 36
                                                0000100 KDOSEL 60, 65, 66, 67,123,124,144,154,156,158,160,152,164,166,168,171,172,174,181 0000200 KDOSEL 182,186,191,193,199,206,208,218,228,230,231,236,260,241,244 (5000350 KDOSEL 282,249,252,289,290,292,294,305,310,312,313,314,315,320
  CO36
  CO36
CO36
  CO36
CO36
CO38
                                                  0030500 QUALIFY AINLETT
0CG0600 AT 3(2);SET VAL(11, INITRO)=.73%%,VAL(11, IOXY)=.26552;DISPLAY VAL(11, INITRO),VAL(11, IOXY)
COCCOOO PROCDEF CO38
                                              COCCOOO PROCDEF CO38

0C0010C KDOSEL 60, 65, 66, 67,123,124,144,154,168,174,181,182,186,191,195,199,201,206,228

CO30200 KDOSEL 230,231,236,240,241,244,248,248,249,252,290,292,294,305,310,312,313

CC00400 KDOSEL 314,315,319,320

CC00400 KDOSEL 399

OC30500 QUALIFY AINLETT

CO30600 AT 3(2);SET VAL(11,INITRO)=.73448,VAL(11,IOXY)=.26552;DISPLAY VAL(11,INITRO),VAL(11,IOXY)

GCC0700 QUALIFY STAPRS
  CO38
CO38
  CO38
                                              OCCOCIO QUALIFY STAPRS
CCCOSC AT 320(2);DISPLAY 'INPUT PSI(1,1), THEN TYPE GO'
OCCOCIO PROCDEF COS2
CODDICO KOOSEL 55, 56, 67,124,137,139,141,154,165,168,178,181,182,195,199,200,201,208,208
COCCOO KOOSEL 226,230,249,252,289,290,292,294,305,313,314,315,320,329,399
COCOLOO QUALIFY AINLETT
COCCSCO AT 3(2);SET VAL(11,INITRO)=.73kb8,VAL(11,IOXY)=.26552;DISPLAY VAL(11,INITRO),VAL(11,IOXY)
COCCOO PROCDEF COSA
COCOLOO KOOSEL 65, 66, 67,124,137,139,141,154,165,168,178,181,182,195,199,200,201,206,226,230
CCCOLOO KOOSEL 249,252,268,289,290,292,294,305,313,314,315,319,320,329,399
CCCOLOO KOOSEL 249,252,268,289,290,292,294,305,313,314,315,319,320,329,399
CCCOLOO QUALIFY AINLETT
CCCOCCO PROCDEF COS7
CCCOLOO PROCDEF COS7
CCCOLOO ROCSEL 62, 65, 66, 74,124,137,139,154,160,168,177,179,181,182,183,187,190,195,199
CCCCOLO KOOSEL 62, 65, 66, 74,124,137,139,154,160,168,177,179,181,182,183,187,190,195,199
CCCCCCC KOOSEL 201,226,226,230,248,249,252,289,290,292,294,305,313,314,315,316,315,320,321
CCCCCCCC KOOSEL 226,226,230,248,249,252,289,290,292,294,305,313,314,315,316,315,320,321
  CO38
  CO 52
  CO 52
  CO 52
  CO52
  COSH
 CO54
  COSA
                                         COOOLOG PROCEEF COS7

OCOLLOG KOOSEL 62, 65, 66, 74, 124, 137, 139, 154, 16C, 164, 172, 179, 181, 182, 185, 187, 190, 195, 189

COCCOO KOOSEL 101, 206, 226, 230, 248, 249, 252, 289, 290, 292, 294, 305, 313, 314, 315, 32C, 321

OCOLOG KOOSEL 139

OCOLOG COLLIFY AIMLETT

OCOCGO AT 3(2); SET VAL(11, INITRO) - .73613, VAL(11, 10XY) - .26387; OISPLAY VAL(11, INITRO), VAL(11, IOXY)

COCOLOG PROCEEF COS6

OCOLOG KOOSEL 201, 206, 226, 230, 248, 249, 252, 289, 290, 292, 294, 305, 313, 314, 315, 319, 320

OCOCCO KOOSEL 201, 206, 226, 230, 248, 249, 252, 289, 290, 292, 294, 305, 313, 314, 315, 319, 320

OCOCCO KOOSEL 201, 206, 226, 230, 248, 249, 252, 289, 290, 292, 294, 305, 313, 314, 315, 319, 320

OCOCCO KOOSEL 321, 329

OCOCCO ROCCEF COS1

OCOCCO ROCCEF COS1

OCOCCO KOOSEL 521, 206, 226, 230, 248, 249, 252, 289, 290, 292, 294, 305, 313, 314, 315, 319, 320

OCOCCO KOOSEL 521, 206, 226, 230, 248, 249, 252, 289, 290, 292, 294, 305, 313, 314, 315, 319, 320

OCOCCO KOOSEL 521, 206, 226, 230, 248, 249, 252, 289, 290, 292, 294, 305, 313, 314, 315, 319, 320

OCOCCO KOOSEL 521, 206, 226, 230, 248, 249, 252, 289, 290, 292, 294, 305, 313, 314, 315, 319, 320

OCOCCO KOOSEL 521, 205, 226, 230, 248, 249, 252, 289, 290, 292, 294, 305, 313, 314, 315, 319, 320

OCOCCO COCCEF COS2

OCOCCO QUALIFY AIMLETT

OCOCCO COCCEF COS3

OCOCCO KOOSEL 139, 201, 206, 226, 230, 248, 249, 252, 289, 290, 292, 294, 305, 313, 314, 315, 319

OCOCCO KOOSEL 139, 201, 206, 226, 230, 248, 249, 252, 289, 290, 292, 294, 305, 313, 314, 315, 319

OCOCCO COCCEF COS3

OCOCCO KOOSEL 139, 201, 206, 226, 230, 248, 249, 252, 289, 290, 292, 294, 305, 313, 314, 315, 319

OCOCCO COCCEF COS3

OCOCCO COCCEF COS4

OCOCCO COCCEF COS4

OCOCCO COCCEF COS5

OCOCCO COCCEF COS5

OCOCCO COCCEF COS6

OCOCCO COCCEF COS6

OCOCCO COCCEF COS6

OCOCCO COCCEF COS6

OCOCCO COCCEF COS6

OCOCCO COCCEF COS6

OCOCCO COCCEF COS6

OCOCCO COCCEF COS6

OCOCCO COCCEF COS6

OCOCCO COCCEF COS6

OCOCCO COCCEF COS6

OCOCCO COCCEF COS6

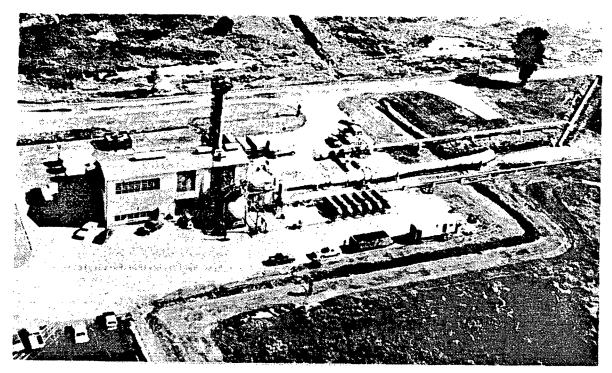
OCOCCO COCCEF COS6

OCOCCO COCCEF COS6

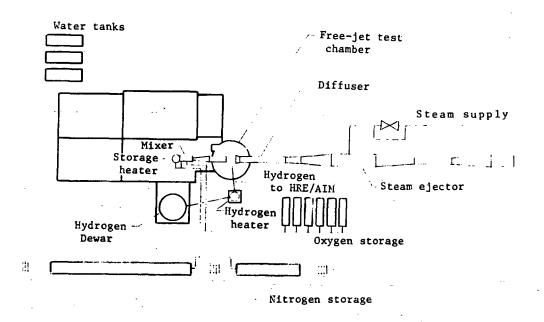
OCOCCO COCCEF COS6

OCOCCO 
 C057
CO57
 C057
 C060
 0.00
C060
C060
C060
 CO61
C061
C061
C061
C061
 C063
C063
C063
C064
C064
COSA
COSA
CO65
C065
                                              0000500 AT 3(2);SET VAL(11, INITRO)=,76751, VAL(11, IOXY)=,23249;DISPLAY VAL(11, INITRO), VAL(11, IOXY)
C059
                                              0000100 KDOSEL 62, 65, 66, 74,137,139,181,182,183,187,190,195,197,199,201,208,226,230,248,252
C069
                                                0000400 QUALLEY AMLETT 0000500 AT 3(2);SET VAL(11, INITRO)-.78079, VAL(11, IOXY)-.23521;DISPLAY VAL(11, INITRO), VAL(11, IOXY)
```

```
0000000 PROCDEF CO71
 CO 71
                          0000100 FX01EF 107,
0000100 KDOSEL 53, 62, 65, 65, 74,124,137,139,158,160,172,179,181,182,183,187,190,195,197,199
0000200 KDOSEL 201,206,226,230,248,249,252,289,290,292,294,305,313,314,315,320,321,322,329,399
 C071
                         CO71
 CO88
  CO8 8
 C088
 CO88
 C088
 CO88
                         0001100 AT 360(3);SET DRAGEX=-0.5 *QOAC;DISPLAY DRAGEX,DRAGEX=PS:ATM,*DRAGEX = -0.5 *
GO01200 QUALIFY CONVTA
0001300 AT 0;SET MY(65)=MY(53),MY(66)=MY(53);DISPLAY MY(53),MY(65),MY(66)
0001400 SETPS 123,0.690
0000000 PROCDEF C089
0000100 KDOSEL 54, 55, 60, 62, 54, 67, 74, 95,124,137,139,157,158,160,165,168,169
0000200 KDOSEL 172,175,176,179,181,182,183,187,190,195,197,199
0000300 KDOSEL 172,275,276,278,283,287,248,249,250,252,289,290,292,294
0000600 KDOSEL 210,223,224,226,227,230,235,248,249,250,252,289,290,292,294
0000600 QUALIFY AINLETT
  6048
 COSS
 C089
 C089
  CD89
 C089
                         0000700 AT 3(2);SET VAL(11, INITRO)-.75188,VAL(11, IOXY)-.28852;DISPLAY VAL(11, INITRO),VAL(11, IOXY)
0000800 QUALIFY CONVTA
0000900 AT 0;SET HV(65)-MY(55),MY(66)-MY(55);DISPLAY MV(53),MY(65),MY(66)
0001000 SETPS 123,0,690
0000000 PROCDEF CO90
 C089
 0089
 C089
                        0001000 SETES 173,0,690
0000000 PROCEEF CO9D
0000100 KDOSEL 54, 55, 60, 62, 64, 67, 74,124,137,139,157,158,160,165,172,175,176
0000100 KDOSEL 179,181,182,183,187,190,195,197,199,202,203,208,207
0000303 KDOSEL 208,216,215,224,226,227,230,235,248,249,250,252,273,289,290
0000503 KDOSEL 292,294,305,313,314,315,320,321,329
0000503 KDOSEL 199
0000503 CDOSEL 199
0000503 CDOSEL 199
0000503 CDOSEL 199
0000503 CDOSEL 199
0000503 CDOSEL 199
0000503 CDOSEL 179,181,181,182,183,187,193,193,187,139,184,187,188,180,187,188,187,190,189,187,188,187,188,160,165,172
0000000 CDOSEL 54, 55, 60, 62, 64, 67, 74, 96,124,137,139,188,137,158,160,165,172
0000000 KDOSEL 175,176,179,181,182,183,187,190,195,197,199,206,238
0000000 KDOSEL 175,176,179,181,182,183,187,190,195,197,199,206,238
0000000 KDOSEL 226,227,230,235,248,249,250,252,289,290,292,294,305,313
0000000 KDOSEL 314,315,320,321,323,399
0000000 KDOSEL 314,315,320,321,323,399,VAL(11,10XY)=.2611;DISPLAY VAL(11,1N1TRO),VAL(11,10XY)
0000000 QUALIFY AINLETT
0000000 QUALIFY AINLETT
 099
 C090
.C090
 C090
 C090
 C090
 C090
 C091
C091
C091
C091
C091
                        ODOBBO QUALIFY ENGPGM
ODCOSO SET ALPHA-3.0;DISPLAY ALPHA
ODOBBO QUALIFY CONVTA
COOLIDO AT C;SET MY(65)-MY(61),MY(66)-MY(61);DISPLAY MY(61),MY(65),MY(66)
ODOBBO PROCDEF COSS
ODOBBO PROCDEF COSS
COCCOSO KDOSEL 54, 55, 60, 62, 64, 67, 74,137,139,148,175,176,181,182,183,187,190,195
CCCOSCO KDOSEL 197,199,206,208,226,227,230,232,248,252,265,266
CCOSCO KDOSEL 167,168,27C,271,272,289,290,292,294,365
COODOBO CONSEL 313,314,315,320,321,329,399
COODOBO QUALIFY ANDZ
CCOOSO QUALIFY ANDZ
CCOOSO QUALIFY CONVTA
ODOBBOO QUALIFY CONVTA
ODOBBOO AT 3560(3);SET DRAGEX--0.5-QOAC;DISPLAY DRAGEX,DRAGEX-PSIATM, DRAGEX --0.5-QOAC
ODOBOO AT 0.SET MY(65)-MY(53),MY(66)-MY(53);DISPLAY MY(53),MY(65),MY(66)
OOOOOO PROCCOEF COSS
OOOOOO PROCCOEF COSS
OOOOOO PROCCOEF COSS
OOOOOO COMACHS
OOOOOOO COMACHS
OOOOOOO COMACHS
C091
 C091
 CO91
C091
C092
 CO9 2
 CO9 2
 C09 2
 CO 9 2
 CO92
CO93
 CO93
C093
                         0200200 KDOSEL 96
                         0000500 QUALIFY AINLETT
                         0000600 AT 3(2);SET VAL(11, INITRO)-.655706, VAL(11, 10XY)-.346296;DISPLAY VAL(11, INITRO), VAL(11, 10XY)
0000700 TUNNOPT 3
0000000 PROCDEF CO94
                         0000100 COMACHS
0000500 QUALIFY AINLETT
C000700 AT 3(2);SET VAL(11, INITRO)=.7628%, VAL(11, IOXY)=.23716;DISPLAY VAL(11, INITRO), VAL(11, IOXY)
0000500 TUNNOPT 3
0000000 PROCDEF C095
0000100 COMACHS
 C094
 C094
 6094
CO95
                          COOGGO QUALIFY AINLETT
 CO9 5
                         -0000700 AT 3(2);SET VAL(11, INITRO)-.7486, VAL(11, 10XY)-.25138;DISPLAY VAL(11, INITRO), VAL(11, 10XY) 0000800 TUNNOPT 3 0000800 PROCDEF C096
 CO95
C096
                        0000000 PROCDEF C096
0000100 COMACH5
0000600 QUALIFY AINLETT
C000703 AT 3(2);SET VAL(11, INITRO)-.76%88, VAL(11, IOXY)-.23512;DISPLAY VAL(11, IMITRO), VAL(11, IOXY)
0000800 TUNNOPT 3
0000000 PROCDEF C097
0000100 KDOSEL 5%, 55, 60, 62, 6%, 85, 68, 67, 7%,12%,137;139,181,182,183,187,196,195,197
0000200 KDOSEL 199, 226, 230, 248, 252, 280, 289, 290, 292, 294, 305, 313, 31%, 315, 320, 321, 329, 399
0000500 QUALIFY AINLETT
0000500 AT 3(2);SET VAL(11, INITRO)-.77086, VAL(11, IOXY)-.2291%, DISPLAY VAL(11, INITRO), VAL(11, IOXY)
 C096
 C096
 CO96
CO97
 CD97
 C097
 CO97
                         0000700 QUALIFY ANDZ
0000800 AT 360(3);SET DRAGEX--0.5.QOAC;DISPLAY DRAGEX,DRAGEX.PSIATH, DRAGEX = -0.5.QO.AC.
 C097
 CO97
CO97 0001000 QUALIFY ACMESTR
CO97 0001000 QUALIFY ACMESTR
CO97 000100 AT 350(3);SET XCTP=XCT;DISPLAY XSLE,XCT,XCTP,XSTE, SUBSONIC COMBUSTION*
COMACHS 0000000 PROCODEF COMACHS
COMACHS 0000100 KDOSEL 58, 55, 60, 62, 64, 65, 66, 67, 74,124,137,139,157,158,160,162,165,172,176,178
COMACHS 0000200 KDOSEL 181,182,183,187,190,195,197,199,206,226,230,248,249,252,280,289,290,282,294,305
COMACHS 0000300 KDOSEL 313,314,315,320,321,329,399
```

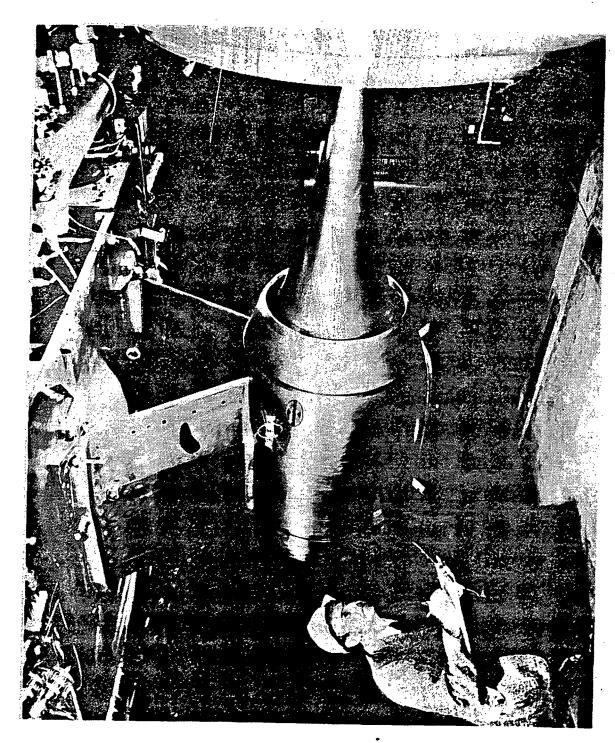


(a) Hypersonic Tunnel Facility (HTF).

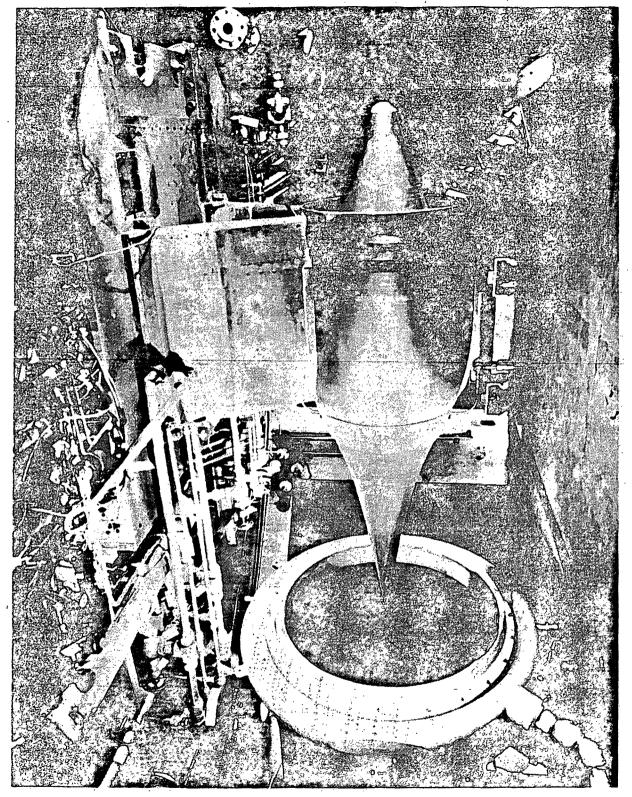


(a) Schematic layout of the NASA - Lewis - Flum Brook Hypersonic Tunnel Facility (HTF).

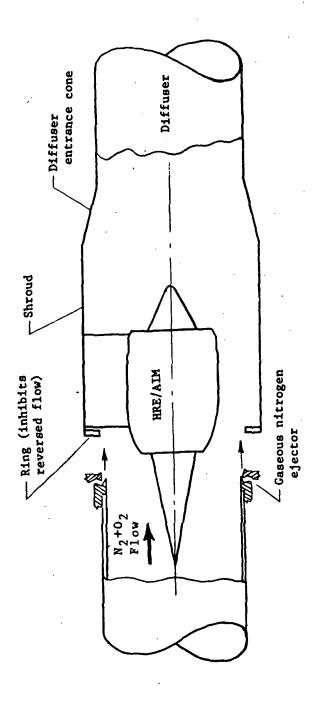
Figure 1. - MASA - Lewis Rosearch Center's Plum Brook Station Eypersonic Tunnel Facility (HTF) and the Hypersonic Research Engine/ Aerothermodynamic Integration Model (HRE/AIM) installation.



(c) HRE/AIM partically installed; pretest.



(d) HRE/AIM partically installed; Mach 5, 5, and 7 post test.



(e) Schematic of HRE/AIM test section located in the free-jet test chamber of the HTF.

Figure 1. - Concluded.

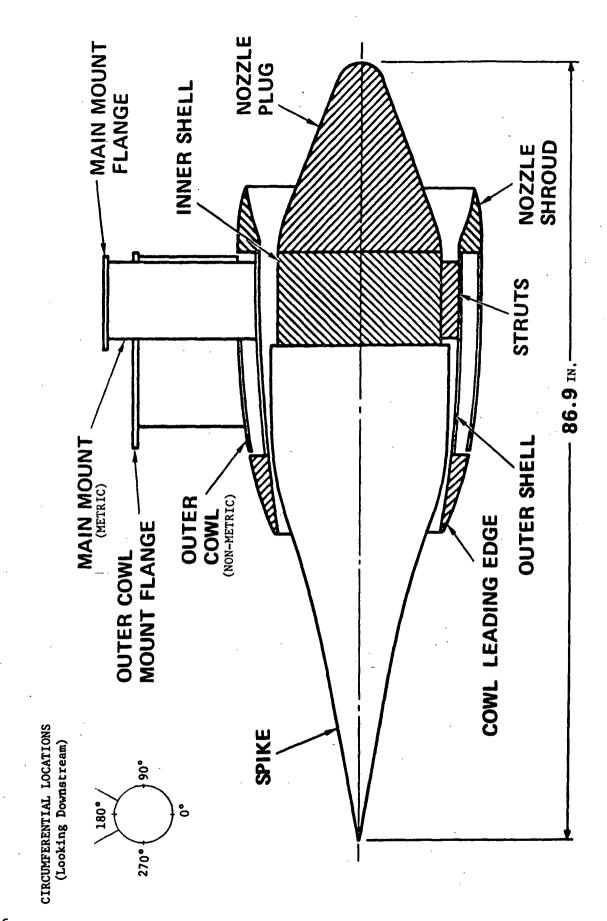
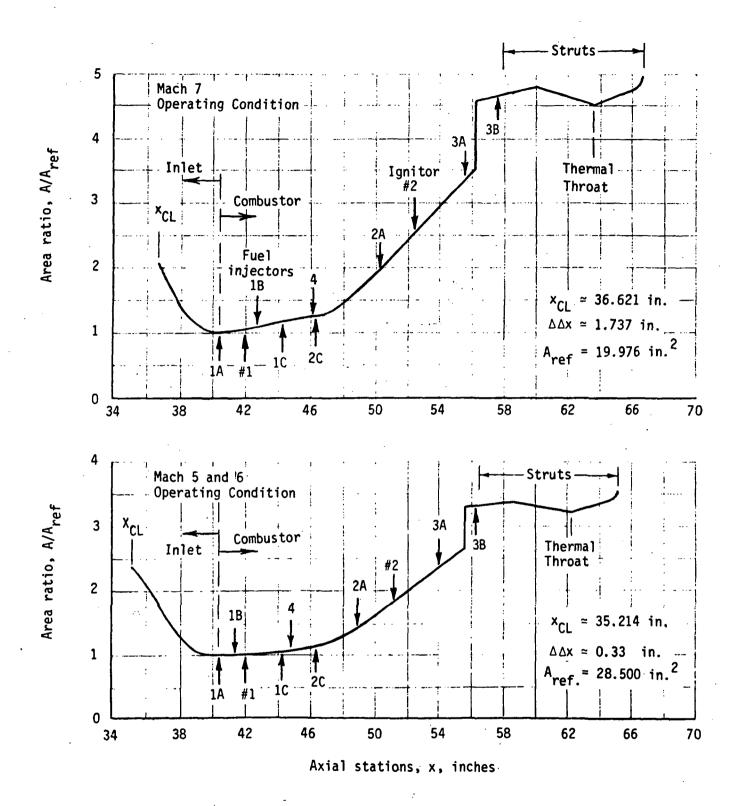


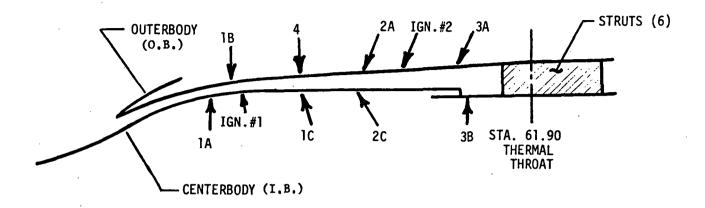
Figure 2. - General Configuration of the AIM



(a) Combustor area ratio distributions

Figure 3. - HRE/AIM combustor information.

### COMBUSTOR CONFIGURATION



(Mach 6 position, x<sub>CL</sub> = 34.884 in.)

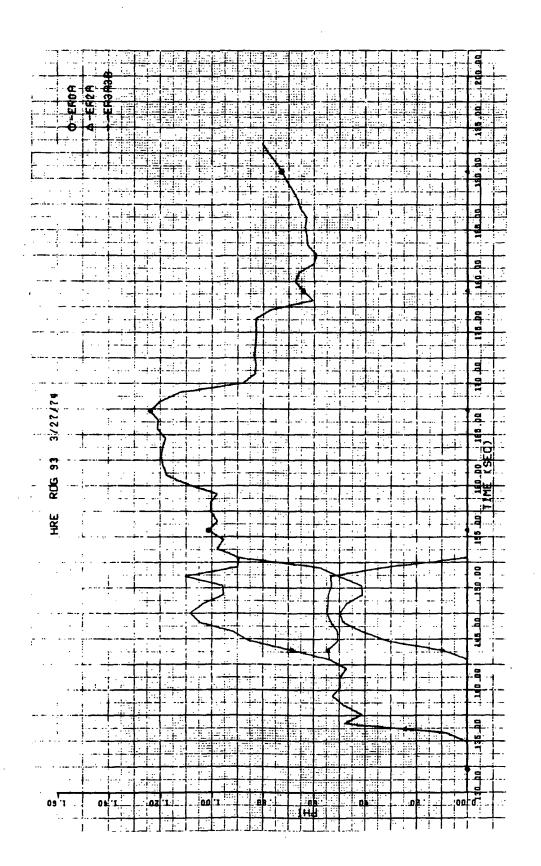
Injector	Number of Injectors	Diameter, in.	Injection Angle <sup>a</sup> , deg	j. <u>S/d</u>	x, in.	Location
1A	37	0.119	90	13.1	40.5	I.B.
18	37	0.119	90	13.9	41.25	0.B.
10	37	0.119	106	13.5	44.5	I.B.
4	37	0.119	90	14.2	44.5	0.B.
2A	60	0.095	67	11.4	48.5	0.B.
20	60	0.095	119	10.6	46.5	I.B.
3A	114	0.090	65	7.0	53.75	0.B.
3B	102	0.095	90	6.3	55.9	I.B.

### IGNITOR PARAMETERS

Ignitor	<u>x, in.</u>	9	Circum	ferent	ial lo	cation	<u>s</u>	Injection Angle <sup>a</sup> , deg.	Location
1°	42.00	55	110	165	230	290	350	94.5	I.B.
2	50.98	40	100	-	220	240	280	60.0 <sup>b</sup>	0.B.

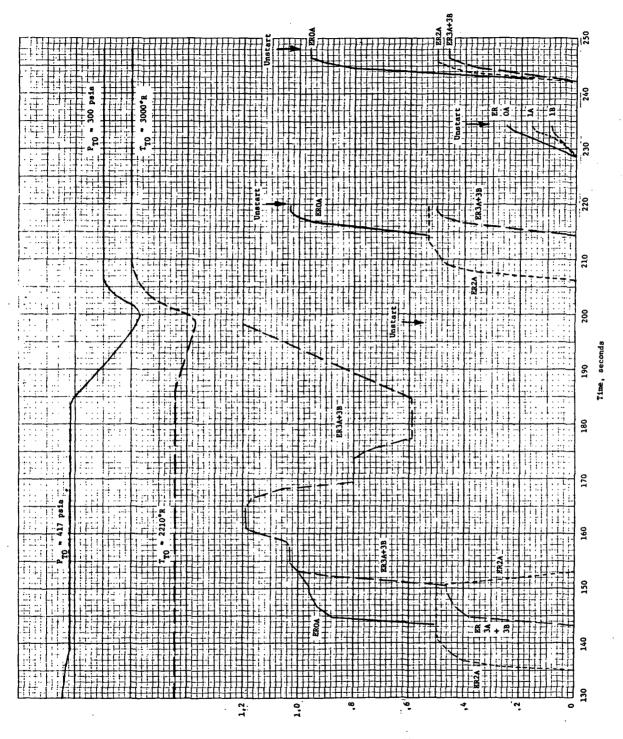
- a. With respect to AIM centerline.
- b. Also looking upstream, ignitors #2 are inclined 30° clockwise.
- c. Plug welded prior to reading 57.
  - (b) Combustor configuration and parameters.

Figure 3. - Concluded.

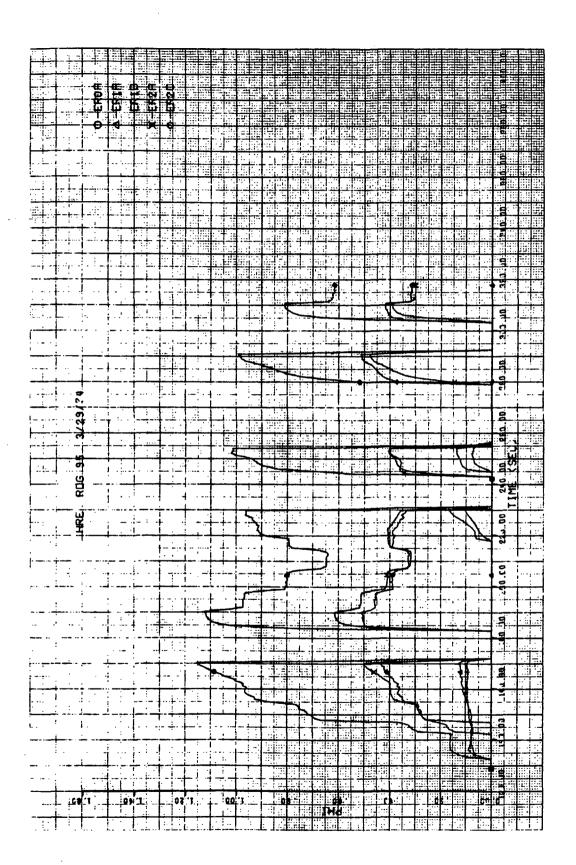


(a) Reading 93 – Measured Equivalence Ratio,  $\phi$ 

Figure 4. - HRE/AIM fuel equivalence ratio; Mach 5 component integration and performance results.

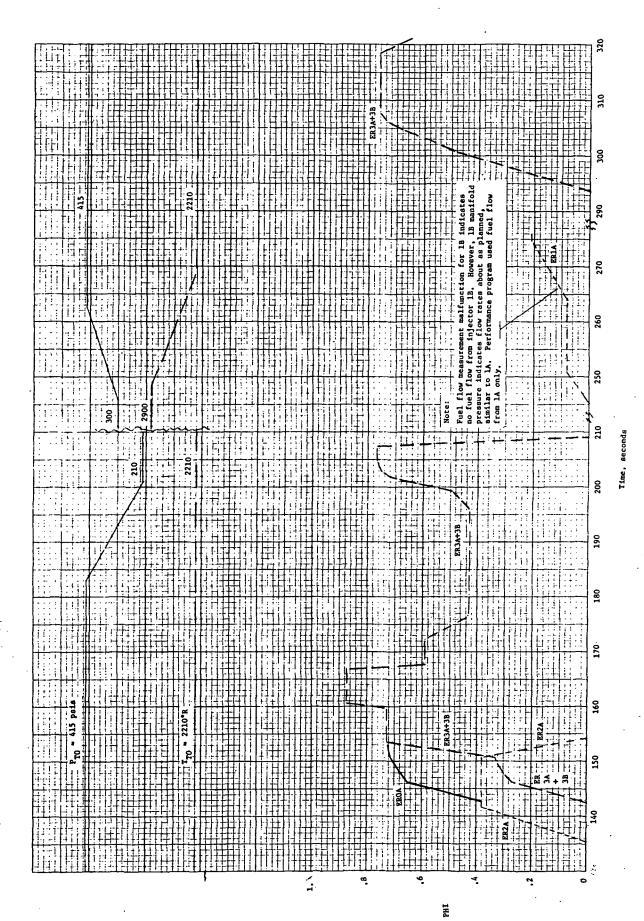


b) Reading 94 - Measured equivalence ratio, ¢



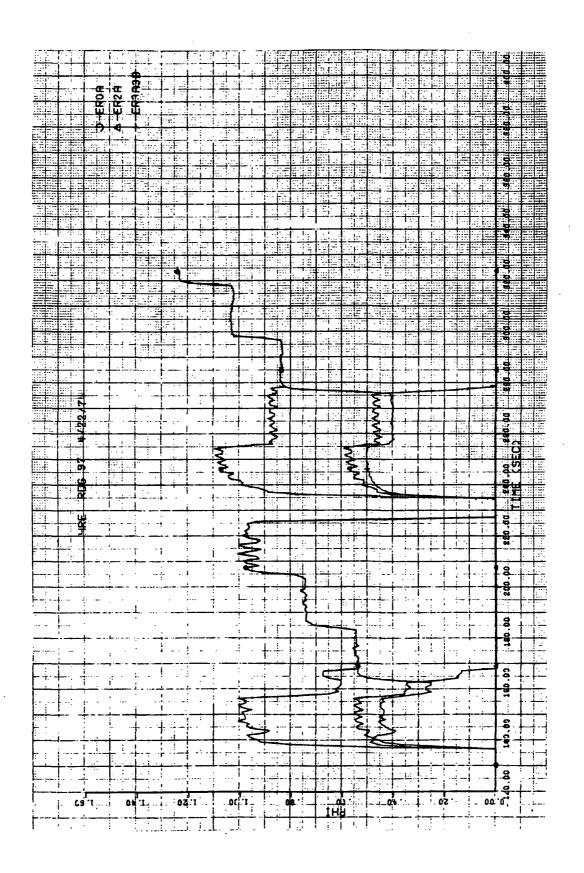
(c) Reading 95 - Measured Equivalence Ratio, Ø

Figure 4. - Continued.



(d) Reading 96 - Measured equivalence ratio,  $\phi$ 

Figure 4. - Continued.



Reading 93

t = 134.03 sec.

READING # 1093 BLUCK # 19 TIME # 134,029 HAUN 5.2 PT # 415,247 TT # 2026.1

	<b>-</b> '	Œ		44440	אטף י	SON	1. A C H	4EL	,	4/1	٠.	A/AC	707	<b>ن</b>	IVAC	9.1
417	2	85.	511)	1.3228	29.269 29.268	2134	5.1/0	4642	1.750	J.15287	35.688	0.8655	5020	11.027	146.1	
- 00	2026	. 5	5111	1.3229	24.249 29.269	2154 2108	0.348	6.59	1.952	0.15287	55.808	0,8055	204	1,993	150.4	
10 kg L	N	3 d d d	511) 81)	1.322A	29,269	901	5.146	4638	1.750	0.15579	365.45	0.8655	5113	11.630	146.1	
- CO	V	365	511)	1.3248	29.264	<134 <107	0.467	658	1.452	0.15579	34.538	0.8655	\$113	2.078	146.1	
NET THROAT 10.400 180.899 10.400 21.574	1155	573.60 151.20	501)	1,3241	29,269	2116	2.038	3337	1.802	1.18081	34,538	0.1120	4203	62.413	121.7	
61		373	501) 268)	1.3241	29.469	2116	2.162	3415	1.602	1.09403	34.554	0.1233	0927	56,055	125.4	
117.00	~ ~	27.5	5013	1.3241	29.269	2116	0.551	1139	1.831	1.09403	34.536	0.1233	4200	19.363	123.4	
က ကြောင်း	~ ~	1. 1.73 1.54	501J	1.3241	29.269	2110	2.016	3315	1.802	1.20328	34.554	0.1121	0027	61.495	121.6	
10 152		76.	4993	1.3243	29,269	2113	1,813	3101	1.613	1.20683	34.558	0.1117	4070	58.161	116.0	
202 150 24 205 150 24 305 20 30	1984	372.05	309)	1,3243	29,269	2113	1.797	3 9 9		1.20751	5 to 5 5 to	6-1117	3 0 3	57.864	117.7	
108 146-02 27-17	1 1 4 6 5 5 6 5 6 5 6 5 6 5 6 5 6 5 6 5 6 5	371 170	314)	1,3244	24.269 29.268	2112. 1728	-	306	5	-2042	34.5	0.111	0 4 0 4	7.14		
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310 117 68 510 31 50	- 5 - 5	364.	492) 342)	1.3253	24.268	1792	1,531	2764	1.620	1.15504	34,558	0.1167	3876	49.256	112.4	
780 115.13	~ 5 3 .	363.	491) 345)	1.3254	29.269	1799	1.504	2706	1.827	1.15056	34.538	0,1172	3456	P85.44	111.6	
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PAGE 4

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# READING # 0995 BLUCK # 59 TLF # 154.629 "ACH 5.2 PT # 415.249 TT # 2026.1

### GANJET PENFURMANTE

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Reading 93

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48 TIRE # 142.129 HACH 5.4 Pl # 415.749 TI # 2064.7

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## RAMJET PERFURHANCE

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MEASURED IMAUST  MEASURED IMAUST  MEASURED SPECIFIC IMPULSE	1404. (LAF.) 1405. (LAF.) 5345. (LAF.SEC/LRM) 0.5046. (LAF.SEC/LBM) 0.5040	ANGLE OF BITACK  TASK FURN ABILL  ADDITING PRESSURE RECOVERY  INTEL PIESSURE RECOVERY  TOTAL PIESSURE RECOVERY  TOTAL PIESSURE RECOVERY		10 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	(DE 6 MEES)
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SHURON GAR SULVESCE			CUMBINSTOR		
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		VACUUM STREAN HAUST NOZZLE CCEFFICIENT ** PACCESS EFFICIENT ** KINETIC ENERGY EFFICI	CCEFFICIENT & CS.		
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10L 4	642.42		29.268	25,056	25.056	25,059	25.059		25.175	25.655	45.655	25.926	25.427	26,123	26,125	24.030	60.73	24.638		24.624	;	25.068		74.464	, ne	24.447	24	24.538	į	24.572		25.244	! !	25.181		4. 40
GAMMA	1.5254	2005-1	1.3633	1.5207	1.3303	1.3206	1.5302	1.5153	1.3236	1.2939	1.3070	1.2776	1.2973	1.2667	1.2801	1.4750	76071	1.2749		1,2661		1.2540		1.4404	0000	1.2296	7716	1.2248	,	1.616/	,1	10146	· •	1.1812	)	1 1747
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1 566	s		2.524			2,522			2.518			2.515			505.5			2,528			2.515			2.519			2.526			2.528			2.424			67576
616.	VEL	•	5249			2301			2695			2982	,		3187			2565			7119			7577			7204	,		7692	,		Bubb			0679
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9 MAC	GAMMA MOLMI SONV MACH VEL S	78.187	25.65		25.192	25.260		25.403	25.491		25.210	25.313	1	25.215	25.320		35.157	902.52		25.410	25.453		25.210	25.453		25.157	25.455		25.157	25.483		25.476	25.453	•	25.209	25.452
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7 1146 1		21	(4551) 9 4	- 12	358.9(1626)	255-1(1549)	20	348,8(1620)	(21515)	002 6	341,9(1615)	164.1(1482)	200	.9(1617)	138.9(1463)		.8(1684)	270-3(1560)	3	341.9(1594)	(612 )30	4	341.9(1594)	.6( \$85)	3	401,8(1654)	(457 )40	3	401.8(1654)	.7( 610)		5	.4( 432)	•	301.6(1517)	.2( 648)
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PAGE 5	P-08/P10	6.5812-02	6.269E=02	6.236E=U2	6.070E-UZ	2.530£=ù2	2.505E=02	2.0436.02	-6106-02	.0566-02	.9186-03	. 960E-US	6.667E=U3	.8396-03	.763E=03	1.6816-03	0	•	0	•	0	
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158,329		GAMMA	1.3196	1,3196	1,3196	1,3196 1,3215	1.3214	1.3214	1.3248	1.3214	1.3217	1.3567	1.3218	1,3221	1.3228	1.3229	1.3231	1.3231	1.3235	1,3237
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PT ==	MACH		1.753	1.867		388	931	0.638	***	# # O	0.626	0.618	0.558	0.558	0.870	0.569	0.573	0.583	0.596	0.624
5.2	SONV	2121	2110	2116 1695	2114	2108	2000	2158	2562	2582 <b>25</b> 10	<b>2637</b>	2720 2655	2989	2960 2903	2989	2997 2939	3011	3047 2988	3082 3021	3157
MACH	MOLWT	29.269 <b>29.</b> 268	29.269	29.269	29.269	29.269	29.188	29.188	25.666	25.668 25.668	25.829	26.094 26.095	23.073	23.076	.2713 23.140 .2765 23.162	23.108	23.232	23,350	23.473	23.775
150.32	BAMMA	1.3237	1.3240	1.3241	1.3843	1.3247	3218	1.3220	1,2984	1.2984	1.2914	1.2798	1.2507	1.2757	1.2713	1.2699	1.2476	1.2613	1.2546	1.2375
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	S.	1E-0	<b>6</b> 6 0	96	9 9	۳.	9. Y		ے د یا لا		E	DE O	36.0	SE 0	얦	96	۵ رو د د د		֓֞֜֜֜֜֜֜֜֜֓֓֓֜֜֜֜֓֓֓֓֜֜֜֜֜֜֓֓֓֓֜֜֜֜֓֓֓֜֜֜֓֓֡֓֜֜֜֜֓֡֓֡֓֜֜֡֡֡֡֓֜֜֡֡֡֡֜֜֡֡֡֡֡֜֜֝֡֡֡֡֡֡֡֡	ם פון	90	16 0	96	SE 0	9. 9.	9 ¢	7.		9	OE G	0 Y	¥.	9 9	9	9		9			36.0	F 0	9 i	36	10	3	A 10 0	, C	9E 0	SE G
	XAB	6.98	1.83	3.07	08.5	20.0	, 5		7		3.70	3.73	3.60	3.83	3.87	4.87		700	) i	0	0	4.04	4.12	4.13	4.15	Ž.			2	4.62	2		10.4	. 92	5.07			9	5.72	5.62	5.62	2.62	90.4	6.6	5.70	5.774E	A.07	6.21	9.46
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PAGE 5	P-08/610	6.270E-02	6.235E-02	.065E-02	.552E-02	2.662E-02	2.132E-02	1.638E-02	1.073E-02	932E-03	963F=03	SUSPED S	909E-03	1.680E-03	558E-03	0000	000	000	000	000	000.0
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	P-08/PS0	4.232E	4.208E	4.093E	1.723E	1.796E	1.439E	1.105E	7.241E	1.304E	2.000E	4.478E	3.921E	1.134E	1.119E	00000	00000	00000	000.0	00000	000.0
	P-18/PT0	5.999E-02	5.999E-02	5.68UE-02	3.035E-02	2.309E-02	1.4735-02	1.208E-02	9.8385-03	7.501E-03	6.4435-03	4.410E-03	4.211E-03	4.947E-03	4.951E-03	6.251E-03	5.687E-03	4.091E-03	4.319E-03	5.831E-03	5.8346-03
	P-18/P50	4.049E 01	4.049E 01	3.834E 01	2.049E 01	1.558E 01	9.944E 00	8.155E 00	00	00	00	00	00	3,339E 00	00	00	3.838E 00	2.761E 00	2.915E 00	3.935E 00	3.938E 00
2119.8	CAWALL	4.337E 03	4.342E 03	4.3688 03	4.583E 03	4.665E 03	4.760E 03	4.848E 03	4.922E 03	5.036E 03	5.088E 03	5.273E 03	5.290E 03	5.374E 03	5.375E 03	5.427E 03	5.525E 03	5.630€ 03	5.684E 03	5.707E 03	5.707E 03
<b>H</b>	0-0B	-1.846E 03	-1.849E 03	-1.865E 03	-1.985E 03	-2.031E 03	-2.085E 03	-2,136E 03	-2.177E 03	-2.227E 03	-2.245E 03	-2.301E 03	-2.306E 03	-2.335E 03	-2.335E 03	-2.396E 03	-2.327E 03	-2.327E 03	-2,327E 03	-2.327E 03	-2.327E 03
PT = 416.749	9-18	-1.570E 03	-1.572E 03	-1.587E 03	-1,690E 03	-1.725E 03	-1.762E 03	-1.792E 03	-1.814E 03	-1.845E 03	-1.857E 03	-1.895E 03	-1.898E 03	-1.913E 03	-1,913E 03	-1.936E 03	-1.972E 03	-2.004E 03	-2.029E 03	-2.071E 03	-2.071E 03
MACH 5.2	X09	-3.415E 03	-3.421E 03	-3,451E 03	-3.675E 03	-3.756E 03	-3.847E 03	-3,928E 03	-3,991E 03	-4.072E 03	-4.102E 03	-4.196E 03	-4.204E 03	-4.248E 03	-4.248E 03	-4.332E 03	-4.300E 03	-4.331E 03	-4.356E 03	-4.398E 03	-4.399E 03
TIME = 158,329																		3.220E 03			
99	P-08	2,613E 01	2.599E 01	2.527E 01	1.0646 01	1.109E 01	8.887E 00	6.825E 00	4.471E 00	8.050E-01	1.235E 00	2.765E 00	2.421E 00	7.000E-01	6.908E-01	000.0	0000	000	0000	0000	0.00
0093 BLOCK =	P=18	2.500E	2.500E	2.367E	1.265E	9.621E	6.1405	5.036E	4.100E	3.126E	2.685E	1.838E	1.755E	2.061E	2.063E	2.605E	2.370E	1.705E 00	1.500E	2.430E	2.431E
ADING = 0093	XABS	.503E 01	.507E 01	.527E 01	.693E 01	.760E 01	.837E 01	.909E 01	.970E 01	.065E 01	.108E 01	.261E 01	.276E 01	.351E 01	.351E 01	. 484E 01	.769E 01	.159E 61	. ##0E 91	.726E 01	.727E 01

READING = 0093 BLOCK = 66 TIME = 158,329 MACH 5.2 PT = 41c.749 IT = 2119.8

ENGINE PERFORMANCE

## RAMJET PERFORMANCE

INLET

			-			
CALCULATED THRUST	2610. 2934. 2944. 0.8988	(LBF) (LBF) (LBF-SEC/LBM)	ANGLE OF ATTACK MASS FLOW RATIO ADDITIVE DRAG COEF LIMITING PRESSURE DELTA PRESSURE TOTAL PRESSURE REC	MASS FLOW RATIO		(OEGREES) (PSI)
• •	1.9	(18F) (18F)	INLET PROCESS EFFICIENCY = 3 INLET PROCESS EFFICIENCY = 5 KINETIC ENERGY EFFICIENCY = KINETIC ENERGY EFFICIENCY = KINETIC ENERGY EFFICIENCY = ENTHALPY AT PO = SUPERSONIC.	SUBSONIC	0.9033 0.9033 0.9258 0.8928	(BTU/LBM)
THRUST COEFFICIENT	0.9177	LBreselvion	ENIMALPT AT PU .	SUBSONIC		9TU/LBM)
MOMENTUM AND FORCES				20.00000	٠	
INLET FRICTION DRAG.  JALET MOMENTUM CHANGE.  COMBUSTOM FRICTION DRAG.  COMBUSTOM STRUT DRAG.  COMBUSTOM MOMENTUM CHANGE.  NOZZLE FRICTION DRAG.		(	FUEL-AIR RATIO EQUIVALENCE RATIO. COMBUSTOR EFFICIEN TOTAL PRESSURE RAT COMBUSTOR EFFECTIV INJECTOR DISCHARGE	FUEL-AIR RATIO	0.0261 0.598 0.916 0.916 0.8760 0.8760	:
		(LBF)		NOZZLE		
		(	VACUUM STREAM THRU NOZZLE COEFFICIENT PROCESS EFFICIENCY KINETIC ENERGY EFF	CT	0.9297 0.8571 0.8618 0.8427	
0	0.68.		,			
				FUEL INJECTORS		
NOMINAL COWL LEADING EDGE	34.884 0.2909 40.400 35.175 73.515		INJECTORS 1A 1B 1C 2A	STATION VALVE 40.400 41.276 44.300 48.751	w	
::	87.267 56.431	(IN) (IN)	3.C.			
STRUT TRAILING EDGE	65.031 62.191	(NI)	96 a	56.226		
		•		)		

t = 162.83 sec.

03/03/25

READING = 0093 BLOCK = 71 TIME = 162,829 MACH 5,2 PT = 416,749 TT = 2112,3
RAMJET PERFORMANCE

SUKMARY REPOR

ETAC					•														
PHI								• .				<b>.</b>							
IVAC	151.6	156.4			124.6	126.3	126.3	124.6	120.8	120.5	119.9	117.1	115.4	115.1	114.6	114.5		114.3 115.5	
g	10.952	1.924	11.176	2,098	64,103	59.202	19,321	63,328	59,541	59,187	58,535	54.886	51,330	50.944	50,109	50.088		47.168 45.361	
MOMTR	4982	5142	5177		4260	4317	4317	4259	4131	4121	4098	£003	3945	3936	3917	3916		3949	
A/AC	0.8648	0.8648	9.0	0.8648	0.1119	0.1231	0.1231	0.1119	0.1115	0.1116	0.1114	0,1125	0.1163	0.1166	0.1171	0.1171	[	0.1243	
*	32.867	32.867	101.4		34.191	34.191	34.191	34.191	34,191	34.191 (	34.191	34.191	34.191	34.191	34.191 (	34.191 (		34.191 (	
W/W	.14838	.14838	15436	15436	ु •14711	.08483	.08483	.19317	.19713	.19656	.19844	.18659	.14733	1.14480	.14009	.13988		99918	
s	1.761 0	1.963 0	1.761 0	1.963	1.808.1	1.808.1	1.840 1	1.808.1	1.819 1	1.620 1	1.822 1	1.628 1	1.632 1	1.832 1	1.833 1	1.833 1	į	1.635 1.1.836 0.	
VEI.	4750	834	4742	87.	3457	3512	1146	3415	3200	318371	3143	2976	2879	2863	2828	2828		2921	
MACH	5.170	0.388	5.120	407	2,099	2,159	0,545	2.056	1,853	1.837	1.802	1.667	1,599	1,589	1,564	1,563	ì	1.648	
SONV	2176	2176	2176 926	2176	2152 1647	2152 1626	2152 2104 (	2152	2148	2148	2147	2142	1800	2132 1803	2130	2130	2124 1802	2120	-
POLNT	29.269	29.269	29.269 29.268	29.269	29.269 29.268	29.269 29.268	29.269 29.269	29,269	29.269	.3219,29,269	29.269	29,269	29.269	29.269	29.269 29.268	29.269 29.268	29.269	29.269 29.268	
GAMMA	1.3198	1,3199	1.3198	1,3199	1,3216	1.3216	1.3216	1.3216	1.3218	1.3219 1.3569	1.3219	1.3223	1.3229	1.3230	1.3231	1,3231	1,3235	1,3238	
	535)	535) 521)	535)	535) 520)	521) 282)	521) <b>2</b> 75)	521)	521)	519)	519)	518) 321)	516) 339)	511)	510)	509)	509) 349)	506) 346)	504)	
I	407.6	393.7(	41.	0 0 407.61 392.4(	193.	393.	367.	393.6( 160.3(	291.5( 186.8(	391.3( 188.9(	391.0( 193.6(	11.	283.4(		381.4(		378. 218.	11 4 376.2( 205.6(	
-	2112	2112 2063	2112	4 2112 2058	2062 1169	2062	2062 1968	2062 1191	2055 1294	2054 1302	11 2053 1320	2043	2025 1413	2023	2018 1428	2018 1428	2007	18 2000 1367	
Q.	6,749 0,586	1.362 9.366	416.749 0.621	NS 21.362 19.177	0AT 189.527 20.481	189,527	119,138 98,336	189.421	158.848 25.557	156.721 25.844	O V	יט פֿט	124.467 29.731	<b>60 0</b>	00	0.38	3,56 8,39	111.447	
	1ND TUNNEL 0.000 41 0.000	0.600 2 0.600 1	00000	0.600 0.600 0.600	NLET THROAT 10.400 189.527 10.400 20.481	00000	0.400 0.400	0.410	1.288	1.000000 1.00000 1.00000	11.500 15	2.460	4.074 6.074 6.074	4.010	4.788	4.800 4.800	6.260	OMBUSTOR 17.310	

## REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

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740	115.5	•	120.3			8.9	150.7 0	152,2 0	'n	50 50 50	65.6		91.1	91.5	192.5 0	•	194.6 0	195.8 0	199.0 0
c	45.373	44 . P.84	43,266		7.11		13,638	12.066	12.053	11.122	027	242	23	•	8.897	9.833	10.221	10,725	11,912
A LAC	3949	4017	4114	4215	8525	5037	5170	5303	5306	5515	5770	6752	6755	6770	4089	6822	6881	6923	7033
A/AC	0.1335	0.1434	0.1554	0.1662	195	23	0.2480	0.2629	0.2631	0.2782	0.2967	•	0.3679	0.3690	0.3716	0.3674	0.3686	0.3695	0.3753
,≅	34.191	34.191	34.191	34.191	19	.31	34.312	34.831	34.831	34.631	ħ	ິ	35.351	35.351	35,351	35.351	35.351	35.351	35,351
. A/#	•	0.93120	0.85899	0.80336		0.56316	0,54015	0.51727	0.51688	0.48879	0.45827	•	0.37511	0.37405	0.37143	0.37566	0.37448	0.37358	0.36778
V:	=	1.834		1.851	1.832	1.866	1.869	2.240	2.240	2.250	2.276	2.575	2.576	2.570	2.573	2,655	2,654	2,654	2,653
VEL	2921	3060	3241	1135	Ŷ		1625	1501	1501	1464	1548	1584	1584	1535	1541	1684	1756	1847	2084
MACH	-	1.770	1.942	645.0	0.32	•	0.796	0.582	0.582	0.558	0.565	0.522	0.522	0.510	0.510	0.489	0.510	0,537	0.608
SONV		2118	2115	2113 2065			2137 2040	2636 2576	2637 2577	2679 2624	2793	3083	3084	3059	3071 3023	3473	3473	3472 3437	3471 3426
MOLWT	W W	29.269 29.268	29.269 29.268	29.269 29.269	29.269	29.187	29.187 29.187	25.061 25.061	25.063	25,186 25,186	25,540	22.231	22,234	22.165	22.200	24.149	24.099	24.101	24.105 24.183
GAMMA	1,3238	1.3240	1.3242	1.3243	1.3247	1.3210	1,3220	1.2970	1.2969	1.2915	1.2754	1.2689	1.2666	1.2727	1.2707	1,1532	1,1533	1,1534	1,1535
	504)	502) 315)	501)	474	496)	513)	514)	825) 781)	826) 781)	862)	969)	(1195)	2 5(1196) 3(1148)	(1160)	1181)	(1867)	(1856)	(1866)	(1810)
I	12 4 376.2( 205.7(	13 374.6( 187.4(	373.2(	372.00 372.00 346.30	16 6 368.8( 359.8(	17 202 462.20 50.30	360.90	392.2(	392.10	389.5(	ומימות	418-59 362-4		200 × 200 ×	364	411.2( 411.2( 354.5(	348.3	408.8 340.6	405.4 318.6
<b>-</b>	19 2000 1367	20 1994 1297	1989 1202	22 1985 1891	23 1973 1940	2034 1788	2029 1839	571	572	2816 2693		3231 3231	3233 3233	3279			5068 4980	5067 4970	5063 4938
	11.464 24.698	113,658 20,831	20,828 16,824		12,150 04,847		54.117	67.754	67.746 2 54.630 2	67.170 55.150	65.803 53.858	63.114 53.220		63,310 63,791	63.190 53.695	60.580 52.832			
	~ <b>~</b>	5 7	<b>,</b>			2.000 2.000 2.000 2.000 2.000			053	. 615 1.615 1.615	3.760 5.760	5.228 5.228	5.238 5.238	5.293 5.293 5.293	5.400 5.400 5.400 5.400	5.513 5.513 0.813	5.793 5.793 DMBUSTOR		

READING # 0093 BLOCK #

m																																	-
PAGE																														•			
	ETAC		1.00	•		1.00			1.00			1.00	) }		1.00			1.00			1.00			1.00			1.00			1.00			1.00
	IVAC PHI		0.71			0.71			0.71			0.71			0.71	•		0.71			0.71			17.0			0.71	•		0.71			0.71
	IVAC		201.1	! !		199.2	1		197.6			204.6	,		198.1			259.8			273.3	1		260.2			273.A			265.1		٠.	240.5
	ø	-	7108 12.721 201.1 0.71 1.00			7042 16.476 199.2 0.71 1.00	•		6986 18.923 197.6 0.71 1.00			7234 20.290 204.6 0.71 1.00	•		7001 16.332 198.1 0.71 1.00			8.445 259.8 0.71 1.00			4.623 273.3 0.71 1.00			8.456 260.2 0.71 1.00			4.618 273.8 0.71 1.00			6.733 285.1 0.71 1.00			8502 7.488 240.5 0.71 1.00
	MOM		7108			7042			6986			7234			7001			9185			9662			9200			9680	1		10079			8502
	A/AC		.3777			3650			.3553			.3553	1		.3553			1.9371			3.8231			.9371			3.8344			.7936		•	1.9371
ņ	. 3		35,351 (			35,351 (			35,351 (			35,351 (		•	35,351 (	ı		15.351			55.351			35.351			55.351			35,351			55.351
.829 MACH 5.2 PT = 416.749 TT = 2112.3	W/W		3417 0.655 2240 2.652 0.36544 35.351 0.3777			3384 0.828 2804 2.649 0.37816 35.351 0.3650			26 24.303 3361 0.933 3135 2.646 0.38841 35.351 0.3553			3348 1,004 3361 2,640 0,38841 35,351 0,3553			97 24,252 3392 0,798 2706 2,648 0,38841 35,351 0,3553			00 24.660 2654 2.873 7627 2.646 0.07125 35.351 1.9371			2415 3.412 6240 2.646 0.03610 35.351 3.8231		<b>89</b> 50	.07125		45 24.123 3468	.03600			24.662 2148 4.082 8769 2.556 0.04941 35.351 2.7936	:		65 24.647 2855 2.368 6763 2.690 0.07125 35.351 1.9371
11 611	S		2.652 0			2.649 0			2.646 0			2.640 0		*	2.648 0			2.646 0			2.646 0			2.648 0		٠	2.648 0			2.556 0			2.690 0
416.	VEL		2240			2804			3135			3361	-		2706			7627			6240			7637			8255	) ) )		8769	· •		6763
PT =	MACH VEL		0.655			0.828			0.933	•		1.004	•		0.798			2.073			3.412			2.870			3.411	,		4.082			2,368
5.2	SONV	0702	3417	•	3466	3384		3464	3361		3467	3348		3468	3392	i	3464	2654		3464	2415		3468	2661		3468	2420		3500	2140		3418	2855
9 MACH	MA MOLNT SONV		571 24.201	1	24.125	502 24.262		24.134	24.303		24.143	50 24.333 3348		24.123	24.252		24.134	24.660		24.134	99 24.662 2415		545 24.123	24.660		24.123	24.662	•	24.256	24.662		24.114	24.647
162.82	GAMMA	444	1.1571		1,1545	1,1602		1,1550	1,1626	  - 	1,1557	1.1650		1,1545	1,1597		1.1550	1,2600		1,1550	1,2799	;	1.1545	1.2595		1,1545	1.2794		1.1656	. 3025	: ::	1.1512	1,2365
TIME = 162				•	1858)	1758)		1855)	1729)		1858)	1711)		1860)	1767)								1860)	927)		1860)	733)		1696)	349		1804)	1115)
11	I	51 21	300,5(1799)	32 200	391.6(1858)	234.54	33 200	385.2	188.8	34 200	385,2(	159.46	35 6	394.10	247.8(1767)	36 5	385.2(	177.21 922)	37 5	385.2(	-971.7( 729)	38 5	294-1 (1860)	771.4(	39 80	394.1	10.796-	0	365.2(	1151.6( 549)	52	338.2(1804)	575,7(
BLOCK =	-	38	4913	6	5050	4818	9	5044	4750	41	5052	4710	42	5054	4839				3	5044	2260	45	5054		9		2271	3	5149	1758-	69	4922	3268
	۵	0 14		0		42,375	0	63.437	38,906		.410	38.906	REGEN	63,437	44.260		63,437	1.624	6		0.621		63.437		PO REGEN	_			189.527		NOZZLE	33,251	2,159
READING = 0093	•	COMBUSTOR	58.763	COMBUSTOR	60.773	60.773	COMBUSTOR	62,193	62,193	SONIC THROAT	62.193	62,193	COMBUSTOR	62.193	62,193	NOZZLE AE		٠	ڇ				67.269			87.269						87.269	87,269

00.000 00.0000 00.00	241E 1154E 1153E 037E
	334E 334E 342E 629E 270E 0
7-10-10-10-10-10-10-10-10-10-10-10-10-10-	1.241E-01 1.184E-01 1.153E-01 1.017E-01 7.057E-02
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READING = 0093 BLOCK = 71 TIME = 162,029 MACH 5.2 PT = 416,749 TT = 2112,3

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## REPRODUCIBILITY OF THE

READING = 0093 BLOCK = 71 TIME = 162,829 MACH	5.2	11 = 2112.3			PAGE
	RAMJET PERFORMANCE	. WANCE			
ENGINE PERFORMANCE			INLET		
CALCULATED THRUST	(LBF-SEC/LBM)	OF ATTACK LOW RATIO IVE DRAG COE! ING PRESSURE PTZ	Y EFFICIENCY		(DEGREES)
STREAM THRUST	(LBF) (LBF)	TOTAL PRESSURE RECOVERY - INLET PROCESS EFFICIENCY INLET PROCESS EFFICIENCY KINETIC ENERGY EFFICIENCY KINETIC ENERGY EFFICIENCY ENTHALPY AT PO - SUBSONIC ENTHALPY AT PO - SUBSONIC	SUBSONIC SUBSONIC SUBSONIC SUBSONIC  Y SUBSONIC	0.2859 0.9051 0.9182 0.9272 0.8942 -23.15 (81	(BTU/LBM)
A PLANTAGE			COMBUSTOR		
INLET PRICTION DRAGGER TO THE THREET MOMENTUM CHANGES TO THE TOWN TOWN CHANGES TO THE THREET MOMENTUM CHANGES TO THE THREET WOMENTUM CHANGES TO THE THREET FRICTION DRAGGER TO THE THREET TOWN DEALE FRICTION DRAGGER TO THE THREET TOWN DRAGGER TO THE THREET TOWN DRAGGER TO THE THREET TOWN DRAGGER TO THE THREET TOWN DRAGGER TO THE THREET TOWN DRAGGER TO THE THREET TOWN DRAGGER TO THE THREET TOWN DRAGGER TO THE THREET TOWN DRAGGER TO THE THREET TOWN DRAGGER TO THE THREET TOWN DRAGGER TO THE THREET TOWN DRAGGER TO THE THREET TOWN DRAGGER TO THE THREET TOWN SPECIFIC IMPULSE TO THE THREET TO THE THREET TOWN SPECIFIC IMPULSE TO THE THREET TO THE THREET TOWN SPECIFIC IMPULSE TO THE THREET TO THE THREET TO THE THREET TO THE THREET TO THREET THREET THREET TO THREET THREET TO THREET THREET TO THREET TH		FUEL-AIR RATIO		0.0308 0.706 1.500 0.3347 0.9280 0.9280 0.9286 0.8492 0.8492	
STATIONS		FUEL	FUEL INJECTORS		
NOMINAL COML LEADING EDGE	12 (12) 12 (13) 14 (13)	TORS	51ATION VALVE 40.400 41.278 46.300	·VĒ	
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t = 174.53 sec.

READING # 0093 BLOCK # 84 TIME # 174,529 MACH 5,2 PT # 417,499 TT # 2149,0 RAMJET PERFORMANCE

						or or	RAMJET M M A	PERF Y	ORMANCE R E P	۳ م				٠.			
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d INNE	 	I		GAMMA	MOLWT	SONV	MACH	VEL	s	4 / H	3	A/AC	MONTH	0	IVAC	PHI	ETAC
417,499	2149	417.96	545)	1.3186	29.269	2194 927	5.170	4795	1.766	0.14657	32.473	0.8450	6964	10,923	153.0		
1P NS 21.387 19,409	214 <b>9</b> 2099	417.90	545)	1.3186	29.269	2194	0.386		968	0.14657	32.473	. 865		06.	80		
NNEL 417.499 0.622	268	417.0		95) 1.3186 87) 47,3988	•	2194	194.		.766	: 7	33.910	0.890			528	٠	
4	2149 2094	417	545) 550)			~~	0.407			0.15306	91	865			52.		
THROAT 0 190,509 0 20,290	9 10	159.00 159.00	530)	1.3204	29.269	2168 1657	2.108	3494	1.812	1.13291	33.910	0.1149	4265	64,244	125.8		
	2096 1157	51.	530)	1.3204	29.269	2168	2,164	3546	1.812	1.07549	33.910	0.1231	4321	59.262	127.4		
119.252 119.252 98.508	2000	408	504)	1.3204	<b>29.269</b> 29.269	2160	0.544	1153	1.844	1.07549	33.910	0.1231	4321	19.272	127.4		
190°446 21.905	2096	403.8( 165.2(	530)	1,3204	29.269	2168	.2.061	3449	1.812	1.18289	33.910	o.iri9	4263	63.407	125.7		
159.486	2068		320)	1.3207	29.268	1740	1.659	3233	1.623	1.18562	33.910	0.1117	4135	59,574	121.9		
157.513	2087 1322	194.00	\$28) 321)	1.3207	29.269	2164	1.843	3216	1.824	1.18632	33.910	0.1116	4125	59,285	121.6		
153.097 26.464	2056 1340	000	3261	1.3208	327) 1.3208 29.269 326) 4.3545 29.268	2163	1.608	3175	1.826' 1	1.18733	33.910	0,1115	4102	58.582	121.0		
136.508 29.061	2075 1408	397.36	525) 344)	1.3211	29.269 29.268	215 <b>8</b> 1797	1.675	3009	1.832	1.17685	33.910	0,1125	4009	55.040	118.2		
125,229 125,229 29,492	2057	392.1	350)	# 3214 1.3492	29.269	2149	1.609	2914	1.836	1.13732	33.910	0.1164	3950	51,496	•		
124,030	2054	223.4	519)	1.3219	1.3219-29.269	2148	1.599	2899	1.836	1.13509	33.910	0,1166	3941	51,134	116.2		
121.406 30.124	144	390.01	354)	1.3220	29.269	2145	1.574,	2864	1.837	.837 1.13099	33.910	0.1171	3922	50,337	115.6		
121.289 30.107	2049 1445	390.06	\$17) 354)	1,3220	29.269	2145	1.574	2863	÷. 1.837 1	1.13013	33.910	0.1171	3921	50,291	115.6		
114,423 28,089		386.	514)	1.3225	29.269	2139	1.581	2864	1.839	1.06439	33.910	0.1244	3914	47.378	115.4		
112.41	2029 1361	384.46	512)	1,3227	29.269	2135	1.661	2959	1.639	.639.0.99067	33.910	0.1136	3984	45,554	116.6		

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		ŧ :		E E C		201	Z X X	VE L	n	<b>∢</b>	*	A/AC	NO N	9	IVAC	H	ETAC
	_	384.4(	512)	1,3227	29.269 29.268	2135 1781	1.661	2958 1	.839	0.99140	33.910	0.1335	3954	45.574	116.6		
12.000 2 21.132 1	•	22.5	510)	1,3530	29.269	2132	1.752	3062 1	839	0.92331	33.910	0.1434	4003	43.936	118.1		
	•	36. 186. 196.	310)	1.3231	29.269 2130 29.268 1718		1,835	3152 1	.839	0.85195	33.910	0.1554	6404	41.736	119.4		
08.695 2 16.246 2	-	1400 1400 1400 1400 1400 1400 1400 1400	508)	1.3233	29.269	2128 1695	1.898	3217 1	.839	0.79677	33.910	0.1662	4082	39.836	120.4		
	•	376.90 136.80	504)	1,3237	29.269	2122 1598	2,169	3467 1	1.832 0	1.67907	33.910	0.1950	4221	36.585	124.5		
77.231 8 F37.500 3	2061	1000 1000 1000 1000 1000 1000 1000 100	\$23)	1,330	29.167 2154 29.167*1980		1,089	2156 1	.077	.55855	34.030	0.2879	4565	18.718	134.2	0.01	1.00
	•	268.7	322) 445)		1,3210 29,187	2151	0.978	1965_1	1.879	0.53572	34.030	0.2480	† 9 9 †	16.356	137.1	5	8
	2566 2566	350		1.2923	26.423	2597 2505	0.738	1850 2	141	0.51067	34.387	0.2629	4766	14.683	138.6	25	0.49
58.224.5		26.92	742)	1,2922	26.425 26.425	2597 2505	0.738	1649 2	171.0	51028	34.387	0.2631	4768	14.666	138.7	0.25 0	•
_		200	1850	1.2863	26.564 26.564	<b>26</b> 40 2557	6.703	1799 2	.180 0	3.48255	34.387	0.2782	4926	13.490	143.3	0.25 0	.57
56,329	7 7	30.00	306	1.2836	26.790	2705	4.682	1793 2	3.	0.45237	34.387	0.2968	5122	12.604	149.0	0.25 0	69.
53,184 3 42,186 3		000 000 000 000 000 000 000 000 000 00	(1014)	1.2699	24.173	2930 2865	Ö.610	1748 2	415	0.36893	34.744	0.3677	5861	10.023	168.7	0.49	0.48
	• .•	100 100 100 100 100 100 100 100 100 100	(1078)	1,2698	24.175	2930 2865	0.610	1748 2	2.415 0	36866	34.744	0.3679	5863	10.015	168,8	0.490	94.
52.889 3 41.469 3	• ,•	342	(1110)	1.2649	24.270	29 <b>59</b> 2891	0.627	1612 2	421 0.	9929	34.744	.û 0.3689	5875	10.354	169.1	0.49	
	4	5 N		1.2636	24.295	2966		1810 2	.423	0.36499	34.744	0.3717	5902	10.266	169.9	0.49	•
	4 . 4	63	5(1419)	1.2634	24.299	2967	0.621	1801 2	422	0.36907	34.744	0.3675	5917	10,329	170.3	0.49	•
53.748 3	00 to 00 to	26	~~	1.2567	24.391	292	0.626	1632 2	427	0.36785	34.744	0.3688	5964	10.471	171.7	0.49	•
53.633 3	3573	95.1( 35.0(	1178)	1,2537	24.486	3016	0.635	1873 2	· 431 0	36716	34.744	0.3695	5998	10.690	172.6	0 64.0	0.58
	3768 3582	02.0( 25.6(	1247)	1.2417	24.709	3068 3001	0.651	1955 2	2.442	0.36146	34.744	0.3753	6091	10,984	175.3	0	99
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READING # 0093 BLOCK # 84 TIME # 174,529 MACH 5.2 PT # 417,499 TT # 2149.0

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	ETAC	0.74	98.0	0.92	1.00	9.65	3.92	3.92	95.0	3.92	00.1	3.92
	IVAC PHI ETAC	64.0	0.49	64.0	64.0	64.0	64.	6#*0	6#.0	64.0	64.0	64.0
	VAC	7.2	ຄ. ອ	ر د. د.	2.7	5.1 (	.7.	7.9	9.7 (	80 20	3.7	2.9
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	ø	11,51	14.34	16,29	17.86	17.03	7.34	4.70	7.39	4.68	7.20	6.59
	MOMTM	6157 11,516 177,2 0,49 0,74	6107 14,344 175,8 0,49 0,88	6064 16,297 174,5 0,49 0,92	6349 17.861 182.7 0.49 1.00	6084 17,036 175,1 0,49 0,92	7927 7.344 228.2 0.49 0.92	8214 4,700 236,4 0,49 0,92	7982 7,390 229,7 0,49 0,92	8279 4,687 238,3 0,49 0,92	8813 7,207 253,7 0,49 1,00	7397 6,594 212,9 0,49 0,92
	A/AC	0.3777	0.3690	0.3553	0.3553	0.3853	1.9372	3.1997	1.9372	3.2338	2.2884	1.9371
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1 = 214	4/4	.35916	.37166	38173	.38173	.38173	.07002	.04239	.07002	.04195	.05928	.07003
<u>-</u>	S	#51.j	162	162	654	1 69	3	162 (	. 99	891	367 (	503
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. 47.	VE	206:	248	274	301	287	674	7136	619	718	782:	605
P	MACH	0.677	0.802	0.888	0.967	0.926	1.961	3.391	2.951	3,388	i. 171	2.443
5.2	SONV	3117	3097	3198	3232	3213	\$198	3198	2213	3213 2122	3259 1876	3164
9 MACH	GAMMA MOLWT SONV MACH VEL S	24.948	25,355 25,396	25.465 25.520	25.689	25.515	25.465	25.465	25.450	25.450 25.585	25.742	25.462
IE = 174,529 MACH 5,2 PT = 417,499 TT = 2149.0	GAMMA	18) 1.2284 24.948 3117 13) 1.2375 24.963 3048 0.677 2063 2.451;0.35916 34.744 0.3777	14) 1.2051 25.355 3184 31) 1.2177 25.396 3097 0.802 2484 2.462 0.37166 34.744 0.3630	61) 1.1994 25.465 3198 57) 1.2146 25.520 3094 0.888 2747 2.462 0.38173 34.744 0.3553	24) 1.1871 25.689 3232 84) 1.2035 25.777 3115 0.967 3011 2.459 0.38173 34.744 0.3553	81) 1.1964 25.450 3213 %7) 1.2121 25.515 3101 0.926 2872 2.468 0.38173 34.744 0.3553	14) 1.1994 25.465 3198 18) 1.2994 25.565 2279 8.961 6748 2.468 0.07002 34.744 1.9372	54) 1.1994 25.465 3198 11) 1.3139 25.585 2104 3.391 7134 2.462 0.04239 34.744 3.1997	11) 1.1964 25.450 3213 33) 4.2976 25.585 2301 2.951 6791 2.468 0.07002 34.744 1.9372	31) 1.1964 25.450 3213 22) 1.3123 25.585 2122 3.388 7189 2.448 0.04195 34.744 3.2338	13) 1.1975 25.742 3259 15) 1.3114 25.872 1876 4.171 7823 2.367 0.05928 34.744 2.2884	27) 1.1982 25.462 3164 59) 1.2833 25.584 2480 2.443 6059 2.503 0.07003 34.744 1.9371
븰		623		(19) (37)	**************************************	66	100	54)	33)	181)	( S ( ) ( )	127)
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BLOCK #	٤.,	3769	4291	4044	454	401	4367	4367	2100	3 ~	1876	4278
	<b>a</b> .	53,535 40,612	53.506 36.637	53.917 34.031	58.266 34.031	53.917	53.917	53.917		53.917 0.622 MBUSTR	190,509 0,622	29.057
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READING = 0093	COMBIGACE	58.761 58.761	60.771	62.191 62.191 50NIC THR	62.191 62.191 COMBUS	62.191 62.191	87.267 87.267	87.267 87.267 87.267	87.267 87.267 NO22LF	87.267 87.267 FICTIV	62.191 62.191 FICTIV	87.267

20,00	000	0000	000	.451E-0	.445E-0	.263E-0	.162E-0	.804E-0	060F+0	.670E-0	.913E-0	.943E-0	- 446E-0	.386E-0	.105E-0	.234E-0	9 9	9	•	ė.	9	.0	Ö	o d	9 9	0	òά	, o	.183E-0	982E-0	9.753E+02	.923E-0	.010E-0	ė i	9	Ö	Ó.	5 5	ò	Ö	Ö.	ó	Ö
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0		0.00	0.00	9,736	7.45	5,540	7.79	1.211	2.05	2.462	2.626	2.646	2.040	2.94	2.084	8.277	0.174	8.172	8.024	8.013	1.682	2.962	3,002	0.00	3.323	364.6	3. 496 0. 947	2.500	2.136	6.027	9.544	6.658	6.774	6.778	6.780	6.780	6.781	6.782	6.752	6.654	6.02V	5.469	4.175
9	2 12 1	3 2	Ŋ.	8	200	80	8	200	2	20	05	8	3 2	2.70	8	20	9 0	10	02	8	3.5	18	8	N 0	20	8	200	8	200	20	200	9 6	3	35	: 5	05	25	5 6	10	20	200	120	8
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TT = 2149.0
PT = 417.499
MACH 5.2
= 174.529
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	in the second se	(LBF) (LBF) (LBF) (LBF) (LBF) (LBF) (LBF) (LBF)	ANGLE OF ATTACK  MASS FLOW RATIO
COMBUSTOR STRUT DRAG. COMBUSTOR MOMENTUM CHANGE. NOZZLE FRICTION DRAG. NOZZLE FRICTION DRAG. NOZZLE FRICTION DRAG. EXTERNAL PRESSURE INTEGRAL. TOTAL EXTERNAL DRAG. TOTAL EXTERNAL DRAG. TOTAL EXTERNAL DRAG. TOTAL EXTERNAL DRAG. TOTAL EXTERNAL DRAG. TOTAL EXTERNAL DRAG. TOTAL EXTERNAL DRAG. TOTAL EXTERNAL DRAG. FUEL VACUUM SPECIFIC IMPULSE -141.7, 0.	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		INJECTOR DISCHARGE COEFFICIENTS 0.8253, 0.6781, INJECTOR DISCHARGE COEFFICIENTS 0.8253, 0.6781, NOZZLE VACUUM STREAM THRUST COEFFICIENT — CS 0.9332 NOZZLE COEFFICIENT — CT 0.8686 KINETIC ENERGY EFFICIENCY 0.8508

t = 182.63 sec.

# 182.629 MACH 5.2 PT = 417.249 TT = 2140.8 RAMJET PERFORMANCE	SCREAR ANDORS	GAMMA MOLWT SONV MACH VEL S W/A W A/AC MOMTM G IVAC PHI ETAC	1.3188 29.269 2190 1.3987 29.248 925 5,170 4785 1.765 0.14694 32.549 0.8648 4970 10.927 152.7	1.3169 29.269 2190	1.3164 29.264 2190 ' 1.3986 29.266' 934 5/116 4777 1.765 0.15339 33.976 0.8648 5183 11.387 152.5	1.3189 29.269 2190 1.3208 29.269 2163 0.407 880 1.967 0.15339 33.976 0.8648 5182	1.3200 29.269 2163 1.3650 29.268 1650 2.118 3493 1.810 1.13601 33.976 0.1119 4267 64.381 125.6	1.3208 29.269 2163 1.3668 29.268 1631 2.173 3545 1.810 1.07804 33.976 0.1231 4323 59.384 127.2	1.3208 29.269 2163 1.3241 29.269 2116 0.542 1148 1.843 1.07804 33.976 0.1231 4323 19.227 127.2	1.3208 29.269 2163 1.3634 29.268 1666 2.071 3449 1.810 1.18570 33.976 0.1119 4265 63.557 125.5	1.3211 29.269 2159 ** 1.3570 29.268 1732 1.868 3234 1.821 1.18963 33.976 0.1115 4137 59.793 121.8	1.3211 29.269 2158 1.3565 29.268 1737 1.852 3217 1.822 1.18906 33.976 0.1116 4127 59.443 121.5	1.3212 29.268 1748 1.818 3177 1.824 1.19093 33.976 0.1114 4104 58.800 120.8	1.3216 29.269 2152 1.3514 29.268 1788 1.685 3013 1.830 1.17916 33.976 0.1125 4011 55.214 118.1	1.3223 29.269 2142 1.3502 29.268 1800 1.623 2921 1.833 1.14014 33.976 0.1163 3952 51.757 116.3	1 1.3224 29.269 2141 1.3500 29.268 1802 1.613 2907 1.833 1.13763 33.976 0.1166 3944 51.391 116.1	1.3225 29.269 2138   1.3495 29.268 1808 1.590 2874 1.834 1.13295 33.976 0.1171 3925 50.601 115.5	1.3225 29.269 2138 1.3495 29.268 1808 1.590 2873 1.834 1.13274 33.976 0.1171 3924 50.581 115.5	1.3230 29.269 2132 1.3504 29.268 1799 1;599 2877 1.836 1.06691 33.976 0.1243 3917 47.696 115.3	1.3233 29.269
5.2 PT = RAMJET	U K M A M Y A	SONV MACH VEL	2190 925 5 <sub>9</sub> 170 4785 1	0,386 836 1	2190 / 934 5/116	2190 2163 0:407 880	2163 1650 2,118 3493	2163 1631 2,173 3545	2163 2116 0.542 1148 1	2163 1666 2.071 3449	2169 */ 1752 1.868 3234	2158 1737 1,652 3217 1	2158 1748 1.818 3177 1	2152 1788 1.685 3013	2142 1800 1,623 2921 1	2141 1802 1.613 2907 1	2138 1808 1.590 2874	2138 1808 1.590 2873	2132 1799 11599 2877 1	#010 B
182,629			6.6(543) 1.3188 29 1.9(86) 1.3987 29	( 543) 1,3189 ( 529) 1,3206	6( 1843) 1.3189 8( 1877 1.3988	543) 1.3189	200	( 527) 1.3208 ( 276) 1.3668	( 527) 1.3200 ( 501) 1.3241	( 527) 1,320 <b>8</b> ( 290) 1,3634	( 525) 1.3211 ( 316) 1.3570	( 525) 1.3211 ( 318) 1.3565	7.0( 524) 1.3212 29 8.2( 323) 1.3554 29	3.9( 521) 1.3216 2.4( 340) 1.3514	( \$16) 1,3223 ( 345) 1,3502	7.5( 515) 1,3224 8.6( 346) 1,3500	96.0 (513) 1,3225 29.2(20.9(348) 1,3495 29.2(	(513) 1,3225 (548) 1,3495	68,4( 510) 1,3230 29,26 17,0( 344) 1,3504 29,26	(507)
EADING = 0093 BLOCK =		۵	1,249 2141 1,585 361	21.387 2141 19.407 2091	417.249 2111 0.622 367	1P NS 4 21.387 2141 19.203 2086	192.089 2085 20.154 1174	192.089 2085 18.395 1146	110 119,397 2085 3	110 192,019 2085 110 21,741 1198	160.774 26% 25.263 1301	353 158.615 2076 3 353 258.615 2076 3 353 25.542 3309 3	508 154.336 2074 3 500 26.257 1327 1 53USTOR	160 137,388 2063 39 160 28,777 1393 21	073 126.300 2644 V	50510K 125.081 2040 36 310 125.081 20416 21	786 122.451 2035 3 788 29.665 1425 2	800 122,390 2035 3 800 122,390 2035 3 800 29,669 1425 3	03107 0 17 10 60 115,659 2022 3 60 27,616 1410 2	510 113,747 2014 II

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COS   COS	æ•	3		34.604			34.604			34.604			34.604			34.604			34.604			34.604			34.604			34.604			34.604			34.604
COS   COS	r = 2140	4/4		3.35772			0.37017			38020			0.38020			3.38020			0.06975			0.04588			0.06974			0.04468			3.06917			0.06975
COS   COS	249 11	s		2,335 (			2.332			2.329 (			2.323	ř		2.344	٠.		2.329			2.329	~		2.344			2.344			2.230			2.363
COS   COS	417	VEL		2163			9459			1897			906			808			1286			5581			390			5714			1060			5673
COS   COS	PT ::	MACH		.731			£39			.923			000			.955			700			,372 (			.976			35.	į	κ.	244	:		505
COS   COS	5.2	NO:	1034	959 0		1028	930 0		1025	0 906		1026	884 1		990	942 0		1025	092 3		1025	952 3		9901	196 2		990	994 3		038	663 4		1961	265
COS   COS	MACH	OLUT S	.682	.704		. 489.	.711		. 686	.716 2		688	.720 2		.665	2 707.		686	. 739		. 686	.739		. 665	. 739 .		.663	. 739 1		704 3	739 1		.691	739
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18 0095 BLOCK 18	_	GAMIN	-	7		٦	ř			<u>۔</u>			_						1.313		1.221	1.326	·	1.214	2.309	•	1.214	1.322	r	1.228	1.354		1.223	1.299
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A	0093	۵	48.50	35,25	-	49.57	32.62				DAT	55,32	30.80	REGE	45		ِ نيو	50.45	-	0	50.42	0.62	E REGE	50.42		•	50,42	0.62	<b>DMBUST</b>	192,08	0.62	DZZLE	27.97	1.50
	ADING		1.763	3.763	510	1.773	27.	_	.193	.193	NIC THE	.193		_	2,193	2.193	SZZLE A	7.269	. (	o.	7.269	7.269	AZZLE A	7.269			7.269	1.269	CTIVE C	. 193	1.193			7.269

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P-18/P .242E .242E .083E	6.831E 00 6.834E 00 7.048E 00 7.039E 00	699E 305E 503E 496E 706E	3.145E 01 2.995E 01 3.181E 01 3.314E 01 3.836E 01 4.961E 01 5.242E 01	3,122E 01 4,978E 01 4,357E 01 4,364E 01 2,444E 01 2,782E 01 1,664E 01	••••••	.244 .903 .816
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CAMMA MOLWI SONV MALM VEL  13.407 26.406 1856 1.576 2010 1  16.55 237 1.3227 28.406 1856 1.576 2010 1  16.75 337 1.3228 28.406 2189 1.562 3035 1  16.75 348 1.3228 28.406 2189 1.745 3121 1  16.75 38 3 1.3228 28.406 2187 1.745 3121 1  16.75 38 3 1.3232 28.406 2187 1.745 3121 1  16.75 38 3 1.3232 28.406 2187 1.745 3121 1  16.75 38 3 1.3238 28.406 2183 1.749 1.745 3121 1  16.75 28 3 1.3238 28.406 2183 1.749 1.745 3121 1  16.75 28 3 1.3238 28.406 2178 2.008 3464 1  16.75 28 3 1.3238 28.406 2178 2.008 3464 1  16.75 28 3 1.3238 28.406 2178 2.008 3464 1  16.75 28 3 1.3238 28.406 2178 2.008 3464 1  16.75 28 3 1.3238 28.406 2178 2.008 3464 1  16.75 28 3 1.3238 28.406 2178 2.008 3464 1  16.75 28 3 1.3238 28.406 2178 2.008 3464 1  16.75 28 3 1.3238 28.406 2178 2.008 3464 1  16.75 28 3 1.3238 28.406 2178 2.008 3464 1  16.75 28 3 1.3238 28.406 2178 2.243 3015 1  16.75 28 3 1.3238 28.406 2178 2.243 3015 1  16.75 28 3 1.3240 28.406 2178 2.243 3015 1  16.75 28 3 1.3240 28.406 2178 2.263 3628 1  16.75 28 3 1.3240 28.406 2178 2.263 364 1  16.75 28 3 1.3240 28.406 2178 2.263 364 1  16.75 28 3 1.3240 28.406 2178 2.263 364 1  16.75 28 3 1.3240 28.406 2178 2.263 364 1  16.75 28 3 1.3240 28.406 2178 2.263 364 1  16.75 28 3 1.3240 28.406 2178 2.263 364 1  16.75 28 3 1.3240 28.406 2178 2.263 364 1  16.75 28 3 1.3240 28.406 2178 2.263 364 1  16.75 28 3 1.3240 28.406 2178 2.263 364 1  16.75 28 3 1.3240 28.406 2178 2.263 364 1  16.75 28 3 1.3240 28.406 2178 2.263 364 1  16.75 28 3 1.3240 28.406 2178 2.263 364 1  16.75 28 3 1.3240 28.406 2178 2.263 364 1  16.75 28 3 1.3240 28.406 2178 2.263 364 1  16.75 28 3 1.3240 28.406 2178 2.263 364 1  17.75 28 3 364 1  17.75 28 3 364 1  17.75 28 3 364 1  17.75 28 3 364 1  17.75 28 3 364 1  17.75 28 3 364 1  17.75 28 3 364 1  17.75 28 3 364 1  17.75 28 3 365 1  17.75 28 3 365 1  17.75 28 3 365 1  17.75 28 3 365 1  17.75 28 3 365 1  17.75 28 3 365 1  17.75 28 3 365 1  17.75 28 3 365 1  17.75 28 3 365 1  17.75 28 3 365 1  17.75 28 3 365 1  17.75 28 3 365 1  17.75 28 3 365 1  17.75 28 3 365 1  17.75 28 3 3	4	3	ċ	÷	•		<i>.</i>	•	•	ċ	ċ	÷	•	·	•	. o	·	0.3	6.0	
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READING 8 0094 BLOCK 8 33 TIME 8 134-142 MACH 5.2 PT 8 426-999 TT 8 2200.0

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REACING B OLGG BLOCK B 53 TIME B 134,142 MACH 5.2 PI	# 426.994 TI # 2200.0			PAGE
e c	RAMLET PERFORMANCE			
ENGINE PERPORANCE		INLET		
CALCULATED THRUST	A PARAMENT A PARAMENT	ANGLE OF ATTACK	00000000000000000000000000000000000000	(DEGREES)
STREAM THRUST	- HHXX MM - NY X HH - NY X CFF- - MM MM I I			(810/L8E)
		COFBUSTOR		
TALET FRICTION DRAG	FUEL + ALR PARTING TO THE PARTING TO THE PARTING TO THE PARTING TO THE PARTING TO THE PARTING TO THE PARTING TO THE PARTING TO THE PARTING		Male       Match       Match       One	
STATIONS		FUEL INJECTORS		
BPINE TRANSLATION:  INLET THROAT:  I	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	######################################		
F/11.70	•	DA - 37		

t = 140.44 sec.

READING = 0094 BLOCK = 40 TIME = 140.442 MACH 5.2 PT = 415.749 TT = 2245.2 Ramjet Performance

SURMARY REPORT

ETAC													٠					
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IVAC	157.5	161.8	157.4	157.4	129.3	131.1	131.1	129.3	125.4	125.1	124.3	121.5	119.6	119.3	118.7	118.7	118.4	119.6
ø	10.688	1.921	11.248	2.068		58.211	19,194	62,211	58.403	58.111	57.405	53,706	. 50.091	49.714	48.875	48.819	45.898	4.164
MOMTE	4958 1	5095	5125 1	5125		4269 5	4269 1	4210 6	#00#	4074 5	6 6 6 6 4	3956 5	3895 5	3885 4	3865 4	3865 4	3855 4	3895 44,164
A/AC I	0.8659	0.8659	0.8659	0.8659	0.1121	0.1234	0.1234	.1122	.1119	0.1118	.1116	.1128	0.1166	0,1168	0.1173	0.1173	0.1246	0.1338
š						0		0	•		•	0					0.1	.:
*	31.481	31.481	32.565	32.565	32.565	32.565	32.565	32,565	32.565	32.565	32.565.	32,565	32.565	32.565	32.565	32.565	32,565	32.565
W/#	3-14195	0.14195	8.14684	n.14684	1.09601	1.03068	1.03068	1.13361	1.13650	1.13716	1.13912	1.12725	90060-1	.08851	1.08432	1.08365	1.02069	0.95003
s	1.783 0	1.988	1.783	1.988		1.834	1.865	1.834	1.648	1.846	1.847	1.854	1.858 1	1.858 1	1.859	1.859	1.862	
VEL	4936	871	4929	906	3570	3634	1198	3531	3307	3208	3243	3866	2957	2939	2900	2899	2894	1667
M.ACH	5.170	0.390	5.127	904.0	2.069	2.136	0.548	2.031	1.631	1.815	1.778	1.642	1.569	557	532	.531	1,532	2206 1860, 1.609, 2991, 1.862
SONV	2257 955	2258	2257 961	2258 2230	2237 1725	<b>2</b> 237 1702	2237	2237 1738	2233	2233 1811	2232 1824	2227 1867	2219 1884	2217 1887 · 1	2215 1894 : 1	2215 1894_1	2209 1689	2206 1860.
VOL NT	28.866 28.866	28.866 28.866	28.866 28.86	28.8%6 28.8%6	28.866 28.866	28.866 28.866	28.866	28.866 28.866	28.866 28.866	28.866 28.866	28.866 28.866	28.866 28.866	28.866 28.866	28.866 28.866	28.866 28.866	28.866 28.866	28.866 28.866	28.806 28.806
GAVMA	3984	1,3179	1.3179	1.3179	1.3194	1.0194	1.3194	1,3194	1.3196	1,3197	1.3197	1.3201	1.3207	1.3208	1.3210	1.3210 2	1.3214 2	1.3216 2
J	12.	(2)	92)	1 1 1 1	689	62)	583	65) 16)	<b>63</b>	563) 1 347) 1	\$62) 1 353) 1	560) 1 372) 1	\$54) 1 380) 1	554) 1	552) 1, 384) 1,	52) 1 85) 1	49) 1 82) 1	47)
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۵.	415.749 0.583	21.125 19.131	15.749 0.612	NS 21.125 18.970	83.691 20.839	183.691 18.703	17.418 96.736	83.52 22.14	54.32	52.44	48.14	31.68	20.72 30.19	19.52	16.953 30.960	16.80 30.96	09.82 29.04	07.395 25.298
1	5 .			<u>.</u>	F .	Z	7 T	۲ ,	K	<u> </u>	K 1	<u> </u>	K .	<u> </u>	¥	¥ ,	,	٦,
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2																				
	ETAC	•		0.07	0.01		0.00	00.00	00.0	0.00	0.00	0.03	0.00	00.00	00.0	0.01	0.00	00.00	00.0	0.00
	H.	•		0.48	9,48		9,48	64.0	6.49	0.49	64.0	67.0	67.0	64.0	6.49	ď	64.0	64.0	64.0	64.0
	IVAC	119.6	121.1	119.0	119.0	ġ	122.7	126.1	126.8	127.8	28.6	129.4	31	131.1	131.2	131.3	131.5	131.6	132.0	132.2
	9	.166	.654	.634	. 665	.895	.677	.858	.882	.915	.100 1	.744	.783 1	.709	583	.938	900	900•	.781	353
	<u>.</u>	5 ##	5 42	6	14 0	39	4 32	1 28	4 27	5 26	61 26	9 24	5 19	7 20	50 20	52 19	8 20	3 20	5 19	20
	KOKTK	389	5965	392	393	3962	4004	4161	4204	423	426	428	404	464	435	4.05	4358	436	437	4380
	A/AC	n.133e	0.1436	0.1552	0.1554	0.1662	0.1950	0.2379	0.2480	0.2631	0.2782	0.2978	0.3678	0.3689	0.3717	0.3675	0.3686	U.3694	0.3753	0.3777
	<b>3</b>	565	.565	.029	.029	.029	.029	. 144	. 144	.144	.144	144	<b>3</b>	.144	.144	.144	.144	.144	#	33-144 (
45.2		32	32	7 33,	3	55	E P	33	S	3 33,	30	23	1 33.1	50	33	20	33	33	33.14	
7 = 224	4/4	0.94997	A.88544	6.8308	0.82979	0.77606	0.66]41	0.54400	6.52177	0.49183	0.46510	0.43573	A.35181	0.3507	0.34818	0.35208	0.35104	0.35031	n.34482	r.34262
6	.so	862	862	174	145	2.144	.140	151	181	152	154	172	2.167	.169	3	171	164	162	.161	.163
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3	H. VEL	9 2992	3	2 3224	9 3226	7 3508	3 31	5 341	ភ័	352	5 3611	5 365	3618	4 3799	1 3804	7 3644	2 3667	36	3 369	8 3822
2 PT	MACH	1.609	1.697	1.582	1.659	1.73	1.64	1.835	1.861	1.938	2.025	2.01	2.028	2.224	2.231	2.037	2.082	2.094	2.11	2.258
ñ,	SONV	2206 1860	2204 1827	2411	2342	2330 1905	2324 1935	2322	2518	2316 1817	2315 1783	2345 1813	<b>2</b> 317 1784	2313 1708	2313	2327 1789	2314 1761	2312 1755	2311	2310 1693
2 MACH	<b>VOLET</b>	28.866 28.866	28.866 28.866	24.473	24.342	24.323	24.320	24.212	24.207	24.207	24.207	24.264	24.215	24.208 24.208	24.207	24.232	24.210 24.210	24.207	24.207	24.207 24.20£
140.441	GAMKA	1.3216	1.3217	.3258	1.3325	3337	.3341	3847	3350	3351	3352	.3323	3349	3805	3354	1,3340	3352	1.5354	.3358	3356
띺	Ÿ	47) 1. 69) 1.	46) 1. 54) 1.	48) 1,	95) 1.	77) 1.	93) 1,	91) 1 58) 1	88) 1. 52) 1.	87) 1,	87) 1. 26) 1.	39) 1,	88) 1. 27) 1.	97) 1.	85) 1. 96) 1.	94) 1. 29) 1.	86) 17) 1.	85) 1, 15) 1,	84) 1, 12) 1,	83) 1, 91) 1,
Ξ		N IO	מו מו	• •	<b>4</b> 10	N IO	<b>M</b> 10	S	<b>10,50</b>	S P	(A) (A)	• 17	10 to	NO 61	10 N	. 2. 5. . 2. 5. 5. •	2 P	<b>S D</b>		
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18 +600	م	07.404 25.291	21.913	ຕິທີ	71.459	69.171 13.312	71.118	66.054 10.900	65.844 10.417	30	٥'n	ທ່ ຈ	÷ •	51.825			•	55.962 6.102	56.288	54.668 4.575
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ADING =	<b>5600</b>	BLOCK	04 =	TIME =	140.44	Z MACI	H 5.2	. P1	415.	1 672	140.442 MACH 5.2 PT = 415.749 TT = 2245.2	5.2							PAGE
	۵	-			GAMMA	SAMMA MOLET SONY	VNOS		MACH VEL	ď	W/A		A/AC	A/AC MOMTM	G	TVAC	TVAC PHT	CTAC	
MBUSTOR							•		!	)		3	•				:	; [	
.761	31,735			626)	1.3291	24,332	2376				3291 24,332 2376								•
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26.75	011111	0-3/62	.379E-0	387E-0	-407E-0	-480E-0	.518E-0	.527E-0	. S48E-0	\$49E-0	.861E-0	. 522E-0	.522E-0	476E-0	. 322E-0	.721E-0	.574E-0	.508E-0	.446E-0	.396E-0	. S60E-0	. 331E-0	0-34004	SACE	9455-0	4546-0	.278E-0	-344E-0	.226E-0	. 196E-0	X45F-0	318E-0	2.483E-03	. S31E-0	. 532E-0	4235-0 4885-0	1865-0	3205-0	.242E-0	.171E-0	.155E-0	.132E-0	.117E-0	.030E-0	.029E-0	-3866.	.972E-0	.962E-0	984E-0	.972E-0	.972E-0;
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HEADING = 0094 BLOCK = 40 TIME = 140,442 MACH 5,2 PT = 415,749 TT = 2245,2

## RAMJET PERFORMANCE

ENGINE PERFORMANCE				INIET		٠
		(LRF) (LRF) (LRF-SEC/LBM)	ANGLE OF ATTACK , MASS FLOW RATIO., ADDITIVE DRAG COLLIMITING PRESSURE			(DEGREES)
CALCULATED THRUST COEFFICIENT			DELTA PT2 TOTAL PRESSURE RE TOTAL PRESSURE RE INLET PROCESS FFF			(PST)
NE PERFO	MANCE			SUBSONIC	0.9302	
	5008. (LBF) -169. (LBF) -352. (LBF-S	(LBF) (LBF) (LRF-SEC/LBM)	KINETIC ENERGY EF ENTHALPY AT PO - ENTHALPY AT PO -	- SUBSONIC		(RTU/LBM) (RTU/LBM)
MOMENTUM AND FORCES				COMBUSTOR		
	117.7 (LBF) -965.7 (LBF)		FUEL-AIR RATIO EQUIVALENCE RATIC COMBUSTOR EFFICIE	EQUIVALENCE RATIO	0.487	
			TOTAL PRESSURE RA		0.2255	
			INJECTOR DISCHARE		 	
	676. (LBF) 706. (LBF)			NOZZLE		
			VACUUM STREAM THRUST		0.9735	
	5.99 (LBF) 5.99 (LBF) 1265. (LBF) -2764. (LBF)		NOZZEK CVEPPICIENY PROCESS EFFICIENCY KINETIC ENERGY EFF	ICIENCY	0.9140 0.9067 0.9422	
8.			·			
STATIONS				FUEL INJECTORS		
			INJECTORS 1A 18	STATION VALVE 40.400 41.266	V.	
	35.165 (IN) 73.505 (IN)		2 2 8	44,300		
			25			
	5.021		AS S	54.031 56.216		
COMBOS ON FALL	(NI) 120°C		<b>3</b>	44.766		

t = 150.34 sec.

## REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

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9.481 E86.0	162	7.00	۲.											•			
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6.953		UT.	136.	129.1	8.064	130.6	29.0	125.2	124.9	124.2	121.4	19.5	119.2	118.7	116.7	114.1	121.2
•	.919	1 984		. 648	300	. 455.1	465 1	.717	9250		. 054	.415	.055 1	.365.	.318 1	1 021.	470.
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0.8659	0.8659	0.8659	4598.0	0.1121	0.1634	0.1234	0.1122	0.1119	0.1118	0.1116	0.1128	0.1160	0.1108	0.1173	0.1173	0.1246	0.1338
31.740	31.790	55.104	33.104	35.104	35.104	35.104	33.104	53.104	33,104	33.104	33.104	33,104	35.104	35.104	33.104	35.104	35.104
.14354 3	4534	4927	.14927 3	1.10077 3	1.04774 3	1.04774 3	.15237 3	. 15531 .	1.15596 3	1.15798 3	.14591.3	.10810 3	.10053 3	.10427 3	. 10159 3	30	.96575 3
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Zb.866	26.000	26.666	26.666 28.666	24.866 24.866	20° 80° 80° 80° 80° 80° 80° 80° 80° 80° 8	26.066	28.866 28.866	20 : CO CO CO CO CO CO CO CO CO CO CO CO CO	28.866 28.866	28,866 28,666	28.866	26.466 24.466	26.666	28.066 28.666	26.066	26,866 20,860	26.666
1.3164	.3184	1,3164	1,3164	1,3203	1.3203	1.3204	1.3203	. \$206	1.3206	1.3207	1,3210	1.3495	1.3217	1.3486	1.3219	3564	3525
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READING B 0094 HLOCK B 51 TIME B 150.342 MACH 5.2 PT B 017.499 TI B 2250.0

## RANJET PERFURMANCE

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t = 157.54 sec.

PEADING # 1094 F	A C V CK	65 8	# !! !-	157.5	42 x 4C	, r	PT	# 417.	244 OFMAN	11 # 222 ice	R.9						
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걸급	1 2229 375	N E	\$73) 90)	1.3184	28.866 28.866	2250	5.170	4916	1.781	0.14331	31,783	9898.0	4863	30.948	156.9		
00 X X 00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2229 2177	429.16	573) 558)	1.3185	28.866	2225	0.388	A62	1.985	0.14331	31.783	98989	5147	1.420	162.0		
M 4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	222	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	573)	1.3184	28.866	2250	5.120	00 67	1.781	0.14912	33,073	0.8659	5183	11.374	156.7		
0.600 21 0.600 21	2229	444.00	973) 997)	1.3185	28.866 28.866	2222	0.407	<b>3</b> 00	1.985	0.14912	33.073	0.8659	5183	2.045	156.7		
N		0 427.5( 427.5(	556)	1,3204	28.866	2222	2.110	3583	1.827	1.10652	33.073	0.1121	4205	64.112	129.0		
0 - 10 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2171		556) 292)	1.3804	26.666 20.806	2228	2.170	3639	1.627	1.04675	33.073	0.1234	4352	59.194	130.7		
0.500 110.00.00.00.00.00.00.00.00.00.00.00.00.		427.51 399.61	556)	1.3205	28.866 -28.886	2222	0.543	1180	1.860	1.04675	33.073	0.1234	4362	19.201	130.7		
0 4 4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2171	487.60	554)	1.3204	26.006	2828	2.064	3540	1.027	1.15120	33.073	0.1122	7927	63.341	128.9		
COMBUSTOR 0 41.276 160.046			554)	1.3207	26,866	2216 1780	1.866	3322	1.838	1.15422	\$5.073	0.1119	4137	\$9.582	125.1		
14841 189 14841 189	2162	\$0.00 \$0.00	554) 336)	1,3207	28.866 28.866	2218	3		. :		•		;		: 6		
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04808708 4.061. 124 4.061. 29	W		\$45) 368)	1.3218	20.866 28.866	4203	1.506	2982	1.851	1.10705	53,073	0.1166	3947	51,307	119.3		
4,310 123	~ 5 5 ·		364)	1,3219	28 . 86 6 28 . 86 6	1860	1.594	2965	1.852	1.10548	34.078	941148	3937	50.936	119.0		
4.776	- 4 E		543)	1,3221	28.866 28.866	2199	1.569	2928	1.852	1.10123	33.073	0.1173	1917	50.115	110.4		
4-600 100.05 4-600 100.05 4-600 100.00	2124		543)	1,3221	28.866 20.669	2199	1.568	7927	1.855	1.10055	3.4.073	0.1173	3916	90.059	2 2 4 6 4		
6-260 113-57 6-260 26-23 6-260	2111	410.	540) 369)	1,3225	28.866 28.866	1400	1.573	2925	1,855	1,63640	33.073	3.1246	3908	121.121	118.2		
7.301		408.4( 223.7(	937) 355)	1.3228	28.856 28.065	2189 1869	1.654	3023	1.855	9.444Bu	51.0.73	0.1338	3949	45.325	1.0.		

PT # 417.249 TI # 2226.V

11rf a 157.542 16Cm 5.4

READING # 0094 BLOCK #

	ĸ	GAPPA	בייוסה .	) i.i.	3461	4.5	Ø	4/4	•	A/AC	rikan l	ěs.	TVAC	140	ETAC
408.4( 537) 1.3226 225.7( 355) 1.3521	<i>-</i> : .:	C -	28.856	2189 1 P 29	1,655	3023	1.855	0.46476	55.015	6.1338	5765	15.521	119.4		
40 6 20 6			28.866 28.866	2146	1,755	3144	1.854	3666.0	53.073	0.1436	4 0 0 S	185.57	121.1		
405.2( 534) 1,3232 192.4( 322) 1,3600	1,3232		26,466	2184	1.864	3263	1.653	0.83090	33.073	0.1554	<b>1</b> 907	42.140	122.9		
404.1(533) 1.3235 2 177.4(307) 1.3635 2	1,3235 2	กัด	8. cc 6.	2162	1.001	3364	1.851	0.77709	33.075	9.1662	4116	40.629	124.5		
400.7( 530) 1.3238 20 128.1( 257) 1.3757 20	1.3757 2	~ ~	8.856 8.866	2176	5,110	1041	, ,	0 0 4 4	11.02	. 4	F 3		\$		
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72.4( 547) 1.3211 2 19.2( 484) 1.3293 2	1,3211		26.786 26.785	2504	0.850	1778	1.895	0.52242	33,169	0848.0	48.2	14.437	145.5	20.0	1.00
422.01 623) 1.3019 367.11 769) 1.3072	1.3072	4 10	24.633	2648	9.0	1691	2.256	0.50035	33.642	. 2629	4000	12,687	144.5	8.5	0.31
422. 307.	1.3018 24	2.5	970	2574	0.644	1657	2.256	16667.0	33.692	0.2631	49.49	12,874	146.6	0.52	0.51
1 4 419.3	1.2960 24	3 3	765	2697	0.619	1626	2.267	0.47280	33,692	0.2782	5120	11,450	152.0	55.0	72.0
415.1( 953) 1.2634 25. 356.3( 897) 1.2688 25.	1.2888 25.	w w	050 051	2793	0.619	1697	2.249	0.40294	33.692	0.797.0	3344	11.413	158.6	9.52	9.0
444.6(1111) 1.2855 21 386.3(1058) 1.2900 21	1.2855 21	22	673	3044 2964	0.557	1650	8.878	0.36321	34.199	0.3676	6141	9.312	179.6	1.03	0.32
42.6(1112) 1.2853 21 86.1(1059) 1.2848 21	1.2855.1	~ ~	.070	\$0.65 \$965	0.557	1691	2.378	50505.0	54.199	0.3678	914	4.316	179.0	1.03	0.52
379.0(1119) 1.2621 21.	1.2704 21.	21.6	636	\$088 \$025	0.586	1773	2.903	0.36193	34.199	0.3689	6157	9.971	180.0	1.03	0.37
441.7(1 378.6(1	1.2864		999	3098 3033	n.586°	1777	2.595	0.35927	34.199	0.3717	6166	9.921	186.4	1.03	0 • XB
441=3(1174) 1.2776 21. 381-3f1116) 1.2826 21.	1.2776 21.	22.	828	\$083 \$050	0.574	1733	2.590	0.50329	34.149	6498*0	6207	9.785	181.4	1.03	92.0
4444-0(1,222) 1,2713 21.	1.2713 21.	22	943	312× 500°	ر. د. د. د.	1793	5.549	0.36222	34.199	7.4666	6254	14.1.95	144.4	10 of 10 of	5 5 6 6
36.9(1265) 1.2657 22 70.5(1194) 1.2715 22	1.2657 22	22	24.0	5161	x 2.5.0	1881	9,00.2	C. 56147	54.199	3 0 0 5	25.20	19.390	184.0	1,03	£ 0 €
35.5613667 1.2512 22 57.261253 1.2503 22	54 57 57 5 7 5 7 5 7 5 7 5 7 5 7 5 7 5 7	<b>~~</b>	٠ د <u>نا</u>	3239 3175	. 96.	. Q.	50000	0.5556	54.199	24/23	141	16.64R	1.80 • ¢	10.4	0.54

READTNG	7600	BLOCK	5.5	TIVE	# 157.5	345 SP	7 . Y	-	417.	249 1	57.542 .ACH 5.2 PT # 417.249 TT # 2724.9	•			٠				PARE	~
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BUAT	· 45	200	31				•	•	•	,							•			
				(1871)6	-	22.539	3297				2377 22,539 3297									
56.751	43			342.8(1373)	-	22.550	3227	0,651	2100	2.634	0.35393	34,199	1777	6462	11.537	6462 11.537 188.9 1.03 0.57	1.03	0.57		
	80		-	•	•											,	•			
60.761	*	4386		422.0(1616)	=	22,988	3389				2078 22,988 3389									
60.761	2		286	9(1503)	-	23.030	3298	0.788	2601	2,651	0.36584	34,199	0.1650	6407	4.785	6407 14.785 187.3 1.03 0.70	1.03	0.10		
COMBUST	5		2	*	•										•		1 1	•		
62.181	56.983		415	9(1653)	-	23,103	3405				1999 23,103 3405									
62.181		4169	247	247.7(1515)	_	23.165	3297	0.880	2002	2.653	0.37575	34.149	0.3553	6359	776.9	6359 16.944 185.9 1.03 0.74	1.03	0.74		
	ğ		34 2		•											•	•	•		
62,181		5011	415	115.9(1862)	_;	23,051	3490				1563 23,051 3490									
62.181	15,981	4	189	6(1717)		23,857	3371	666.0	3346	2,651	0.37575	34,199	0,3553	6852	9.653	6852 19,653 200,4 1,03 1,00	1.03	1.00		
COMBUST	6		5	•							•				•		•			
62,181			_	(0591)0		23.099	3409													
62.181	35.7	4173	~	\$1.6(1519)	_	23.165	3299	0.887	2927	2.654	2153 23.163 3299 0.887 2927 2.654 0.37575 34,199 4,3553	34,199	0.3553	6364	7.093	6364 17.093 186.1 1.03 0.74	1.03	0.74		
MOZZLE	¥		ž	3													•			
87.257	•			15.411691)	_	23.103	800K													
07.257		1 2104		-614.8( 695)	-	23.235	2420	2.966	7182	2.653	3009 23.235 2420 2,968 7182 2.653 0.06893 34,199 1.9372	34.199	1.9372	6300	7.693	8300 7.693 242.7 1.03 0.74	1.03	0.74		
MOZZLE	2			4									•			•				
87.257	80	t t 0		415,9(1651)	_	23.193	3405				1000 25.103 3605									
67.257	120.0	1753	_	66 568)	-	25.235	2223	3.424	7611	2.653	0.04051	34.199	3.2963	8614	4.791	8614 4.791 451.9 1.03 0.74	1.03	2.74		
3-1220N	¥	57		•											•					
87.257	<b>L</b>	1 4503	423	423.0(11659)	-	23.099	3409						1041 ଅଧାରତ୍ର ଅଧାରତ୍ର							
158.10	:	2114	-610	10.8( 699)	-	23.235	2426	2,965	7192	2.654	0.06893	34.199	1.9372		7.704	7,704 243,1 1.03 0.74	1.03	0.74		
NOZZLE	0	9	2		,							i i	1							
67:257		4505	423	0(1659)	-	23.000	\$409				1001 23.000 3400		•							
87.257		1761	-739	39,0( 571)	1.3164	23.235	2227	3,424	7625	2.694	0.00040	34.190	3.5047	0631	4.788	8631 4.788 252.4 1.03 0.74	1.03	5.74		
FICTIVE		99	-	•	•	•		ı				•	•		•	-  -  -  -				
62.181	190.976	5	ਕ	•	_	23.775	3537				1667 23,775 3537									
62.181		_	-1133	33.1( 538)	-	24,226	2141	4,112	F.B.C.4	2.558	0.05019	34.199	2.6608	9761	6.867	9781 6.867 286.0 1.03 1.00	1.03	000		
FICTIVE		Ş	~												•	<b>;</b>				
47.297		4393	374.7	7(1612)	-	23.100	3369						100 000 000 000 000 000 000 000 000 000							
87.257				_	-	23.235	2637	2.441	6434	2.697	10.06893	34.199	1,6371	7738	6.897	224.1	10.0	7.34		

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6.751	46.636	7065	410,961	(1862)	1,2561	25.436	3074				1.2581 25.436 3074								•
_	35.287	3665	314.8	(1174)	1.2483	25.449	0667	0.733	2192	2,390	0.34794	33,619	0.3777	5704	5704 11,839 169,7 0,59 0,80	169.7	0.59	09.0	
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0.761	44,273	3	403.8	(1319)	1.2271	25.649	3111				1.2271 25.649 3111				•				
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2,101	44.826	4110	398.9	(1333)	1.2243	25.712	5119				1.2243 25.712 3119								
2.101	30.694	3756	251.8	(1202)		25.743	2999	500.0	2713	2.394	0.16938	33.619	15533	5629	5629 15.575 167.4 0.59 0.90	167.4	9.0	06.0	
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2,181	52.610	4512		(1404)	1.2104	454.62	3162				1.2104 25.454 3162								
-	30.694			(1884)	1.2206	20002	3035	096.0	2913	2,393	0.36938	33.619	0.3553	5638	5638 16.724 173.6 0.59 1.00	173.6	0.50	1.00	
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2,101	49.826	4823	•	(1375)	1.2179	25.694	3159				1.2179 25.604 3155								
2,181	21.964	3627		(1155)	1.2052	25.749	2953	1.193	3524	2.406	0.36958	33.619	1983	5682	5682 20.232 169.0 0.59 0.90	169.0	05.0	06-0	
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7.257	49,626	3		(1325)	1.2243	25.712	3119												
_	1.152	1832		( 926 )	1.3150	25.768	2156	2.997	6460	2.394	1.3150 25.768 2156 2.997 6460 2.394 0.06776 33.619 1.9371	33.619	1.9371	7322	7322 6.803 217.8 0.59 0.90	217.8	0.50	0.0	
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7.257	989.67	4110	396.9	(1325)	1.2243	25.712	3119				1.2243 25.712 3119								
7.257	0.621	1576	-516.3	(454)	1.3279	25.768	2010	3.367	4767	2.394	97990.0	33.619	2.9523	7541	7541 4.676 224.3 0.59 0.90	220.3	95.0	0.0	
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7.297	49.626	4223	449.2	(1375)	1.2179	25.694	3155				1.2179 25.694 3155								
7.297	1 . 100	1916	-400-	561)	1-3112	25.768	2201	2.975	6550	2.406	0.06776	33.619	1.9371	7434 4.897 221.1 0.58 0.90	4.897	221.1		00.0	
OZZCE PO		70	9	į			,	•	1		)· · · · · · · · · · · · · · · · · · ·								
7:257	49.62	4243	440.2	(1375)	1.2179	25.694	3155				1.2179 25.694 3158								
7.257	0.621	1638	16.9670	( 473)	1.3246	25.768	2046	1.363	6661	404.5	0.04350	31.619	3.0176	7470	7670 4.651 228.1 0.50 0.90	228.1	9.50	00.0	
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	191.541	1757	398.9	(1414)	1.2202	25.985	3183				1.2202 25.985 3183								
	0.021	1216	-714.7	( 341)	1.3474	20.050	1768	4.221	7465	2.294	0.06426	33.619	2.0426	6125	6125 7.455 241.7 0.59 1.00	201.7	0.50	1.00	
-	37226	60	9			) ;	), ),						k		1				
7.257	26.920	407	362.1	(1204)	1.2248	25.713	3044						经银色银 经工作分割 医牙宫韧带						
	1.544	2206	-312.1	( 657)	1.2993	25.766	2352	2.470	8008	2.432	0.06776	11.619	1.0371	4416	4.117	205.1	95.0	0-0	

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t = 214.24 sec.

Test cell pressure was high which resulted in increased pressures in the AIM nozzle.

IVAC PHI ETAC

READING = 0094 BLOCK = 122 TIME = 214,242 MACH 5,2 PT = 299,750 TT = 2917,7 RAMJET PERFORMANCE

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	<b>4/</b>		617 25,022 2992	.21418 2			874 25.048 2722 1.302 3545 2.405 A.21999 20.022 0.3553			972 24.892 2632 1.401 3687 2.398 0.20852 20.022 0.3749		658 24,957 2967	.19386 2		600 24.952 3014	.19386 2			476 24.966 1964 3.022 5934 2.410 6.04036 20.022 1.9378		658 24.957 2967	.03251 2		606 24.95g Jolt	2 98040-		600 24.952 3014	203170 2			1839 4.172 7653 2.325 A.04289 20.020 1.8225		277 24.376 2386	.04036 2
	S			406			405			398			410			424	!		014.			.410			424			424			325			.236 0
	Ę,			15 2			4 5 2	) )		87 2			179 2			48 2			34 2			182 2	:		2 95	1		207 2			53.2	1		33 2
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	Ĭ			1.3			1.3			1.4		:	1.3			1.2			3.0			3.2	٠.	٠.	2.0			3.2			4.1			3.0
	SON		2992	2706		2994	2722	]    -	2948	2632		2967	2679		3014	2746		2967	1961		2967	1887		3014	2014		3014	1928		3239	1834		2386	1499
	MMA MOLINT SONV MACH VEL S		25.022	25.032		25.038	25.048		24.886	24.892		24.957	24.965		24.952	24.964		658 24.957 2967	24.966		24.957	24.966		24.952	24.966		24.952	24.966		26.191	419 26.309 1834		24.376	24.376
	GAMMA		1.2617	1.2889	,	1.2611	1.2874	•	1.2698	1.2972	,	1.2654	1.2923		1.2600	1.2867		1.2658	1.3476		1,2658	1,3543	:	1.2600	1.8431	,	1.2600	1.3507		1,2073	1.3419		1,3277	1,3905
			135)	198		138)	197		(1086)	122)	ı	107	861)		.2(1154)			104)	418)		104)	380)	`.	154)	440)		154)	398)		-	369)		633)	226)
	I	m	582,8(1135)	21.5	n	BO.6(1	29.8	3	₹	•	*	3	3	n	25.2(1	73.6(	36 0	575.6(1104)	20.04	n	75.6(1	63.7(	<u>.</u> د ا	25.2(1	03.01	39 85	28.2(1	16.94	0	75.6(1	14.76	0	420.8	
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	F	38	3570						3 342	7 267	9 41	1 340																				67	2103	79
	٩	J	29,187	10.462	J	29.559	11,100	J	28.77	9.390	_	26,121	9.38	REGEN	26.12	9.956	AE	26.121	0.605	0	26.12	0.43	E REGEN	26.12	0.624	O REGEN	26.121	0.437	OMBUSTE	128,120	0.43	022LE	29,317	0.744
		<b>GMBUSTOR</b>	0.759	0.759	<b>GMBUSTOR</b>	2.179	2.179	OMBUSTOR	649.4	649.4	OMBUSTOR	5.019	5.019	CMBUSTOR	5.019	5.019	IOZZLE A	7.255	7.255	OZZLE P	7.255	7.255	OZZLE A	7.255	7.255	OZZLE P	7.255	7.255	ICTIVE C	5.019			7.255	

2917.7

11

299,750

PT =

5.5

TIME =

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₩600 =

READING

EAUING = 0094	) 	<b>*6</b> 00	groc <sub>l</sub>	 	GLOCK = 122	T I M	TIME = 214.2	4.242	MACH	5.2	PT = 299.750	. 66		"	TT = 2917.7						PAGE 5
XABS		P-18	<b>6</b> 0	_	P-08		PDA		X00		Q-1B		0-0H		CAWALL		P-18/PS0	0	P-18/P10	P-08/PS0	P-08/PT0
5.506E	0	9.57			.101E		•	0	-1.822E	30	-8.567E	02	-9.65nE	02	4.342E	03	2.192E (	=	3.194E-02	2.084E 01	3.036E-02
5.526E	70	9.10			.962E		•	5	-1.829E	S	-8.589E	3	-9.7018	E 02	4.368E	20	2.085E	=	3.037E-02	2.052E 01	2.990E-02
5.692E	5	5.20			.800E			6	-1.881E	03	-8.752E	_	-1.006	9	3 4.584E	03	1.191E	=	1.735E-02	1.328E 01	1.935E-02
6.759E	5	3.97			.317E			80	-1.899E	03	-8.808E	_	-1.018E	6	4.665E	03	9.104E	9	1.327E-02	1.218E 01	1.774E-02
6.836E	0	2.570E		* 00	4.17E	8	2.396E	02	-1.920E	6	-8.867E	_	-1.034E	ю ы	3 4.760E	60	5.884E	9	8.5746-03	9.563E 00	1.393E-02
6.908E	5	3.19			.110E			05	-1.942E	30	-8.919E		-1.05AE	, 0	3 4.848E	03	7.316E	9	1.066E-02	7.121E 00	1.038E-02
969E	5	3.72			.408E			02	-1.959E	93	-8.961E	0	-1.063E	3	3 4.922E	03	8.529E	9	1.243E-02	5.514E 00	8.034E-03
7.064E	5	3.50			•315E			05	-1.976E	8	-9.027E	_	-1.073	S = 0	3 5.036E	03	8.024E	2	1.169E-02	3.011E 00	4.387E-03
7.107E	5	3.40			.839E			90	-1,981E	8	-9.056E	_	-1.076E	20	5.088E	50	7.796E	9	1.136E-02	4.211E 00	6.136E-03
7.260E	5	3.91			.70SE			05	-2.012E	3	-9.147E	05	-1.097E	9	3 5.273E	03	8.964E	9	1.306E-02		1.236E-02
7.275E	5	3.96			.717E			05	-2.016E	3	-9.154E	_	-1.1006	8	5.290E	20	9.078E	9	1.325E-02	8.512E 00	1.240E-02
7.350E	5	50.3			. 780E			80	-2.039E	3	-9.191E	-	•	30	3 5.374E	2	9.380E 0	9	1.367E-02	8.655E 00	1.261E-02
7.350E	5	3			.780E			0.5	-2.039E	3	-9.191E	9		03	5.375E	03	_	00	1.367E-02	8.656E 00	1.261E-02
7.4835	5	4.0			000		· 9.252E	<b>%</b>	-2.085E	8	-9.247E	_	-1,161E	8	_	3	9.914E 0	9	1.445E-02		00000
7.768E	6	4.00			000		1.104E	03	-2.09SE	6	-9.341E	_		93	5.525E	6	1.653E 0	=	1.535E-02		00000
8.158E	5	4.7	_		000		1.304E	0	-2.104E	3	-9.429E	0	-1.161	_	5.630E	2	1.093E 0		1.593E-02		0000
9684 B	5	5,07	025E 0	8	000		1.4136	03	-2.111E	8	-9.505E	05	-1.161	E 03	3 5.684E	20	1.151E 0	=	1.676E-02		0000
B. 725E	5	5.7	_		000		1.543E	0	-2.12SE	3	-9.646E	80	+1.161E			ຣ	1.315E 0	<u>-</u>	1.917E-02		0000
B.725E	5	5.74	-		• 000		1.543E	03	-2,125E	03	-9.646E	2	-1.161E	20	5.707E	63	1.316E 0		1.917E-02		000*0

## REPRODUCIBILITY OF THE ORIGINAL PAGE

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4.040E 01 1.319E-01 9.652E 01 2.566E-03 3.491E-02 4.040E 01 1.319E-01 1.099E 02 2.681E-03 3.491E-02 4.139E 01 1.319E-01 1.1009E 02 2.005E-03 3.990E-02 4.139E 01 1.329E 01 1.1009E 02 2.005E-03 4.0050E-02 4.139E 01 1.209E 01 1.251E 02 2.005E-03 4.0050E-02 4.139E 01 1.209E 01 1.251E 02 2.005E-03 4.0050E-02 4.491E 01 1.209E 01 1.251E 02 2.005E-03 4.0050E-02 4.491E 01 3.004E 00 1.490E 02 2.005E-03 4.0050E-02 4.497E 01 3.135E-01 1.109E 02 2.005E-03 4.005E-02 4.491E 01 3.135E-01 1.109E 02 2.005E-03 4.005E-02 4.491E 01 3.135E-01 1.109E 02 2.003E-03 4.005E-02 4.497E 01 3.135E-01 1.109E 02 2.492E-03 3.100E-02 4.491E 01 1.109E 02 2.492E-03 3.100E-02 4.491E 01 1.109E 01 1.209E 02 2.492E-03 3.100E-02 4.491E 01 1.109E-01 1.209E 02 2.492E-03 3.100E-02 4.491E 01 1.209E 02 2.492E-03 3.100E-02 4.491E 01 1.209E 01 1.209E 02 2.492E-03 3.100E-02 4.491E 01 1.209E 01 2.492E 02 3.492E-03 3.100E-02 5.492E 01 1.209E-02 5.492E-03 3.100E-02 5.492E 01 1.209E-02 5.492E-03 3.100E-02 5.492E 01 1.209E-03 5.492E-03 3.100E-02 5.492E-03 1.109E-03 5.492E-03 1.109E-03 5.492E-03 1.109E-03 5.492E-03 1.109E-03 5.492E-03 1.109E-03 5.492E-03 1.109E-03 5.492E-03 1.109E-03 5.492E-03 1.109E-03 5.492E-03 1.109E-03 5.492E-03 1.109E-03 5.492E-03 1.109E-03 5.492E-03 1.109E-03 5.492E-03 1.109E-03 5.492E-03 1.109E-03 5.492E-03 1.109E-03 5.492E-03 1.109E-03 5.492E-03 1.109E-03 5.492E-03 1.109E-03 5.492E-03 1.109E-03 5.492E-03 1.109E-03 5.492E-03 1.109E-03 5.492E-03 1.109E-03 5.492E-03 1.109E-03 5.492E-03 1.109E-03 5.492E-03 1.109E-03 5.492E-03 1.109E-03 5.492E-03 1.109E-03 5.492E-03 1.109E-03 5.492E-03 1.109E-03 5.492E-03 1.109E-03 5.492E-03 1.109E-03 5.492E-03 1.109E-03 5.492E-03 1.109E-03 5.492E-03 1.109E-03 5.492E-03 1.109E-03 5.492E-03 1.109E-03 5.492E-03 1.109E-03 5.492E-03 1.109E-03 5.492E-03 1.109E-03 5.492E-03 1.109E-03 5.492E-03 1.109E-03 5.492E-03 1.109E-03 5.492E-03 1.109E-03 5.492E-03 1.109E-03 5.492E-03 1.109E-03 5.492E-03 1.109E-03 5.492E-03 1.109E-03 5.492E-03 1.109E-03 5.492E-03 1.109E-03 5.492E-03 1.109E-03 5.492E-03 1.109E-03 5.492E-03 1.109E-03
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READING = 0094 BLOCK = 122 TIME = 214,242 MACH 5,2 PT = 299,750 TT = 2917,7

ENGINE PERFORMANCE

# RAMJET PERFORMANCE

INLET

MEASURED THRUST	-2384. -5790. -338. -821. -0563	(LBF) (LBF) (LBF-SEC/LBM) (LRF-SEC/LBM)	ANGLE OF ATTACK MASS FLOW RATIO. ADDITIVE DRAG CC LIMITING PRESSUR DELTA PTESSURE R TOTAL PRESSURE	ANGLE OF ATTACK	0.000 0.000 0.0110 0.2655 0.0947 0.4274	(PSI)	
REGENERATIVE-COOLED ENGINE PERF. STREAM THRUST	PERFORMANCE 73604 72483 1352	(LBF) (LBF)		FFICIENCY SUPERSONIC FFICIENCY SUBSONIC EFFICIENCY SUPERSONIC EFFICIENCY SUPERSONIC EVPERSONIC SUPERSONIC	<del>-</del>	(BTU/LBM)	
MOMENTUM AND FORCES				COMBUSTOR	<i>‡</i>		
•	100 400 600 600 600 600 600 600 600 600 6		FUEL-AIR RATIO EQUIVALENCE RATI COMBUSTOR EFFICI TOTAL PRESSURE R COMBUSTOR EFFECT INJECTOR DISCHAR	FUEL-AIR RATIO	0.0161		•
TRESTOR INTEGRAL  L PRESSURE INTEGRAL  XTERNAL DRAG  TRUT DRAG  TRUT DRAG  TRUT DRAG  TRUT DRAG  TRUT DRAG  TRUT DRAG  TRUT DRAG  TRUT DRAG  TRUT DRAG  TRUT DRAG  TRUT DRAG  TRUT DRAG  TRUT DRAG  TRUT DRAG  TRUT DRAG  TRUT SPECIFIC IMPULSE  TRUT SPECIFIC IMPULSE	24.00 24.10 24.10 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 24.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00 26.00		VACUUM STREAM THRUST NOZZLE COEFFICIENT PROCESS EFFICIENCY KINETIC ENERGY EFFIC	TREAM THRUST COEFFICIENT ~ CS  OEFFICIENT ~ CT  EFFICIENCY  ENERGY EFFICIENCY	1.1897 1.1183 0.9067 0.9428		
STATIONS				FUEL INJECTORS			
NOMINAL COWL LEADING EDGE SPIKE TRANSLATION INLET THROAT COWL LEADING EDGE NOZZLE SHROUD TRAILING EDGE STRUT LEADING EDGE STRUT LEADING EDGE COMBUSTOR EXIT	34.884 40.2739 40.2739 36.160 73.550 76.550 65.019 65.019	SURVESSE	INJECTORS 18 18 10 20 20 38 38	STATION 4U.400 41.264 44.306 46.250 56.214 44.764	VALVE		

t = 215.14 sec.

Test cell pressure was high which resulted in increased pressures in the AIM nozzle.

FTAC

7 1

IVAC

TIME = 215.142 MACH 5.2 PT = 292.500 TT = 2918.9 RAMJET PERFORMANCE BLOCK = 123 READING = 0094

7.169 182.5 1,145 196.2 7.811 182.0 1.390 182.0 2896 43.848 148.0 2934 39,926 149,9 2934 12.915 149.9 3265 3511 3561 3561 MOMIN 28.866 2518 28.866 1942 2.133 4142 1.932 0.62297 19.566 0.1121 2518 2467 0.544 1347 1.964 n.61928 19.566 0.1234 2553 1106 5:171 5717 1.863 0.08068 17.894 0.8659 2553 2530 0.361 913 2.090 0.08068 17.894 0.8659 2553 1126 5.058 5697 1.883 0.08823 19.566 0.8659 28.866 2553 28.866 2525 0.402 1814 2.090 0.08823 19.566 0.8659 28.866 2518 28.866 1939 2.139 4149 1.932 A.61928 19.566 0.1234 A/AC REPORT ۷/ ۲ n 7 SUMMARY MACH MOLIT SONY 28.866 28.866 28.866 28.866 1.2418 1,2961 1,2960 1.2961 1.2960 1.2988 1.2988 GAMMA 407) 127) 772) 756) 406) 712) 747) 747) 747 747) 629.5 54**6.2**( 620.6( 277.8( 646.2( 646.2 620.6 620. **5**64. 20. 14.725 2919 2919 13.543 2863 0.400 127,982 2834 0.400 13,132 1631 127,982 2834 0.383 67.023 0.000 298.500 128,632 VLET UPNRSK IIND TUNNEL 004.0

2826 40.795 148.4 2820 40.643 144.1 2717 36.107 138.9 2895 42,757 148.0 2806 40.274 143.4 2755 38.317 140.8 2710 35,841 138,5 2694 35,250 137,7 2687 33,116 137.3 2694 35.210 137,7 2719 31.870 139.0 28.866 2476 28.866 2051 1.752 3593 1.952 0.57082 19.566 0.1338 2512 2029 1.894 3844 1.940 0.68286 19.566 0.1119 2512 2033 1.882 3828 1.940 0.68326 19.566 0.1118 20.866 2492 28.866 2085 1.702 3547 1.949 0.65495 19.566 0.1166 28.866 2487 28.866 2096 1.660 3480 1.950 0.65111 19.566 0.1173 28.866 2088 1.664 3475 1.953 N.61328 19.566 0.1246 2518 1976 2.045 4039 1.932 n.68112 19.566 0.1122 2511 2044 1.853 3786 1.942 0.68443 19.566 0.1116 2504 2076 1.754 3640 1.947 0.67730 19.566 0.1128 2490 2088 1.689 3526 1.949 n.65402 19.566 0.1168 28.866 2987 28.866 2096 1.661 3482 1.950 0.65151 19.566 0.1173 28.856 28.866 28.866 20.066 28.866 28.866 1.5555 1.3007 1.3016 1,3019 1.2988 1.2342 1.2992 1,2998 1.5009 1.3011 1,3011 721) 743) 738) 729) 726) 726) 718) 453) 458) 461) 424) 744) 451) 743) 728) 246.0 616. 321. 5 13 2772 1897 16 2760 1880 1903 1693 2 1.276 112,319 1.500 108.516 18.750 15,583 18.728 18.894 19.211 15,280 111,175 91.057 89.971 OMBUS TOR SMBUSTOR COMBUSTOR

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	IVAC	139.0	140.9	138.5 (			143.0 0	147.0 6	83	150.5 0	53.6	157.8 B	174.5 0	174.7 0	175.3 0	175.7 0	176.7	177.5 0	179.8 0	181.6 0
	. 9	31,872	30.745	8.865	28.844		22.633	9.734	7.580	4,839	2,278	11.214	8.856	690.6	8.977	8,921	8.901	8.757	8.089	7.766
	MONTR	2719 3	2756	2751 2	2751 2	2775	2841 2	2938 1	79	3007 1	3068 1	3154 1	3486	3491	3563	3510	3531	3547	3593	3628
	A/AC	1338	1436	1552	.1554	*	.1958	.2379	.2480.	.2631	.2782	.2970	.3678	.3689	.3717	.3675	.3686	±69€•	.3753	1115.
_		9.566.0	0.566 0	3.868 0	0.868.0	. 868 0	0.868.0	9.981 0	0.981 0	9.981 0	0.981 0	.981 0	9.981 0	.981 0	0.981 0	.981 0	9.981 0	0.981 0	0.981 0	19.981 0
= 2918.9	#/ <b>#</b>	78 1	.53201 19	61 08664.	49915 1	.46683 19	.39786 19	.32796 1	.31455	.29651 1	.28039 19	.26269 19	.21210 1	.21146 19	.20990 1	.21225 19	.21163 1	.21119 19	.20788 19	0.20655 19
500 11	s	1,952 0	1.951 0	2.281 h.	2.257 0.	2.256 0	2,253 0	0 772.2	2.325 0	2.365 0	2.387 0	2,401 0	2,439 0	2,440 0	2.441 0	2.439 0	2.439 0	2,438.0	2.437 0	2.435 0
29P.	VEL	3593	3719	3716	3718	3834	3661	3872	3896	3220	2818	2747	2687	2760	2752	2704	2707	2668	2504	2419
PT =	F.ACH	1.752	1.850	1.655	1.722	1.817	1.700	1.828	1.521	1.233	1.016	0.961	0.869	0.892	0,887	0.869	0.870	0.857	0.801	0.773
5.2	SON	2476	2473	2672	2611	2599	2595	2614 2118	2738	2868	2950 2775	2011	3190	3197	3202	3208	3208	3207	3206	3205 3129
. KACH	FOLKT	28.866 28.866	28.866 28.866	24.176 24.176	24.038	24.017	24.017	23.894	24.186 24.186	24.543	24.818	25.054	25.977	26.027	26.063 26.143	26.108 26.191	26.109 26.192	26.110 26.191	26.112 26.184	26.116
215,142	GAMMA	1.3019	1.3022	1.3384	1.3160	1.3172	1.3474	1.3160	1.3280	1.2846	1.2872	1.2591	1.1997	1.1963	1.1938	1.2060	1.2062	1.1913	1.1917	1.1922
TINE #		718)	716)	823) 549)	5000	766)	163)	478)	622)	795)	1084)	(1155)	(1431)	1445)	(1888)	(1355)	(1384)	(1387)	(1465)	1463)
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. 215.14	GAMMA MOLET SONV MACH VEL S		1.1933	1,2081		-4	-	1	-	-		-	-		-	1.2143		1.1936	1.2990	,	1.1936	1,3103		1.1857	1.2945		1.1857	1.3065	1	1.2084	1.3425		1,2138	1.3580
1 1 ME			1458)	1247		14561	1319)	:	1449)	1256)		1447)	1259)		3.9(1492)	1287)		1426)	6373		1426)	549)		1492)	676)		1492)	577)	•	1467)	366)		1.8(1457)	1967
C21 =	I	51 200	576.5(1458)	400.00	32 200	572.2(	398.2	33 200	564.7(1449)	323.6(	34 200	563.80	327.6(	35 3	628.9(	362.7(	36 4	4 565.8(1426) 1,	-328.6(	37 4	563.81	-416.8( 549)	38	628.9(	-290.06	39 4	628.9(	-388.7(	59	563.3(	-599.6(	0 09	344.8	-670.3(
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2918.9

11

298,500

PT =

2.5

MACH

= 215,142

TINE

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BLOCK

₩600 ±

READING

READING = 0094 BLOCK = 123	₩600	BLOCK	= 123			142		5.2	PT = 298.500	ē.		TT = 2918.9	6.81					PAGE 5
XABS	P-18		P-08		PDA		X00		0-1B		0-0H		CAWALL	P-18/PS0	/PS0	P-18/P10	P-08/PS0	P-08/PT0
.506E 01	1.35	0E 01	1.366E		3.565E	05	-2.077E	03	3446.0-	2	-1,182E	03	4.342E 0	3.092E	. 01	4.5235-02	3.129E 01	4.577E-02
5.526F 01	1 1.27	1E 01	1.3276		3.565E	020	-2.089E	03	-8.976E	2	-1.191	03	4.368E 0	3 2.912E	010	4.259E-02	3.041E 01	4.447E-02
5.692E 01	1 6.175E	<b>5€ 00</b>	5.925E	00	4.626E	02	-2.166E	S	-9,197E	20	-1.247E	03	4.584E 0	3 1.4146	0.1	2.069E-02	1.357E 01	1.985E-02
6.759E 01	1 4.52	1E 00	5.467E		9.744E	0	-2,189E	S	-9.267E	80	-1.262E	6	4.665E 03	1.036	10	1.5156-02	1.252E 01	1.832E-02
6.836E 01	1 2.620E	3€ 00	4.301E		6.894E	70	-2.213E	S	-9.337E		-1.28AE	03	4.760E 0	4.001E	00	8.777E-03	9.851E 00	1.4416-02
6.908E 01	1 2.609E	_	3.210	00	7.707E	02	-2.237E	S	-9.395E	20	-1.29AE	03	4.8486 03	1 .5.976E	00	8.741E-03	7.353E 00	1.075E-02
6.969E 01	1 . 2.600E	_	2.4756		8.300E	70	-2.256E	8	-9.443E	70	-1.312E	03	4.922E 03	\$ 5.955E	00	8.710E-03	5.669E 00	8.291E-03
7.064E 01	1 2.610E		1.330E		9.0445	05	-2.277E	ខ	-9.513E	N	-1.325E	03	5.036E 03	5.979E	00	8.745E-03	3.046E 00	4.456E-03
7.107E 01	1 2.61		1.762E		9.352E	6	-2,284E	S	-9.544E	. 70	-1.330E	03	5.088E 03	5.990	00	8.760E-03	00	5.904E-03
7.260E 01	3.15	<b>P</b> E 00	3.300E		1.067E	3	-2.310E	3	-9.643E	<b>2</b> 0	-1.354E	63	5.273E 03	3 7.221E	00	1.056E-02	00	1.106E-02
7.275E 01	1 3.20		37の4・の		1.081E	8	-2.322E	S	-9.652E	80	-1.357E	50	5.290E 0	1 7.341E	00	1.074E-02	7.866E 00	1.150E-02.
7.350E 01	1 3.254E		4.10SE		1.202E	0	-2.34SE	S	-9.694E	20	-1.375E	20	5.374E 03	1 7.453E	_	1.090E-02	00	1.375E-02
7.350E 0;	1 3.25	<b>₩</b> 00	4.109E		1.210E	S	-2.34BE	3	3469°6-	20	-1.375E	ń	5.375E 0	3 7.453E	00	1.090E-02		1.376E-02
7.483E 01	1 4.34	0E 00	0.000		1.280E	S	-2.390E	2	-4.760E	80	-1.414E	03	5.427E 0.	3 7.650E	00	1.119E-02		0.000
7.768E 0.	1 3.63	SE 00	00000		1.419E	03	-2.402C	9	-9.878E		-1.414E	20	5,525E 03	3 8.326E	00	1.218E-02		0.00
8.158E 0	4.73				1.598E	S	-2.414E	S	-1.000E	3	-1.414E	S	5.630E 0	1.083E	0.	1,5855-02		00000
_		3E: 00	0000		1.714E	3	-2.426E	S	-1.012E	2	-1.414E	03	5.684E 0	1.314E	01	1.921E-02		0000
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PT = 296.500 TT = 2918.9

5.2

KACH.

READING = 0094 BLOCK = 123 TIME = 215.142

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4.040E 01 9.854E 01 9.854E 01 2.564E-03 3.795E-02
4.134E 01 1.316E-01 9.871E 01 2.564E-03 3.795E-02
4.134E 01 8.442E-01 1.100E 02 2.647E-03 3.997E-02
4.134E 01 8.442E-01 1.100E 02 2.647E-03 3.997E-02
4.406E 01 2.046E 00 1.255E 02 2.756E-03 4.075E-02
4.406E 01 1.295E 01 1.255E 02 2.756E-03 4.075E-02
4.406E 01 1.395E 01 1.455E 02 2.756E-03 4.075E-02
4.406E 01 1.776E 01 1.455E 02 2.756E-03 4.075E-02
4.406E 01 1.776E 01 1.456E 02 2.756E-03 3.006E-02
4.406E 01 1.776E 01 1.456E 02 2.756E-03 3.006E-02
4.406E 01 1.776E 01 1.456E 02 2.756E-03 3.006E-02
4.406E 01 1.776E 01 1.456E 02 2.756E-03 3.006E-02
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4.406E 01 1.776E 01 1.456E 02 2.756E-03 3.006E-02
4.806E 01 1.776E 01 1.833E 02 2.756E-03 3.006E-02
4.807E 01 1.776E 01 1.833E 02 2.756E-03 3.006E-02
4.807E 01 1.776E 01 1.833E 02 2.756E-03 3.006E-02
5.605E 01 1.776E 01 2.935E 02 2.756E-03 2.756E-03
5.005E 01 1.776E 01 2.935E 02 2.756E-03 2.756E-03
5.005E 01 1.776E 01 2.935E 02 2.756E-03 2.756E-03
5.005E 01 1.776E 01 2.935E 02 2.756E-03 2.756E-03
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5.005E 01 1.756E 01 2.935E 02 2.756E-03 2.756E-03
5.005E 01 1.706E 01 2.935E 02 2.756E-03 2.756E-03
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5.005E 01 1.705E 01 2.936E 02 2.756E-03 2.756E-03
5.005E 01 1.705E 01 2.936E 02 2.756E-03 2.756E-03
5.005E 01 1.705E 01 2.946E 02 3.536E-03
5.005E 01 1.705E 01 2.966E 02 3.756E-03
5.005E 01 1.705E 01 2.966E 02 3.756E-03
5.005E 01 1.705E 01 2.966E 02 3.756E-03
5.006E 01 1.705E 01 2.966E 02 3.756E-03
5.006E 01 1.705E 01 3.006E 02 3.756E-03
5.006E 01 1.705E 01 3.006E 02 3.756E-03
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5.006E
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READING = 0094 BLOCK = 123 TIME = 215.142 MACH 5.2 PT = 298.500 TT = 2918.9

ENGINE PERFORMANCE

## RAMJET PERFORMANCE

INLET

(DEGREES)	(BTU/LBM)			
0.000 0.000 0.0110 0.2665 0.0946 0.4268	0.8970 0.9137 0.9161 0.8825 26.44 48.20	0.00 0.00 0.00 0.00 0.00 0.00 1.00 1.00		<b>w</b>
TY EFFICIENCY SUPERSONIC	INLET PROCESS EFFICIENCY - SUPERSONIC INLET PROCESS EFFICIENCY - SUBSONIC KINETIC ENERGY EFFICIENCY - SUPERSONIC KINETIC ENERGY EFFICIENCY - SUPERSONIC ENTHALPY AT PO - SUPERSONIC ENTHALPY AT PO - SUBSONIC	COPPLIENTS U.7560. COFFICIENT - CS. CT.	FUEL INJECTORS	STATION 40.400 41.266 44.300 46.250 54.031 56.216 44.766
ANGLE OF ATTACK MASS FLOW RATIO, ADDITIVE DRAG CC LIMITING PRESSUR DELTA PT2 TOTAL PRESSURE F	INLET PROCESS INLET PROCESS INLETIC ENERGY KINETIC ENERGY ENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT POENTHALPY AT PO	FUEL—AIR RATIO		INJECTORS 11A 11B 11C 2A 2A 3A 3B
(LBF) (LBF) (LBF-SEC/LBM)	(LBF) (LBF)			
1406. 1289. 4428. 4059. 0.7027	FERFORMANCE 5089. 4694.	11 40 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		34.884 0.2809 40.400 35.163 735.163 735.287 65.021 65.021
CALCULATED THRUST	STREAM THRUST	INLET FRICTION DRAG.  INLET WOMENTUM CHANGE.  COMBUSTOR FRICTION DRAG.  COMBUSTOR STRUT DRAG.  COMBUSTOR STRUT DRAG.  NOZZLE FRICTION DRAG.  NOZZLE STRUT DRAG.  NOZZLE STRUT DRAG.  NOZZLE STRUT DRAG.  TOTAL EXTERNAL DRAG.  TOTAL EXTERNAL DRAG.  TOTAL EXTERNAL DRAG.  CAVITY FORCE.  CAVITY FORCE.  CALCULATED LOAD CELL FORCE.  MEASURED LOAD CELL FORCE.	STATIONS	NOMINAL COWL LEADING EDGE SPIKE TRANSLATION INLET THROAT COWL LEADING EDGE NOZZLE SHROUD TRAILING EDGE STRUT LEADING EDGE STRUT TRAILING EDGE

t = 218.74 sec.

Test cell pressure was high which resulted in increased pressures in the AIM nozzle.

READING # 0094 BLUCK # 127 TIME # 216.742 AACH 5.2 PI # 296.000 TI # 2935.5

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2 6	1,2956 2	28,867	2559	5.1/1.5	5736 1	1.8A5 0	.08011	17.706	0.8659	3252	7.140	183.0		
1.2955		28.866	2559	0.360	914 2	2.092.0	.08011	17.766	659#°U	<b>35u2</b>	1.138	197.1		
1.2956	56 2	28.867	2559	5.056 5	5715	1.685 0	.08772	19.454	0.8659	3552	7.791	182.6		
1.2955	10.0	26. 36. 35.	2559 2531 0	401	1010 2	0 590°	. UB77¢	19.454	0.8654	5552	1.385	182.6		
1.2986	9 5	28.866	2519	.209	4228	1.928 0	.61853	19.454	0.1121	2912	005.88	149.7		
1.2986		28.866	2519	2.214 4	4233 1	1.928 0	51510.	19.454	0.1234	4762	40.502	151.5		
1.2986	<b>⇔</b>	26.866	2519	0.533	1317 1	1.064 0	0.61572	19.454	0.1234	8968	12.605	151.5		
1.2986		28.866	2519	2.122 0	4132 1	1.928 0	0.67720	10.454	0.1122	2912	43.483	140.7		
1.3388	~ ~	28.666	2513	2.034 4	4019	1.932 0	0.07893	19.454	0.1119	2869	404.84	147.5	٠	
1.2991	N	26.866	2513	2.044	1 6007	1.932 0	0.07932	14.454	0.1118	4865	42.319	147.3		
1.2992	<b>CH</b> CH	26.666	2515	2.005 3	3962 1	1.933 0	0.68049	19.454	0.1116	2855	42.109	146.8		
1.3367	~ ~	28.866	2504	950	3960	1.936 0	.07340	19.454	0.1128	2822	40.618	145.1		
1.3008 1.3368	~ ~	26.866	2491	126	3842 1	1.937 0	0.65118	19.454	0.1166	2794	38.678	143.6		٠
1.3009	~ ~	26.866 26.866	2063 1	1,906 3	3672 1	1.937 0	0.65026	19.454	0.1168	2786	30.621	143.2		
1.3012	<b>~ ~</b>	28.896	2486	. 360	3780 1	1,938 0	0.64776	19.454	9.1173	2770	38.051	142.4		
1.3912	~ ~	28.866	2011 1	6/8	3778 1.	986.	0.64736	19,454	6711.0	2769	30.010	142.5		
1.3018		26.866	2478	.876	3761 1	. 146.	5/409*0	19.454	0.1246	2758	35,659	141.8		
1.5022	~ ~ ~ ~	26.866	2473	1,956 3	3853 1	1.940 0	0.56753 19 <sub>.</sub> 454 0 <sub>6</sub> 1538	454.61	0.1538	2785	35.985	143.1		

	<b>D.</b>	-	r		4 i 4 8	MOL * 1	V 408	I V	VEL	:0:	4)4	ŧ	24/40	K. P. J. P.	٤	74 7	o.	747
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<u>.</u>	0	2717	\$65		1.3024	28.866	2449											
•	11.930	1012	272.	404)	1.3428	28.866		2.050	3959.1	. 438 0	.52895	19.454	0.1436	2018	32.545	144.9		
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1007	11.165	2044	610,4	623) 523)	1.3096	24,116	2672	47	4	276	10101	100	4		5	:	5	•
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	13.200	1910	336.	575)	1.3345	24.188	2289	1.598	3658 2	.265 0	.39566	954-61	0.1950	2906	35.496	147.1	68.0	11.0
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	23.950	3133	420.7	84)	.2866	24.669	2832	0.936	2651 2	.383 0	. 32014	14.871	0.2379	3047	13.439	155.6	75.0	97.0
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9	•	>	430.5	( \ 20	1 . 4750	/ no e c y	2 7	400.0	2 0 6 2	. 245	.51246	14.671	0.845.0	3155	13,318	158,8	9.24	9.0
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	7	-	394.36	1.88)	2668	25.078												
	22.073	3087	439.6	10401	1.2040	23.063	2922	1 286.0	2782 2	0.533.0	29708	20.020	12650	3218	12.801	4	9	<b>1</b>
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•	∹	3205	423,3(	103)	1.2743	23.295	2980	996.0	2884 2	.545	0.28093	20.020	0.2782	3298	12.591	164.7	0.79	27.0
Š	•	2	23.															
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8	_	326	7 7 72	7	. 434	75655	7005	<b>* B • 0</b>	2/36 A	986.		070.07	0.2970	3347	11.272	100.7	0.70	0.51
	2.8	4316	591.00	100	2126	22.408	8408											
	22.601	4047	452.00	484)	1.2269	22.447	3314	0.746	2637 2	.732 0	.21420	20.169	0.3676	3761	8.777	187.5	1.04	0.57
COMBUSTOR	. (	2	2 52															•
36,226	32.694		240.00	1601	1.2124	22.410	7400	4		•								
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•	2.70	4391	590.5	640)	2062	22.488	3422											
56.241	21.935	4102	B. C. 2.2	1507)	1.2213	22.535	3325	0.825	2737 2	.735 0	.21144	20,169	9645.0	1780	0.080	4	770	•
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	33.200	t 500	286.00	1627)	1.2071	22.480	2420											
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Š	Z . Z	96.44	£4 #	4.6		62 623												
	23.200	4167	2649	1913)	1.2168	22.582	2367	0.786	2 5296	735 6	19117	20,100	1. 16.86	4.8.4	- 7	0	9	4
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57.007	33.492	4475	585.46	1663)	1,1990	22,585	3437											
100.16	,,,,	100	440.7	553)	1.6164	22.539	3351	100	2054. 2	4،750 د	.21517	20.109	0.3694	3855	0.720	191.1	1.004	54.0

NEADING # 0094 BLOCK # 127 TIME # 218-742 KACH 5-2 FT # 298-000 TT # 2935-5

ě																				·											
IVAL PHI ETAC		29.0			0.71	•		0.79			0.79	•		0.74			0.79			0.79			0.70			22.0	•	٠	1.00		
T d		100			70.1	•		1.04			1.04	•		1.04			1.04			300			1.04			1.04	•		1.04		
1 y & C		19501			195.6			94.5			93.0			94.5			988.9			4.60			0.09			\$006			96.4		
9		59.7 6.52.3 193.1 1.04 0.67			3945 8.523 195.6 1.04 0.71	1		3917 10:077 19462 1:04 0:79			3693 11.271 193.0 1.04 0.79			3922 12.295 194.5 1.04 0.79			5162 4.761 255.9 1.04 0.79			5355 3.089 go5.5 1.04 0.79			4.826 260.0 1.04 0.79			5455 3.058 270.8 1.04 0.74			5937 4,760 295.4 1,04 1,00		
AZAC MUNTY .G		2 '65			3945			3917			3693			3922			5162			5.355			5200			5455			5937		
10/0		0.3755			0.3777			0.3650			0.3553			0.1553			1.9372			3.1007			1.9372			3.2505	1		2.3363		
•		20.169			20.169			20,109			20.169			20.169			20,169			20.109		•	20.169			20.169			20,169		
* * */*	2.196.52.094 3453	3.40985		1,1808 22,616 3467	67802.0		1,1670 22,994 3486	0.21575		1,1669 23,013 3484	0.22159		1,1612 22,424 3519	0.22159		1.1669 23.013 3484	5907000			1,2977 25.584 dulu 5,306 7479 2,740 0,02491 20,109 3,1007			2.868 7640 2.757 0.04065 20.169 1.9372		1,1612 22,924 1519	3.02422		101141 145,000 1460 1	0.03370		+ 1961 21 21 21 1504
တ		. 734			2.741			2010			2.740			1.157			2.740			001.3			1.757			157 (			2.623		
1 1 1		1014			2631			9001			1273			1570			1536			610						1123			1087		
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A NOS	1053	1372 0		1467	3389 0		985	389 0		797	1369 0		1519	1365 1		1464	2 6682		797	2414 3		5519	2000		6151	2466 3		1593	\$219 #		40.51
F () [ H ] ()	460.2	2.764		2.616	369.5		766.7	3.127		3,013	3.160		2.424	3.126		3.013	3.384		3.013	3.584		2.924	7.304		2.924	3.384		3,460	4.115		1 210
GAMMA POLMT SONV MACM VEL S	5 "96" 5	5 22021		1.1808 2	1.1919	,	1,1670 2	1.1783 2		1.1669 2	1.1809 2	· ·	1,1612 2	1.1751 2		1.1669 3	1.2837 2		1,1669 2	1.8977 2		1.1612 22,924 3519	1.2788 2		1.1612 2	1.2937 2		1,1571 2	2 0208.1	•	2 1001
	_	(#651)6°F		_	_		_	581.7(1670)		554.5(1798)	40.4(1652)		637.7(1944)	_		254.5(1760)			554.5(1760)	765		044	383		144)	734)		(1963)	(585)		( ATO)
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_ 5	£ 57.0	4351	7	1197	4434	3	5197						4918				2475		4616	2112	5	87.00	0 7 9 7	9	4918	2211			1633	9	000
<b>a</b>	\$5.518	₹	0	34.661	23.737	0	34,048	21.750	0	34,552	20.231	RECEN	34,552	16.500	iaă.	34,552	288.0		34.552	0.436	AE. REGEN	34,592	0.410	KEGEN	34.552	0.436	<b>にしかせいおイカ</b>	136.896	0.436	NOZZLE	120.081
0.15	187	.731	BUSTOR	151.		BUSTER.	761		BUSTOR	.181	191	BUSTOR	.181		₹	257		14 B17	457	•		557		מלוב שמ	257		Ü				257

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EADING # 0094			BLOC* = 127	# 4		11.	11.F # 219.	8.142	H.A.C.H	5.5	P) a 298.000	÷		#	11 = 2935,5	.5					PAGE 5
XABS		91 = d	•		F-08		V Ü d		X O O		3 F		8 Ú <b>•</b> B	80		CAWALL		P-IB/PSU	P=18/P10	P-08/P80	P=08/P10
6.464E	70	1.6086	8£ 0		. 0 U BE	1.	7.09AE	_		03	-1.537E	S S	-1.737E	75.0	3 4	1.289E 0	, ·	1.684E 01	5.3958-02	3.689E 01	5.3958.02
6.502t	70	1.51	ZE O	_	3777°	<u>.</u>	7.09AF	<u>~</u>		0.3	-1.353E	03	-1.74	35	<b>⊅</b>	. 337E U	<b>,</b>	5.471E 01	5.0765-02	3.544E 01	5,1825=02
9.506E	0	1.512E			.537€	10	7.096	_		03	-1.554	0	-1.16PF	0 48	2	. 342E	-	1.471E na	5.070102	3.5268 01	5.1595-02
6.526E	70	1.42			3005 ·	0.1	7.096E	2	30110E	3	-1.3632	3	-1.78ZE	35	7	. 36BE U	,,,	3.275E U1	4.7865.02	3.451E 01	5.046E=U2
6.692E	3	7.100E	06 00		0.412F	00	8.287E	90	-3.44E	0.5	-1.418E	0	-1.87EF	و الانتا	7 5	. 584E 0	_	1.629E 01	2.363E=02	1.472E 01	2.152E-02
6.759E	0	5.40			.187€	00	9.557£	S C	-3.340E	S	-1.434E	03	-1.907E	7E 0	7 T	.665E 0	_	SAUE OF	1.8136-02	1.420E O1	2.0766.02
6.836E	70	3.450E		00	1.129F	e	1.094	~	-3.340E	Š	-1.449	5	-1.9011	1.0	3 6	. 760E 0	<b>I</b>	P. STAE DO	1.154E-02	1.177E 01	1.721E=02
6.908E	70	2,93		7 Ú	9377º	0	1.1934	2	-3.437E	S	-1.467E	0	*1.470F	0 49	3 4	BUBE 0	۳,	737E 00	9.851E=03	9.501E 00	1.389E+U2
9696.9	<b>7</b> 0	2.500E		٠ 0	. U51E	0	1.261	Š	-3.4/5E		-1.476E	03	-4.005E	SE U	7	.922t 0	×.	5.737E CO	6.389£-U3		1.0245-02
7.0645	<b>:</b>	2.77		0	.3556	00	1.341	03	-3.564E	S	-1.485E	03	-2.040E	0 30	3	5.056E U	_	1.377E 00	9.325E-03	3.110E	4.547E=03
7.107E	5	3.90SE			2,361	00	1.375E	ô	-3.544E	03	-1.4916	0.	-2.053E	3E 0	3 5	.088E U	_	6.667E 00	9.7486-03	_	7.923E=03
7.260E	70	4.53			3006·	00	1.563E	03	.3.613E	0	-1.5136	S	42.10	1E 0	3	5.273E 0	-	10 40E 01	1.520E-02	1.3635	1.9936=02
7.275E	5	4.690E	0E 0		. 89BE	°	1 . 586E	ô	-3.661E	03	-1.5156	03	•2.106E	96	3	.290E 0	<u>_</u>	.076E 01	1.5746-02		1.9796=02
7.350E	៊ី	7.00	<b>SE</b> 0	5	3069.	C	1.76RE	0	-3.660E	<b>~</b>	-1.5256	5	-2.13	6E 0	3	.374E 0	'n	71E 01	1.565E=U2	_	1.909E=02
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8.726E	3	8.00	<b>)E</b>	c	00000		2.661E	03	=3.947E	3	-1.729E		-2.197E	7E 0	2	5.707E 0	- m	.836E 01	2.685E=02	00000	0000

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## PAMJET PERFURMANCE

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t = 231.34 sec.

The injected fuel is possibly unburned.

TIME = 231,342 - MACH 5,2 PT = 298,750 TT = 2945,6 RAMJET PERFORMANCE BLOCK = 141 READING = 0094

REPORT SUMMARK

ETAC 0.05 0.04 2759 40.588 141.6 0.13 0.00 2698 40,439 138,4 0,13 0,35 0.00 0.00 2864 44.267 147.2 0.07 0.07 0.01 2774 41.124 142.4 0.13 0.00 0.01 0.28 PHI 2782 41.399 142,7 0.13 2781 41.330 142.7 0.13 2653 35.963 136.1 0.13 2645 35,490 135,7 0,13 2631 32.648 135.0 0.13 2629 34.549 134.9 0.13 2629 34,485 134,9 0.13 IVAC 7.151 183.4 7.790 183.0 1,384 183.0 2865 43,039 147,6 1.141 197.2 2904 39.200 149.6 2904 13.087 149.6 3257 3502 3552 3552 KOMI 917 2.093 0.08008 17.759 0.8659 28.866 2535 0.401 1018 2.093 0.08754 19.414 0.8659 27.463 2548 27.463 2070 1.851 3831 2.026 0.68172 19.489 0.1116 27.463 2150 1.591 3422 2.036 0.64852 19.489 0.1173 27.669 2528 1.544 3439 2.060 0.61084 19.489 0.1246 28.866 1112 5.170 5747 1,885 0.08008 17.759 0.8659 28.866 1132 5.058 5726 1.885 0.08754 19.414 0.8659 28.866 2531 28.866 1976 2.074 4097 1.940 0.61829 19.414 0.1121 28.866 2531 28.866 1973 2.080 4105 1.940 0.61446 19.414 0.1234 2531 2478 0.553 1371 1.968 0.61446 19.414 0.1234 28.090 2554 28.090 1966 2.139 4206 1.990 0.67728 19.456 0.1122 27.491 2558 27.491 2061 1.899 3914 2.028 0.68062 19.489 0.1118 27.467 2550 27.467 2050 1.907 3910 2.025 0.68015 19.489 0.1119 27.464 2054 1.893 3888 2.025 0.68054 19.489 0.1118 0.1128 1.656 3547 2.040 0.65235 19.489 0.1166 1.641 3506 2.036 0.65143 19.489 0.1168 2525 2150 1.594 3426 2.036 0.64892 19.489 0.1173 A/AC 27.715 2622 27.716 2173 1.775 3857 2.067 0.67461 19.489 VE. 2563 2541 0.361 SONV MACH 2542 2142 2530 2136 28.866 28.866 27.500 27.469 27.464 1.2978 28.866 VOL'ST 1.2951 1.3388 1.2978 1.3020 1.3316 1.2951 1.2953 1,2953 1.2994 1,2933 1,2970 1,3033 1,3034 SAPPA 1,3031 1.3046 1,3050 3317 780) 780) 128) 780) 760) 157) 757) 720) 7571 768) 766) 462) 760) 759) 526) 755) 506) 745) 502) 742) 509) 742) 509) 466) 820) 0 5 654.2( -5.8( 654.2( 637.4( 607,81 633,50 530.10 19. 46 607.70 654.21 30.1 93.3 2946 2890 2946 2877 .400 13.675 1693 120,775 2865 13,528 1688 14.687 298,750 14.395 14.687 13.247 120,775 19,876 0.383 65,753 17.419 11.178 12,519 16,866 18.454 14,358 966.96 14.636 15,323 110,031 OMBUSTOR BUSTOR

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	PHI	0.13	0.13	0.13	0.13	0.13	0.13	0:15	0.15	0.15	0.15	0.15	0.15	0.15	0:15	0.15	0.15	0.15	0.15	0.15
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	A/AC	0.1338	0.1338	0.1436	0.1554	0.1662	0.1950	0.2379	0.2480	0.2631	0.2782	0.2970	0.3678	0.3689	0.3717	0.3675	0,3686	0.3694	0.3753	0.3777
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298•	VEL	3502	3504	3532	3680	3834	3986	4280	4266	4287	4310	4369	4356	6644	4505	4386	4415	9624	4326	4417
PT =	KACH	.647	,659	. 665	.778	.910	040	328	.324	.351	379	2.384	407	.601	.614	424	498	.473	295	.486
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MACH	POLWT S	27.494 2	27.468	27.513 2	27.497	27.468 2 27.468 3	27.471	27.213	27.203	27.201 2	27.201	27.277	27.233	27.206	27.202 2	27.254 2	27.209	27.212 2	27.345 2	27.230 2
231,342	GAMMA	.3330	.3343	.3330	3051	1.3424 2	.3067	1.3081 2	3087	.3089	1.3090 2	1.3583	3078	1.3090 2	1.3692	1.3069 2	1.3089 2	.3088	1.3526	1.3640 2
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231.342	GAMMA	710) 1.3094 27.205 2481 269) 1.3776 27.205 1621	1,3096	1,2843	1.2948	1.2862	1.2948	1.2948	1.2862	1.2862	1,2738	1,2956
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9	CAWAL	4.342E	Š.	.5	.665E	1.760E	9.	4.922E	0	. 088E	5.273E	3.290E	5.374E	5.375E	5.427E	5,525E	5.630E	3,6845	ž	7.
376	•		4	• <b>•</b>	<b>4</b>	<b>-</b>	<b>.</b>	<b>.</b>	٠,	٠,		<b>47</b>	47	un 		<b>U</b> 3	9)	•	(D)	43
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F	0-0B	946	.607E	.755E	936	396	.900E	<b>30E</b>	192E	OIE	71E	BIE	142E	35 t-1	71E	71E	71E	71E	7 1E	716
0	Ġ	-7.584E	7.6	7:	7.7	-7.839E	٠. د	-7.950E	-7.992E	-8.001E	-8.071E	-8.081E	-9.	-8.1	-8.271E	-8.271	-8.2711	-8.271	8.2711	6
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11	91-0	800	.807E	873E	.903E	939E	.972E	-7.997E	034E	-8.050E	<b>3660</b>	104E	124	124E	156E	211E	-8.267E	318	4156	-
P	9	-7.800E	۲.	۲.	٠,	ŗ	۲.	۲.	ę.	ø,	ø,	-8.1	ę.	-8.1	-8.1	-8.21	ø.	ę	8	8
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		緩	H	35	9E	<b>BE</b>	<b>587E</b>	<b>595E</b> .	H	Ñ	.617E	,618E	627E	627E	띪	뜅	,654E	띯	96	Ã.
KACH	X O D	1.538E	52	.56	.5	5	58	53	1.603E	. 605E	.6	19.	3	9.	.643E	648E	.65	1.659E	1.669E	3699€
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231,342		05	02	9	8	8	5	5	8	5	6	5	5	8	8	0	8	8	9	05
31.	⋖	535	153E	<b>386</b>	46E	305	<u>9</u>	318E	3.214E	256	BJE	81E	93E	•001E	131E	400E	,780E	3966*	2,236E	.236E
11	PDA	-3.153E	-3.1	-2.698E	2.1	1.5	6.0	ຜູ	S.	1.5	6.781E	7.1	<b>6</b>	1:0	7:	1.4	1:7	5.3	2	2.5
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141	-0B	6.505E	750	2.687E	2.047	2.330E	2.595	93	.310	.276E	• 155E	1.067E	300	6.277E	0.000	8	90	0.000	900	000
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P.O	m								님	띰	911E-01	١	779E-01	775E-01	<u>.</u>	٥	850E-01	į.	Į Į	<u> </u>
	P-18	2.600E	69	.47	.682E	1.770E	.746E	.725E	.370E	77	5	ğ	7	ζ,	.500E-0	.950E-0	ž.	9.600E-01	•025E	, 025E
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9N1	38	<b>06E</b>	<b>3</b> 92	<b>356</b>	<b>20E</b>	366	380	9E	54 104	107E	20E	75E	30E	20E	336	58E	<b>28E</b>	2	23,5	26E
READING # 0094	XABS	6.506E	6.526E	6.692E	6.759E		3806°9	6.969E	7.064E	Ţ.,	7.260E	7		7.350E	7.483E	7	÷	*	ř	9.7
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READING = 0094 BLOCK = 141 TIME = 231,342 MACH 5,2 PT = 298,750 TT = 2945,6

## RAMJET PERFORMANCE

	INLET	IENT.	PRESSURE RECOVERY - SUBSONIC 0.2674 PROCESS EFFICIENCY - SUPERSONIC 0.8910 PROCESS EFFICIENCY - SUPERSONIC 0.9119 C. ENERGY EFFICIENCY - SUPERSONIC 0.9140 C. ENERGY EFFICIENCY - SUBSONIC 0.8833 PY AT PO - SUPERSONIC 31.11 (BTU/LBM) PY AT PO - SUBSONIC 51.19 (BTU/LBM)	COMBUSTOR	FUEL-AIR RATIO	5TATION VALVE 40.400 B 41.266 B 44.300 48.741 46.250 54.031 56.031
TENTOUS TOUR		-92. (LBF) -37. (LBF) -37. (LBF) -3011. (LBF-SEC/LBM) -403. (LBF-SEC/LBM) -00460 -00460 -00460 -00460 -00460 -00184	TOTAL TOTAL INLET INLET INLET KINETI (LBF) ENTHAL (LBF-SEC/LBM) ENTHAL		96.4 (LBF) 123.6 (LBF) 193.6 (LBF) 193.6 (LBF) 194.6 (LBF) 195.6 (LBF) 195.6 (LBF) 197.6 (LBF) 197.6 (LBF) 197.6 (LBF) 197.6 (LBF) 197.6 (LBF) 197.6 (LBF) 197.6 (LBF) 197.6 (LBF) 197.6 (LBF) 197.6 (LBF) 197.6 (LBF) 197.6 (LBF) 197.6 (LBF) 197.6 (LBF) 198.7 (LBF) 198.7 (LBF) 198.7 (LBF) 198.7 (LBF) 198.7 (LBF) 198.7 (LBF) 198.7 (LBF) 198.7 (LBF) 198.7 (LBF) 198.7 (LBF) 198.7 (LBF) 198.7 (LBF) 198.7 (LBF) 198.7 (LBF) 198.7 (LBF) 198.7 (LBF) 199.7 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (LBF) 199.6 (	34.884 (IN) INJECTORS 0.2809 (IN) IA 40.400 (IN) IB 35.165 (IN) 2A 73.505 (IN) 2A 65.021 (IN) 3A 65.021 (IN) 3B
1	6 ENGINE PERFORMANCE	MEASURED THRUST	STREAM THRUST	MOMENTUM AND FORCES	INLET FRICTION DRAG.  INLET MOMENTUM CHANGE.  COMBUSTOR FRICTION DRAG.  COMBUSTOR STRUT DRAG.  COMBUSTOR MOMENTUM CHANGE.  NOZZLE FRICTION DRAG.  NOZZLE FRICTION DRAG.  NOZZLE MOMENTUM CHANGE.  NOZZLE MOMENTUM CHANGE.  NOZZLE PRESSURE INTEGRAL.  EXTERNAL PRESSURE INTEGRAL.  TOTAL STRUT DRAG.  CAVITY FORCE.  CALCULATED LOAD CELL FORCE.  CALCULATED LOAD CELL FORCE.  CALCULATED LOAD CELL FORCE.  FUEL VACUUM SPECIFIC IMPULSE 0.0.	NOMINAL COWL LEADING EDGE. SPIKE TRANSLATION. INLET THROAT. COWL LEADING EDGE. NOZZLE SHOUD TRAILING EDGE. NOZZLE PLUG TRAILING EDGE. STRUT LEADING EDGE. COMBUSTOR EXIT.
1	Ju					

t = 233.14 sec.

The injected fuel is possibly unburned.

IREADING # 0094 BLOCK = 143 TIME = 233.142 MACH 5.2 PT = 299.500 TT = 2941.8

ETAC 0.53 2672 35.559 136.6 0.23 0.08 0.00 2869 44.335 147.0 0.15 0.07 0.23 0.03 2785 41.363 142.4 0.23 0.00 2778 41.155 142.0 0.23 0.00 0.23 0.00 34.163 135.7 0.23 0.00 2666 32,396 136,3 0,23 0,00 2666 35.093 136.3 0.23 0.01 PHI 2705 40,447 138.3 0.23 2654 34.100 135.7 0.23 IVAC 3552, 1,384 182,8 7.173 183.3 2785 41,432 142,4 2762 40.577 141.2 2909 13,036 149,7 7.791 2870 43,148 2909 39,334 3267 3504 3552 2654 MONTY 5.170 5743 1.885 0.08038 17.826 0.8659 920 2.092 0.08038 17.826 0.8659 28.867 2562 28.866 1131 5.062 5723 1.885 0.08760 19.427 0.8659 2562 2534 0.401 1017 2.092 0.08760 19.427 0.8659 28.866 2529 28.866 1970 2.084 4105 1.938 0.62062 19.427 0.1121 28.866 2529 28.866 1966 2.094 4116 1.938 0.61486 19.427 0.1234 26.513 2568 26.513 2069 1.884 3900 2.077 0.68254 19.557 0.1119 1.3068 26.508 2566 1.3416 26.508 2073 1.871 3878 2.077 0.68294 19.557 0.1118 26.599 2579 26.599 2198 1.590 3495 2.096 0.65465 19.557 0.1166 26.508 2540 26.507 2176 1.550 3372 2.083 0.65080 19.557 0.1173 28.866 2528 28.866 2477 0.551 1364 1.967 0.61486 19.427 0.1234 27.317 2577 27.317 1996 2.105 4200 2.036 0.67927 19.513 0.1122 26.545 2580 26.545 2086 1.872 3903 2.082 0.68301 19.557 0.1118 26.507 2565 26.507 2089 1.827 3817 2.078 0.68412 19.557 0.1116 27.136 2760 27.139 2365 1.626 3844 2.158 0.67699 19.557 0.1128 1.594 3454 2.085 0.65372 19.557 0.1168 26.509 2541 26.509 2176 1.552 3376 2.084 0.65121 19.557 0.1173 2528 2154 1,579 3401 2,082 0,61299 19,557 0,1246 A/AC ¥/¥ ≂ 0 ± ⊒ ≃ s VEL SUFFARRY MACH 2562 2539 0.362 MOLINT SONV 28.867 2562 28.866 1111 751) 1.3078 26.521 2549 514) 1.3345 26.521 2167 28.856 28.866 28.866 28.866 1.3356 26.507 GAMMA 1,3086 1.2954 1,2953 1,2979 1.2953 1,2979 1.2979 1.2954 1.3437 1.3051 1.3418 1.3404 1,2801 1.3042 1.3087 745) 519) 779) 128) 759) 755) 421) 755) 745) 519) 737) 507) 763) 762) 933) 533) 123) 755) 774) 471) 763) 179) 459) 765) 463) 464) 779) 653.1( 9 21 605.7( 378.0( 10 21 605.6( 378.4( 608.3( 369.91 653.1( 597.70 536.2( 119.90 524.00 323.6( 523.3( 518,51 632,4( 628.4( 89,8( 291.7 122,256 2860 13,615 1682 16 2630 1892 1892 2886 13,396 1675 13,247 287 14.687 77.676 20.060 10,052 14.416 0.438 14,698 104.128 14.453 77.688 20,118 11,199 93,496 75,121 18,328 93,969 91,755 15,465 12,751 COMBUSTOR 46.260 COMBUSTOR 44.800 44.800 COMBUSTOR 44.776 44.776

PAG																				
	ETAC	0.05	0.05	0.19	0.17	0.13	0.22	0.04	0.13	0.17	0.21	0.15	. ~	60.0	90.0	0.24	0.19	0.21	0.28	0.15
	F		0.23	0.23	0.23	0.23	0.23 (	0.25 (	0.25	25	ຄ	. 10	. 25	0.25 (	 (N	•25	. 25	20.	12	0.25 (
	IVAC	0.6	0.6	4.	3.6	5.2	60	51.4 (	52.0 (	53.1 0	O	5.1	7.3	57,4 (	57.5 0	57.6 0	57.7 0	57.9 0	58.3 0	158.4
		#e 1	66 13	69 14:	. 89 14:	31 14	048 148	.875 15	310 15	234 15	283 15	596 15	• •	760 15	689 15	411 15	34 1	72 1	20 1	.442 15
	G	30	30.7	28.6	27.8	27.2	24.	21	20.	-61	18.	17.	=		¥.	14.	14.5	14.4	14.1	7
	MOMTM	2719	2719	2766	2808	2840	2911	2979	2991	3011	3030	3050	3095	3096	3098	3100	3103	3106	3113	3117
	A/AC	.1338	.1338	.1436	.1554	.1662	.1950	.2379	.2480	.2631	.2782	.2970	r,	.3689	. 7117	.3675	.3686	.3694	.3753	0.3777
		557 0	557 0	557 0	557 0	557 0	557 0	.672 0	.672 0	.672 0	672 0	.672 0		.672 0	572 0	.672 0	.672 0	.672 0	.672 0	
41.8	3	5 19.	19.	19.	19.	19.	19.	13	19	61	. 61	19	19	19	19.6	19	19	19	19	19.672
TT = 29	4/4	Ω.	0.57052	0.53176	0.49135	0.45953	0.39165	0.32288	0.30969	0.29192	0.27605	0.25862	0.20881	0.20819	0.20666	0.20897	0.20835	0.20792	0.20466	0.20336
500 T	s	•	• 086	•105	.102	• 095	.109	060	.113	.121	.129	.116	.151	.105	.103	.140	130	134	.147	2.116
299.	VEL	3468 2	3470 2	3469 2	3652 2	3813 2	3951 2	4360 2	4220 2	4240 2	4262 2	378 2	4384 2	562 2	4574 2	4438 2	4489 2	4479 2	4439 2	4570 2
PT	MACH		.610 3	556 3	.684 3	.821 3	.879 3	386 4	57	1444	137 4	301 4	193 4	579 4	602 4	91	376 4	347 4	.248 4	.520 4
5.2		-	-	Ξ.	7	-		~	50 36 2:1	. «	ď	~	~	ત	ď	5 2.2	ູ່	588 908 2.	. 0	a
MACH	T SONV	00	4 2542 4 2155	~~	9 2586 9 2169	5 2564 5 2094	4 2103	6 2515 6 1827	9 2560 9 1956	1 2578 1 1977	8 2592 8 1994		0 2621 1 1999	8 2530 8 1769	0 2527 0 1758	2 2601 2 1945	4 2580 4 1889	~	9 2618 9 1974	7 2556 7 1813
Q.	FOLWT	Ø W	26.564 26.564	26.732 26.732	26.709 26.709	26.655 26.655	26.764	26.316 26.316	26.439	26.491	26.538 26.538	26.462	26.630 26.631	26.378 26.378	26.370 26.370	26.572	26.514 26.514	26.539 26.539	26.629 26.629	26.457
= 233,14	GAMMA	1,3075	1,3075	1.3007	1,3019	1,3044	1,3001	1.3107	1,3054	1.3033	1.3014	1,3048	1.2976	1.3086	1,3090	1.3001	1.3027	1,3016	1.2978	1,3054
TIME :		748) 509)	748) 509)	792) 553)	783).	766) 477)	793)	727) 349)	762) 408)	776)	788) 427)	765) 383)	812)	740) 325)	737) 320)	795)	778) 378)	785) 387)	810) 419)	760) 344)
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BLOCK =		19 1 2641 1862		2787 2787 2015	725 759 898	23 2702 1757	793	255 554 297	26 670 508	27 27 716 546	28 2 757 5	29 679 423	20 2 2837 1593	214 214	•	33 26 2781 50 1499 1	2724 1405	748	2830 1551	,
# B			. 208 2 . 782 1			.066 2 .275 1					406 2 950 1					140 2 104 1			965 2 150 1	
600	•	75	15	17	69 14	12	<b>9</b> -	76		61	ຼິສະ	9	3	, s	30 6	51	S	S S	89 3	61. 3.
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	711	ر ا		3.02		10			. 4.	20.		43			67			43			63			64	•		67			00			1.67
	-70	JUL 101		0.25		90.0	200		30			200			200			20.0			28			96.0			20.0			25.			0.25
	TVAC	) 	į	0.851		157 A			1,23	•		67.0			0 191			A7 0			AA 7			98			9, 46			2000			185.2
	æ	,		384		1.861			A7A .			8.30			160			1. 483			3.274 188 7 0 28 0 67			3.607 198.1 0.95 0.67			1.241			5.382			5.411 1
	MENCH			3108 15,384 158,0 0,25 0,02		3101 14 A61 157 4 0 25 0 27			F2 0 80 0 1 721 878 61 090F			TARR 11 830 157 0 0 25 0 54			EA 0 30 0 0 131 100 01 081F			1695 3 483 187 0 0 25 A 57			3712			3837			3867 3.241 196.6 0.25 0.67			4121 5.382 20974 0.25 1.00			3642 3.411 185.2 0.25 0.67
•	A/AC		,	3656		13554			5749	``		4032	•		CE 047			.9372		٠	0755	3		9371			1827			4367			.9371
o	3		•	9.672.0		9.672 0			9.672 0			9.672 0			0 672 0			9.672			9.672 2			9.672 1			9.672 2			9.672 1			9.672 1
0.1.42       UUC.424     7.4. 0.44   2.4	W/W		711) 1,3127 26,296 2492	. 21043	803) 1,2988 26,615 2609	121614 1		935) 1.2777 27.099 2755	. 20487	•		1 74061.			1 74001		943) 1.2753 27.150 2769	.03965 1			1 103701			1 39650		029) 1,2651 27,144 2860	1 613519		067) 1,2575 27,600 2882	.05346 1		941) 1.2760 27.150 2759	.03965 1
-	v	,	. 0	9/0		141 0			.202 0			.212 0			237 0			.212 0			.212 0			.237 0			.237 0			.126 0	·		.221 0
C * & C 7	VEL	<b>i</b>	,	7 *0.4		2 4244	• • •		1045 2	1 }		1000			6 1901	•		5653 2	1		5692 2			5854 2			5927 2			5479 2			5536 2
_	MACH		6	260		252			748			.705			1 652			258			.323	, 1		204	•		315			245			.112
0	NOS		2492	7 9791	6096	1964 2		2755	2314 1		5769	2346 1		2860	1458 1	1	6922	1735 3	· }	2769	1713 3	)  -  -	2860	1827 3		2860	1788 3		2882	1526 4		2759	1779 3
	GAMMA MOLET SONV MACH VEL		26.296	062.02	26.615	26.615		27.099	27.102		27.150	27.154		27.144	27,153		27.150	27.154		27.150	27.154		27.144	27.154		27.144	27.154		27.600	27,611		27.150	27.154
11000	GAMMA		1.3127	1610.1	1.2988	1.3471		1.2777	1,3131	·	1.2753	1.3100		1.2651	1.3016		1.2753	1.3614		1,2753	1.3634		1,2651	1.3528	· •	1,2651	1.3565		1.2575	1.3742		1.2760	1.3574
 			(117	10/3	803)	414)		935)	614)		948)	635)		(620)	710)		943)	317)	1	943)	308)		1029)	356)		(620)	339)		1067)	242)		941)	335)
2	I	31 21	562.3(	32 50	561.36	170.16	33	559.2(	232,3(	50	558.9	239.2	35. 3	644.2(1	314.6	36 2	558.91	-79.61	37 2	558.9(	-88.6	38 3	644.2(1	140.7	39 GE	644.2(1	-57.8(	.0 65	558.9()	-279.91	0 09	550.8(	-61.6(
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	م	0	83,069	•	51,643	4(350	0	33,340	6.420	0	30,160	6.218	REGEN	30,160	6,767	٠.	30.160	0,482		30.160	0.435	REGEN	30,160	0.520	REGEN	30,160	0.435	MBUSTR	22,256	0,435	122LE	25,737	0.519
	•	COMBUSTOR	60,761	COMBUSTOR	62,181	62,181	COMBUSTOR	64.645	64,645	COMBUSTOR	65,021	65.021	COMBUSTOR	65.021	65.021	NOZZLE A	87.257	87.257 · ·	NOZZLE P	87.257	87.257	NOZELE A	87.257	67,257	NOZZLE P	87.257	87.257	FICTIVE C	65.021	65,021	FICTIVE N	87.257	87.257

REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR 7-08/7 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.0000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 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P-08/PT0	2.260E-02	2.316F=02	1.194F=02	1 2675-02	104611	0.0175-01	7.7435-03	16.7576-03	4 240F-03	10 10 E	2001	2000000	1.920E-03	1,911E-03	0.00					000.0	0000
P-08/PS0	1.557E 01	1.596E 01	A.222F 00	A. 72AF 00	7.74AF 00	A. B.SIF ON	5.333F 00	3.001F 00	2.921F 00		100000				0000	0.00				0000	0000
P-18/PT0	1.903E-02	1.831E-02	1.235F-02	9.760F=03	6.778F=0.3	6-145F-03	5.609E-03	4.3916-03	3.840E-03	2.5026=04	2.3715-03	2 1066-03	C0-1001-2	Z.104E-03	1,636E-03	2.5545-03	2.5215-03	2.821F=03	2556.04	D. F. COL	3.256E-03
P-18/PS0	1.311E 01	1.262E 01	8.510E 00	6.723F 00	4.669F 00	4.233E 00	3.864E 00	3.025E 00	2.645E 00		1.6335 00			104206 00	1.127E 00	1.759E 00	1.736E 00	1.9435 00	2000 0000		2.243E 00
CAWALL	4.342E 03	4.368E 03	4.584E 03	4.665E 03	4.760E 03	4.848E 03	4.922E 03		5.088E 03								5.630E 03		5.707F 03		5./U/E US
6-0B	-	_		. –	-9.456E 02		-9.643E 02														003E
0-1B	09E 02	-8.619E 02	06E 02	05	05	05	-8.857E 02	05	2	2	02	2	9 6	9	20	8	8	20	2	9	_
X00	-1.771E 03	7	-1,801E 03	-1.811E	-1.824E	-1.839	-1,850E 03	-1.860E	-1.863E	-1.876E	-1.878E	-1.887F	1 8875	11.00	-1.906E	-1.912E	-1.917E	-1.921E	-1,929E	1000	
PDA	-2.054E 02	-2,054E 02	-1.498E 02	-7.901E 01	3.077E 00	6.757E 01	1.146E 02	1.672E 02	1.851E 02	2.361E 02	2.400E 02	2.658F 02	2.660r 02		2. /8./E UZ	3.038E 02	3.363E 02	3.541E 02	3.760E 02	1 760F 02	30 JOOL 02
P-08	6.769E 00	6.937E 00	3.575E 00	3.795E 00	3.369E 00	2.970E 00		1.305E 00	1.270E 00	1.145E 00	1.050E 00	5.750E-01	5.72KF-01	1000	0000	0000	0000	0000	0000	000	2
P-18	5.700E 00	5.485E 00	3.700E 00	2.923E 00	2.030E 00	1.841E 00	1.680E 00	1.315E 00	1.150E 00	7.493E-01	7.100E-01	6.307E-01	6.302F-01		10-3006-4	7.650E-01	7.550E-01	8.450E-01	9.750E-01	0.753Fent	40-110
XABS	0.500E 01	6.526E 01	6.692E 01	6.759E 01	6.836E 01	6.908E 01	6.969E 01	7.064E 01	7.107E 01	7.260E 01	7.275E 01	7,350E 01	7.350E 01	10 0 0 0 P	10 1001	7.768E UI	8.158E 01	8.439E 01	8.725E 01	A.726F 01	***

| | READING = 0094 BLOCK = 143 TIME = 233,142 MACH 5.2 PT = 299,500 TT = 2941.8

## RAMJET PERFORMANCE

t = 234.04 sec.

The injected fuel is possibly unburned.

READING = 0094 BLOCK = 144 TIME = 234,042 MACH 5,2 PT = 298,250 TT = 2936,8

<b>⊢</b>			GAMKA		SONV	MACH	VEL	s	N/N	3	A/AC	MOVIV	ø	IVAC	H.	ETAC
651.6		1231	1.2955	28.867 28.866	2560	5,170	5737	1.885	0.08017	17.781	0.8659	3255	7.148	183.1		
51.		778) 761)	1.2954	28.866 28.866	2560 2537	0,361	915	2.092	0.08017	17.781	0.8659	3502	1.140	197.0		
51.		778)	1.2955	28.867 28.866	2560 1130	5.057	5717	1.885	0.08769	19.449	0.8659	3552	7,791	182.6		
51.		778) 757)	1,2954	28.866 28.866	2560 2532	0.401	1016	2,092	0.08769	19.449	0.8659	3552	1,385	182.6		
618.3( 361.5(		745)	1,2990	28.866 28.866	2515 2105	1.703	3585	1.958	0.61905	19.449	0.1121	2681	37.721	137.9		
18. 59.		745)	1.2990	28.866 28.866	2515 2102	1.710	3596	1.958	0.61555	19.449	0.1234	2733	34.397	140.5		
`		745)	1.2990	28.866 28.866	2514 2447	0.630	1541	1.970	0.61555	19.449	0.1234	2733	14.746	140.5		
18.7( 07.8(	1- 3	771)	1.3022	27.238	2567 2063	1,912	3944	2.069	0.68020	19.540	0.1122	2680	41.693	137.2	0.16 0	.07
16.2(	7 4	69)	1,3065	26.315 26.315	2576 2112	1,793	3786	2,123	0.68429	19.594	0.1118	2615	40.264	133.4	0.25 0	.03
29.9( 29.9(	L 3	758)	1.3082	26.277 26.277	2562 2092	1.809	3784	2.118	0.68382	19.594	0.1119	2614	40.216	133.4	0.25 0	.01
15.9( 31.2(	<b>-</b> 3	756) 473)	1,3085	26.272 26.272	2559 2092	1.804	3774	2,117	0.68421	19.594	0.1118	2609	40.128	133,2 (	0.25 0	. 8
15.3( 35.6(	1-3	755) 477)	1,3086	26.271 26.271	2558 2100	1.781	3740	2.117	0.68539	19.594	0.1116	2598	39.839	132.6	0.25 0	• 00
11.6(1		067)	1.2566	27.410	2888 2586	1.421	3673	2.226	0.67825	19.594	0.1128	2555	38.717	130.4	0.25 0	1.07
605.7( 384.2(	,	794) 575)	1.3022	26.436	2605 2271	1,466	3329	2,137	0.65587	19.594	0.1166	2514	33.927	128.3	0.25 0	.13
04.7( B6.6(		752) 535)	1,3085	26.295 26.295	2552 2207	1,497	3304	2,119	0.65494	19.594	0.1168	2506	33.624	127.9	0.25 0	-02
602.7( 391.5(		744)	1,3097	26.274 26.274	2541 2205	1.474	3251	2.117	0.65242	19.594	0.1173	2488	32,960	127.0	0.25.0	. 00
02.6( 91.7(		743)	1,3098	26.271 26.271	2540 2204	1.474	3248	2,116	0.65202	19.594	0.1173	2487	32.910	126.9	0.25 0	00.
109		735) 508)	1,3106	26.271 26.271	2529 2158	1,566	3380	2.127 (	0.61414	19.594	0.1246	5424	32,260	125.3 (	0.25 0	00.00

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PAGE																					
	ETAC	.53	0.08	.01	0.00	00.	00.	.01	90	00.00	0.00	91.	.03	.00	00.0	90	00.0	00	8	.01	
	PHI	.25 0	.25	.25 0	.23	.25 0	.25 0	.27 0	.27 0	.27		.27 0	.27 0	.27 0	0.27	.27 0	0.27	.27 0	.27 0	.27 0	
	IVAC	5.1 0	5.10	5.3 0	5.1 0	6.8	.4.	9.0	30.8 0	.0		. S. O	9.6	9.	134.7 0	1.7	σ.	5.0 0	5.3	'n.	
	=	1 125	77 129	5 12	36 126	9 126,	9 128	61 130	55 13(	3 131	0 131	4 132	3 139	75 134		6 134	5 134	50 139	9 13	5 135	
	œ	31.171	31.17	29.04	27.43	25.709	22.039	18.46	18.45	17,363	16.390	15,364	12,323	12.57	12,484	12.366	12.35	12,35	12.19	12,355	
	MOMTH	2451	2451	2456	2471	2485	2521	2569	2578	2587	2596	2608	2652	2653	2655	2656	2659	2661	2667	2670	
		m		-														76	. 53		
	A/AC	0.1338	0,1338	0.1436	0.1554	0.1662	0.1950	0.2379	0.2480	0.2631	0.2782	0.2970	0.3678	0.3689	0.3717	0.3675	0.3686	0.369	0.375	7775.0	
		.594	.594	594	594	.594	.594	.708	708	.708	19.708	.708	.708	708	19.708	708	19.708	.708	708	.708	
2936.8	_	19	61	6 19	19	61	19	19	19	19		16	19	7 19.		19		19	19	61	
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P.	MACH	1.446	1,620	1,659	1.723	1.731	1.752	1.800	1.927	1,924	1.921	1,792	1.885	1.977	1.981	1,915	1.923	1,929	1,878	1,995	
5.2	SONV	2750 2427	2558 2166	2520 2114	2512 2082	2509 2076	2504 2063	2501	2496	2494 1986	2492 1985	2590 2129	2504 2011	2491 1962	2489 1959	2489 1984	2488 1981	2487 1978	2531 2038	2491 1956	
MACH	MOLWI	26.958 26.960	26.371 26.371	26.286 26.286	26.273 26.273	26.271 26.271	26.271 26.271	26.048 26.048	26.039 26.039	26.038 26.037	26.037	26.299	26.076 26.076	26.043	26.038 26.038	26.038 26.038	26.037	26.037 26.037	26.149 26.149	26.054 26.054	
.042	X X	808 26 070 26	068 26 344 26	10 26 193 26	18 26 20 26	20 26 25 26	24 26 35 26	35 26 62 26	40 26 08 26	42 26	43 26 10 26	27 26 58 26	28 26 83 26	43 26	45 26 32 26	45 26 10 26	46 26 14 26	46 26 16 26	96 26 50 26	41 26 33 26	
234	GAMA	1,280	1,306	1,31,	1.34	1,31	1,31	1,34	1,31	1,31	1.31	1,30	1,34	1,310	1,31,	1,31	1,31	1,31	1.30	1,31	
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234	GA	-	'n	•	1.31	1.35		1,31	1,34		1.31	1.34		1.30	1.3		1.3	1.36		1.3	1,38		7	1.30		1:30	7		7.2	7		1,33	1.3
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BLOCK = 144 TIME = 234,042 MACH 5.2  18	BLOCK = 144 TIME = 234,042 MACH 5.2  18
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DING ABS 5506E 5506E 5506E 5506E 5506E 5506E 5506E 5506E 5506E 5506E	READING  XABS  6.506E 6.609E 6.609E 6.909E 7.106E 7.106E 8.158E 8.158E

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PEADING = 0094 BLOCK = 144 TIME = 234,042 MACH 5,2	PT = 298.250 TT = 2 RAMJET PERFORMANCE	2936.8	PAGE
ENGINE PERFORMANCE		INLET	
CALCULATED THRUST	(LBF) MASS FI (LBF-SEC/LBM) ADDITI (LBF-SEC/LBM) LIMITION TOTAL P	MASS FLOW RAIIO	0.000 (DEGREES) 0.8659 0.0110 0.2402 0.1108 (PSI) 0.2459
STREAM THRUST	INCET PR INCET PR INCET PR KINETIC (LBF) (LBF-SEC/LBM) ENTHALPY (LBF-SEC/LBM)	CESS EFFICIENCY - COESS EFFICIENCY - ENERGY EFFICIENCY - AT PO - SUBSONIC.	0.6751 0.6751 0.8055 0.8662 43.84 (8TU/LBM) 52.55 (8TU/LBM)
MOMENTUM AND FORCES		COMBUSTOR	
INLET FRICTION DRAG	FUEL-A: COMBUSION TO TO TO TO TO TO TO TO TO TO TO TO TO	FUEL-AIR RATIO	0.0083 0.272 0.211 0.2104 0.3355 0.4435
43.93 -878 -922 -13.65 -266 -2266	VACUUM S NOZZLE O PROCESS KINETIC	STREAM THRUST COEFFICIENT - CS COEFFICIENT - CT	1.0170 0.9513 1.112 1.0338
STATIONS		FUEL INJECTORS	
SPIKE TRANSLATION	INJECTORS 1A 1B 1C 2A 2A 2C 3A 3B	STATION 40.400 41.266 44.300 48.741 46.250 54.031 56.216 44.766	VALVE B B

t = 129.55 sec.

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## RAMJET PERFURMANCE

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The injected fuel is possibly unburned.

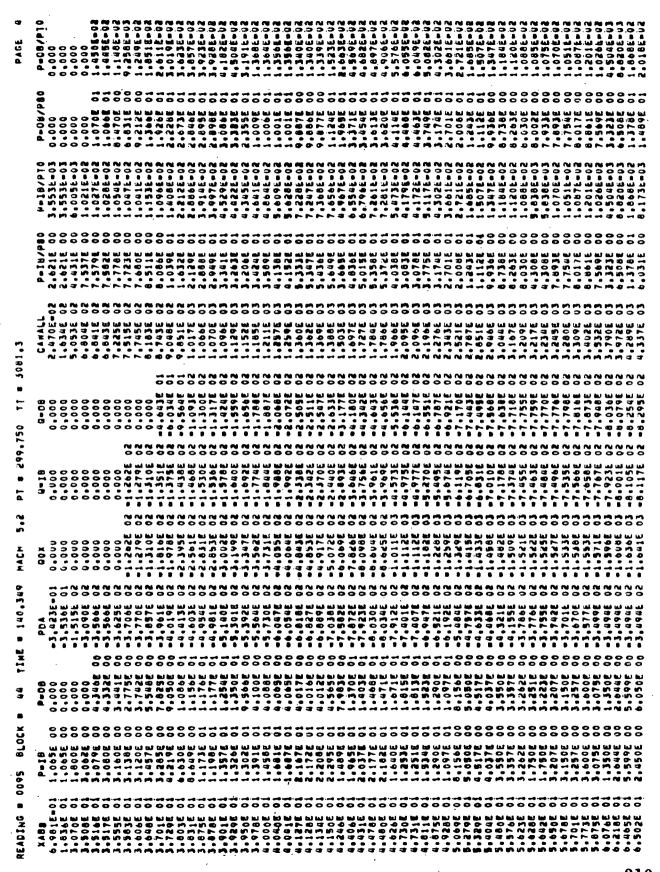
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	A/AC .	0.8655	0.8655	0.8655	0,8655	0.1120	0.1233	0.1233	0.1121	0.1117	0.1117	0.1117	91110	0.1126	0.1165	0.1167	0.1172	0.1173	0.1245
	x	17.010	17.010	17.942	17.942	17.042	17.942	17.942	17,983	18.023	18,023	18.043	16.023	16.023	18,023	18.023	16.023	16.023	18.023
<b>⊢</b> α:	<b>*</b>	0.07673	0.07673	76090.0	46080.0	0.59270	0.56635	0.56635	0.62652	0.6290	0.62978	0.63014	0.63100	0.62486	52409.0	0.60276	0.60042	0.60011	0.56529
OK Per O	w	1.898	2.109	1.898	2.109	1.059	1.959	1.986	2.011	2.065	3.061	2.061	2.062	2.132	2.081	2.073	2.071	2.071	2.072
> 0x	· ver	5865	971	5880	1034	4122	0 4177	1409	1 4297	0 4010	4007	3965	3919	1915	3523	3470	1926 9	3387	5 3416
Z Z	MACH	5.170	0.375	5.103	0.400	Z*011	2.05	0.55	2.127	1,69	1.901	1.868	1.042	*****	1.508	1.50e	1.51	1.917	1.54
<b>⊅</b>	1 80NV	9 2615	9 2614	9 2615	9 2567	9 2569	9 2585	9 2532	2 2609	2622	9 2612	5 2610	4 2128	2777	4 2618	7 2591	6 2583 6 2232	4 2583	4 2571
	MOLKI	28.91	26.91	26.91	26.91	26.91	28.91	20.02	28.112	27.319	27.289	27.28	27.28	27.897	27.37	27.29	27.28	27,284	27,28
	SAMA	1.2906	1.2903	1.2906	1.2903	1.3924	1.2929	1.2929	1,2946	1.2070	1.2990	1.2942	1.2994	1.2731	1.2970	1.3004	1.3012	1,3013	1.3022
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	•		T.		GAMFA	MOLWI	30×	MACH	<b>VEL</b>	•	<b>4/</b> 4	£	34/4	MOFIF	œ	IVAC	A H	ETAC		
CZ C	61.461	19 1 2831 2033	2 2 633. 390.	787)	1.2998	27,352	2586	1.576	9440	2.078	0.52514	16,023	0.1340	1872	284.85	137.7	91.0	90.0		
800	63.337	- E	433	771) <b>52</b> 9)	1.3294	27.294	2567	1.597	3492	2.071	0.52608	16.023	0.1336	1002	20.546	137.0	0.14	10.0		
0 0 0	64.087 15.285	_	9 9 9 E	765) 523)	1.3031	27,285	2559	1.606	1691	2.068	0.49033	16,023	0.1435	6182	20.018	139.7	0.14	0.00		
្ត ១	18.881		527	162	1.3034	27.284	2555	1.711	3645	2.067	0.45281	18.023	0.1554	2555	25.050	141.6	0.14	00.0		
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	\$0.11.0 \$0.11.0	2729	103.50	464)	1,3028	27.311	2556	1.063	2000	2.072	0.36043	18.023	0.1450	2643	22.381	146.6		60.0		
	5.030	t 4	612. 252.	753) 394)	1.3051	27.055	2543	2.204	7077	2.087	0.29769	16.137	0.2379	2700	19.634	140.9	41.0	0.02		
0 M	54.829	-25	611	748)	1,305,	27.043	4536	3.20	4207	2.066	0.28553	10.137	0.24.0	2709	19.007	1 00 .	• 1 • 0	00.0		
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900	45,391 3.262	<b></b>	900	750)	1.3052	27.066	1887	2.340	4363	2.100	0.19249	18.137	0.3879	2778	111-11	153.2	9.10	. W.		
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	45.226	2002		743) 337)	1.3063	27.041	2530	2.511	4512	2.09B	0.19057	10.137	0.3716	27.80	13.363	193.3	. 910	0000		
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267	.2( 759) .5( 413)	1.5008	27.655	1959	2.133 4	177 2.	004 0.65242	18,726	6 0.1121	2739	42.355	146.3	0.0	0.07
ii.	61 •4( 762) •1(. 461)	1.3044	26.951	2002	1.889 3	896 2.0	64 0.0561	4 18.77	5 0,1117	1592	39.725	141.2	0.18	40.0
77.	.3( 753) .6( 452)	1.3058	26.916	2546	1.904 3	692 2.	058 0.05606	18.77	5 0.1117	2650	39.684	141.1	0.18	0.01
, ne .		1.3061	26.911	2593	1.691 3	3871 2.0	58 0.65643	16.77	5 0,1117	2043	39.494	140.7	0.18	0.00
323	.8( 750) .4( 462)	1.3062	26.911	2541	1.844 3	3805 2.05	9 0.6573	9 18.77	5 0,1115	2626	58.677	139.9	91.0	0
	21 1.8( 931) 1.2( 650)	1.2769	27.608	2748		3793 2.1	42 0.65093	1 18.775	5 0.1120	2563	38.369	136.5	9.0	99.0
2710 593 1955 362	3( 529)	1,3036	27.012	9912	1.555 3	3401 2.07	76 0.62443	18.77	5 0.1165	2528	33,264	134.0	0.18	0.10
25	.4( 755) .5( 515)	1.3078	26.925	2516	1.539 3	3325 2.06	4 0.6279	1 16.775	5 0,1167	2823	32.443	134.4	0.18	\$.0 <b>.</b> 0
72 587	.0(729) .2(528)	1.3081	26.930	2512	1.457 3	3186 2.063	0.0254	7 18,775	5 0.1172	4516	30.968	134.1	91.0	20.0
997	.8( 731) .7( 530)	1.3078	26.938	2513	1,452 5	3180 2,063	0.6251	5 18,775	0.117	2518	30.894	134.1	0.18	20.0
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MACH

BLOCK B MEADING # 0095

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	. #	•	;	0		98.0			49.0			0.86	•		99.0			0.86			0.66	•		98.0	•		0.86			980	•		0.66			99.0			99.0
	TVAC		,	*		186.3			187.7			187.2			186.4			186.2			187.2			243.3			252.9			248.7			259.6			283.1			230.6
	3	)	•	2513 14.076 18/.4 0.00 0.36		3651 13.107 186.3 0.46 0.69			3621 11.323 187.7 0.86 0.82			3611 12.019 187.2 0.86 0.80	•		5595 11,000 186.4 0,86 0,80			4.752 186.2 0.85 0.81			3610 7.256 187.2 0.86 0.81			4.307 243.3 0.86 0.83			2.787 252.9 0.86 0.81			4.390 248.7 0.86 0.81			4.752 259.0 0.86 0.81	•		4.427 283.1 0.66 1.00		1	4449 4.958 230.6 0.86 0.81
	100			6166		3651			3621 1			3611 1			1895			3592			3610			1003			4878			4797			2004			5461			7777
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4 MACH	GAMMA MOLLI SONV		23.161		23.475	23,579		23,621	23.977		23,770	23.417		23,780	23.420		23,608	25.947	•	23,704	23.802		23,808	24.079		23,808	24.080		25.704	640042		23,704	24,080		24.333	24,818	3	22000	0
INE # 160,149 MACH 5,2	GAMA		469) 1,2251 23,161 3294	300307	1.2012	276) 1.2405 23.579 3097	•	693) 1,1749 23,621 5598	1.1956		1.1799	1.2045	•	1.1798 23.780 3382	1.2030		1.1764 25.608 3383	1.1962		736) 1,1669 23,704 3430	1.1745		1.1764	7843 1.2870 24.079 2532		628) 1.1764 23.808	1.5013		736) 1.1669 25.704 3430	1.2802		736) 1,1669 23,704 3430	1.2959		1.1636	540) 1.3073 24,818 2142		11120	1.6/27
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18 S600	a.				~	.325	0	.359	0.087	0	271	009.	0	.321		0	290	277	EGER		.437		.062	77		290	0.4.0	REFER	28.062	0.040	REGEN	290	0.410	MBUBIR	9.257	0.410	44LE		ה ה
READING .	-	Demo	57,735		8,755	6.73	OHBO	0.765	0.765	2	2·10	2.18	USTOR	079.7	679.7	810	5.025	5.025	OFBUBIO	5.025	5.025	1 31220	7.261	7.261	OZZLE PU	7.261	7.261	OZZLE AE	-	1090/	DZZEE PO	7.261	7.201	ICTIVE CO	5.025	52.	ICTIVE NU	1000	•

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6.465E 0	1.	1,530€	11 10	.530F	-	4.983E	9	-3.304E	0	*1.621E	0.5	*1.6A3E	3E 03	1 4.249E	13 3.7316	F 03	5.100t-62	4-7316 01	5.100F-10
6.502F 0	1.	.5306	71 17	. 525E		4.9636	20	·5.338E	S	-1.637E	S	-1.701E	IE O	1 4.337E	3 3.751	01	5.1002-02	3.720E 01	5.085F = C2
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6.759E 0		7875	<u>.</u>	924796	ô	7.387£	2	-3.544E	63	•1.722E	0	-1.802E	2E 0.	1 4.665E	.3 1.107	10 3	1.5966-62		2.158E=U2
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6.908E 0		2,367E (	90	3.240	00	9,5296	20	-3.611E	03	-1.749E	0	-1.862E	2E 0.	S LANGE C	15 5.174	1. 00	7.841E=US		1.040E-UZ
6.969E 0	<u>.</u>	9078	ر ا	4.452E	0	1.006E	S	-5.645E	0	-1.758E	0	.1.08	7E 03	1 4.922t u	13 . 447	رد د 0 د	6.153E=03		8.1/45-03
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7.107E 0	- -	1.3056	-	1.26UE	00	1.0016	3	-3.703E	03	-1.775E	0	#1.928E	8E 0]	1 5.088E	3 3.1836	00 31	4.350E=03		0.200E=US
7.260E C		.8156	- 2	388E	0	1,1516	5	-3.749E	03	-1.790E	5	-1.95	FO 35	3 5.273E (	13 4.427	رد د	6.050E=03	3.370£ 00	4.6176-03
7.275E C		. 865E (	90	1.251	06	1.15AE	3	-3.755E	03	-1.7916	03	-1.90	2E 03	5.290E 0	B 4.548	1E 00	6.217£=03		4.169E=U3
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7.403E C	<u>.</u>	.405E (	9	00000		1,234E	5	-3.616E	0	-1.807£	S	-2.00	9E 01	5 5.427E 0	13 3.427	رو و	4.663E=03	00000	00000
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### RAMJET PERFURMANCE

LAINE	ANGLE OF ATTACK	INLET PROCESS EFFICIENCY - SUPERSONIC 0.60007 INLET PROCESS EFFICIENCY - SUBSCNIC 0.6142 KINETIC ENERGY EFFICIENCY - SUPERSONIC 0.6014 AINETIC ENERGY EFFICIENCY - SUBSCNIC 0.6014 ENTHALPY AT PO - SUPERSONIC 255.45 (BTU/LBM) ENTHALPY AT FO - SUPERSONIC 250.45 (BTU/LBM)	COVEUETOR	FUEL-AIR MAID	3727CH	VACULM STREAM THRUST COEFFICIENT = CS 6.9480 NOZZLE COEFFICIENT = CT	FUEL INJECTORS	INJECTURE BTATION VALVE  1A 40.400  1B 41.270  1C 44.300  2C 46.250  E 54.045  3G 56.025
	1040, (LBF) 770, (LBF) 1931, (LBF-SEC/LBM) 1487, (LBF-SEC/LBM) 15209	ANCE 46. (LBF) 99. (LBF) 23. (LBF-8EC/LBF) 727		10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000		14.35 (LBF) 14.05 (LBF) 14.05 (LBF) 14.05 (LBF) 14.05 (LBF) 14.05 (LBF) 14.05 (LBF) 14.05 (LBF)		
ENGINE PERFORMANCE	CALCULATED THRUST	REGENERATIVE CODLED ENGINE PERFORMANCE CALCULATED CALCULATED NET THRUST	SERVICE CAN ACTUAL CONTRACT	•	PONCHE PROBLEM CANADA	EXTERNAL PRESSURE INTEGRAL	BIATIONS	MOPINAL CONL LEADING EDGE

t = 169.15 sec.

シースペース

TO TIME B 160,140 KACA SOR DIB SOO.250 IT B 2935.6 PEADING # 0095 BLOCK #

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	ANGLE OF ATTACK	UELTA PTZ	KINETIC ENERGY EFFICIENTIFE FILLE ENTIFICE NO BUPERS ENTIFE AT PO BUBERS ENTIFE AT PO BUBBON		FUEL-AIR RATIO		VACULT SIREAM THRUSH CO NOZZLE COEFFICIENT & CT PROCESS EFFICIENT & CT AINETIC ENERGY EFFICIEN	FUEL IN	INJECTORS STATION 40,400		. Nww.a	
	(LBF) (LBF) (LBF=8EC/LBF) (LBF=8EC/LBF)	:44	( #E=8EC/LBM) (LBF) (LBF)				_					
	993. 1086. 1606.	. 0.5154 . 0.5636 RFURMANCE	4566. 1105. 1747.		44 84 84 84 84 84 84 84 84 84 84 84 84 8	917	Meradon		100 C	35.169	67.261 56.423 65.025 65.025	
ENGINE PERFORMANCE	CALCULATED THRUST	CALCULATED THRUST COEFFICIENT		MONENTUM AND FUNCES		NOTZER TOMBATCH CHANGE	EXTERNAL PRESEURE INTEGRAL TOTAL STRINAL DRAG. TOTAL STRUT DRAG. TOTAL STRUT DRAG. TOTAL STRUT DRAG. TOTAL STRUT DRAG. TOTAL STRUT DRAG. TOTAL STRUT DRAG. TOTAL STRUT DRAG. TOTAL STRUT DRAG. TOTAL STRUT DRAG. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTAL STRUT. TOTA	SACITATE	NOTINAL COME LEADING EDGE	NOVAL EMPLY EDGE	NOZZLE PLUG TRAILING EDGE	

t = 189.85 sec.

READING = 0095 BLOCK = 49 TINE = 189.849 MACH 5.2 PT = 300.250 TT = 2937.7 RAMJET PERFORMANCE

SUNNARY REPORT

IVAC PHI FTAC 2530 22.606 132.1 0.45 0.03 2531 22,750 132,2 0,45 0,04 7,178 183.0 1,188 191,5 7,573 182,7 2769 41.420 146.7 2807 38.098 148.7 2596 35.221 137.5 2544 32.594 134.8 2536 32,287 134.3 1,342 182.7 2807 12,507 148.7 2768 40.703 146.6 2675 38.015 141.7 2659 37,550 140.8 2536 32,302 134.3 2682 38,205 142,1 2551 32.860 135.1 3450 3419 3268 3450 NONTE 28.919 2533 0.375 949 2.093 0.08054 17.855 0.8655 28.919 2557 28.919 2550 0.401 1014 2.093 0.08516 18.879 0.8655 28.919 2507 28.919 1957 2.071 4052 1.934 n.62214 18.879 0.1120 28.919 2507 26.919 1941 2.112 4099 1.934 0.59803 18.879 0.1233 28.919 2507 28.919 2455 0.548 1346 1.964 0.59803 18.879 0.1233 1,3016 28.919 2473 1,3278 28.919 2113 1,581 3341 1,953 0,63291 18.679 0,1165 24,408 2600 24,408 2422 1.006 2437 2.230 0.60061 19.150 0.1245 28.919 1109 5:170 5735 1.884 0.08054 17.855 0.8655 28.919 2557 28.919 1122 5.100 5722 1.884 0.08516 18.879 0.8655 28.919 2500 28.919 2047 1.821 3727 1.944 n.65969 18.879 0.1117 28.919 2498 28.919 2064 1.771 3655 1.946 n.66103 18.879 0.1115 1.3022 28.919 2465 1.3279 28.919 2112 1.565 3305 1.953 n.62860 18.879 0.1173 24.406 2421 1.009 2442 2.236 0.60090 19.150 0.1244 28.919 2507 28.919 1979 2.012 3982 1.934 0.65775 18.879 0.1121 28.919 2052 1.806 3706 1.944 n.66006 18.879 0.1117 28.919 2489 28.919 2104 1.646 3463 1.951 0.65453 18.879 0.1126 28.919 2470 28.919 2115 1.571 3322 1.953 n.63138 18.879 0.1167 28.919 2465 28.919 2112 1.565 3305 1.953 n.62893 18.879 0.1172 A/AC \* / 4 7£1 MOLET SONV MACH 28.919 1.2949 1.2951 1.2949 1.2990 1.2990 1.2990 1,2990 1,2326 1,2995 1.2997 1.3284 1,3018 1,3278 772) 1,3140 654) 1,3260 7771 1.2951 1,3140 653) 1,3261 GAMMA 1771 740) 712) 711) .(111) 757 415) 705) 734) 496) 7151 126) 728) 111) 171) (01/ 426) 7361 735) 491) 740) 1094 463) (04) 475.9( 3.2 651.2 633.2 .30.7 984.4 366.1 13. 88. 90 0.000 0.384 512 SPIKE TIP NS 2 0.600 14.275 2936 0.600 13.045 2878 1956 2726 1959 300,250 2938 00 119,849 2813 13.637 1662 119,849 2813 1954 862 15.032 97,366 63,915 17,300 17.499 63,127 33,793 101,342 100.145 67,202 9.574 19.924 19.804 9,100 968.61 8.281 19,872 19,853 119,941 IND TUNNEL CMBUSTOR

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IVAC	137.1	137.0	141.9	142.6	142.7	146.8	157.0	168.5		174.0	176.8	179.9	188.3	188.5		189.1	189.9	
ø	16,691	16.722	16.280	18.561	18,577	19,435	16.717	17.468		17.070	17.052	16.323	12,915	14.165	#.0 <b>.</b>	13,140	13,264	
MOMTK	2625	2623	7172	1112	2778	2859	3056	3301			3464	3525	3688	3692		3704	3719	
A/AC	.1340	1338	1,1435	,1552	1554	.1662	1950	.2379		.2631	.2782	.2969	.3679	.3698	.3716	.3674	.3688	, ,
3	19.150 0	19.150 0	19-150 0	19.472 0	19.472 0	9.472 0	19.472 0	19.588 0		19.588 0	9.588 0	19.586 0	19.588 0	9.588 0	9.588 0	9.588 0	19.588 0	
<b>4/B</b>	.55795	.55895	.52097	.48985	.48922	.45754 1	.38995	.32150	*	.29067	.27487 1	.25758 1	.20788	.20726 1	20561 1	0.20815 1	0.20739 1	1
v	.236 n	.235 0	.258 0.	.541 0.	.541 0.	.565 0.	.614 0	. 68	673 0	0 000	683 0	0 169	.738 O.	.721 0.	.722 n.	.737 0.	.0 787.	
VEL	1925 2,	1925 2.	11 2	2438 2.	2443 2.	2733 2.	2759 2.	. 96		3779 2.	3992 2.	4678 2.	3998 2	398 2,	4408 2.	4062 2,	4116 2.	
MACH	.766	.767	.775 20	.924	0.925 2	•10.	.961	.186 34	.206 3	.272	353	365	.252 3	B 1111.	844.	.274	.291	
NOS	2619 2512 U	2617 2510 0	2702 2593 0	2639 0	2806 2640 0	2881 2683 1	3046	3198 2947 1	3226 ·	3250	3260 2950 1	3295 2987 1	3415	3364 3045 1	3368 3050 1	3418 3190 1	3420 3187 1	3399
MOLWT	24.479	24.475	24.701	20.787	20.790	20.932	21.295	21.613		21.792	21.837	21.973	22.518 22.604	22.261 22.310	22.279	22.535	2,553	22.437
GARMA	1,3114 2	1.3189	1.3093	1.3182	1,3180	1.3231	1.2906 1	1.2681	1.2628	2577	2553	1.2468	1.2386	1.2257	1.2243	1.2386 2	1.2383 2	1.2124
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<b>و</b>		2,463 3,113	0.261 1.359			53,427		0 44.028 19.250	2.996 8.367	1.961 5.446	1.361			34,586 4 10,733	34.441 10.675		33.061 ( 12.850 :	34.231
BUSTOR		-							3-	30.5103 34.5 34.5 34.5	_			-,	-,			

99 TIME = 189,849 MACH 5.2 PT = 300,250 TT = 2937,7

READING = 0095 BLOCK =

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g	,	3758 16.145 191.9 0.99 0.39		. 7 00 4 F 10: 100 F 1 84CF			F 0 00 4 0 000 077 51 0FTF			375	O'CT TYPOLA TAGE! BEAD O'C			3/54 10.008 190.0 0.99 0./c		9	7'-0 A6'-0 1916' 0'-3A 0'-1		4 443	***** S+8.2 6.3% 0.74		2 BKR 2KB & B 00 0 12			4 5 50 0 6 2 CRC 05 4	•		"T 0 00 0 7 170 468 6			4 318 204 8 8 00 1 00			4.092
MONTA		3758		4740			4740			1000	216			3776		935	F + / D		6 20 4	7004		9.0			4947			6161			SART	}		4605
A/AC		1.3777		3450			14654			474.	A +		4000	3501		9104	3001		6473	776		75.66			4372			3906			5045			.9371
3		19.588		19.5AA			AGS.			S. S. S.	000.61			000.41			000061			000.61		F ARR T	,		14.5AA 1			F. 588.			9.5AA 2			9.588 1
4/#	-	1.940 5131 2.664 0.20249 19.588 0.3777	•	1.958 UNEN 2.738 0.20054 18.588 8.3658			1.166 3891 9.740 0.91500 18.548 0.3551		,	1.086 3480 2 746 0.90400 to 888 A 1748	20103	(1740) 1.1764 22.801 3452	1004	6000		(1664) 1.1813 22.958 358 0.903 484; 9 77; 0.1805K 18 888 6 4040			# 70 KO	7100 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 1000 T 10		1 674) 1.3026 23.165 2387 3.245 7744 9.743 0.02479 48.888 4.9946		(1792) 1.1688 22.822 3490	846E0		(1792) 1.1688 22.822 3490	FORCU	,		( 625) 1.2943 24.282 2273 4.003 9100 2.636 0.03054 19.588 2.5045		(1712) 1.1731 22.867 3423	.03948
s		2.064		2.734 n			2.740 0			9.746.0			9 783 c	2 22 2		9 771 0			2.753.0	-		9.783 0			2,771 0			9.771 0			2.636 0			2.789 0
VEL		1616		4040			1921			38,00			7011			TAK!			7974	-		7744	:		7384			7899			9100	,		6999
MACH VEL		046.		1988			166			.086			.039			F 06 4			7181			245		•	.786			1.234			.003	)		.419
NOS	5228	C # 0.2	34.39	\$229		5452	5277		2452	5303		3452	1322		0000	288		14.52	582		5452	1387		3490	651		24.90	2442	!	1881	273 4	)	5423	1757 2
VOLWT :	1.783	26.141	2.717	2.840		2.820	2.957		2.877	3.013	)	106-24	3.034		. 859	2.952		106.30	3.165		2.901	3.165		2.822	3.165		2.822	3.165		3.519	4.282		2.887	3.164
GAMMA FOLKT SONV	(1326) 1.2610 21.783 3228	~	(1689) 1.1914 22.717 3439	1,2251 2		(1723) 1,1837 22,820 3452	1.2112 2		(1735) 1.1795 22.877 3452	2025		1.1764 2	1960 2		1.1684	1,1813		1.1764 2	2878		1.1764 2	1.3026		1.1688 2	1.2825 1		1.1688 2	2 5883		1.1543 4	2 5943		1,1731 2	1.2738 2
	1326)		16891	1422)		1723)	1497)		1733)	1540)	1	1740)	1572)		1792)	1664)		1705)	614)	•	1705)	6745		1792)	1698		1792)	712)		1979)	625)		1712)	957)
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<b>-</b>	38 3620				0																9995	2036 .	9	4784	2553	47	4784	2141	29	5254	1950-	99	4598	2781
۵.	46.370	900	33,395	13.650		33,571										18.256		.065				914.0		29.065					COMBUSTR	119.049	0.416	NOZZLE	18.081	
	COMBUSTOR 58.755 58.755	COMBUSTOR	60.765	60.765	CCMBUSTOR	62,185	62,185	COMBUSTOR	649.49	649.49						65,025	NOZZLE AE	87,261	87,261	NOZZLE PO	•				_	W	_	~				ICTIVE P	87.261	

11 = 2937.7
PT = 300.250
MACH 5.2
: 189,849
99 TINE
BLOCK =
ADING = 0095

READING = 0095 BLOCK = 99 TIME = 189,849 MACH	5.2 PT = 300.250	11 = 2937.7			PAG
	RAMJET PERFORMANCE	RMANCE			
ENGINE PERFORMANCE			INLET		
CALCULATED THRUST	(LBF-SEC/LBM) (LBF-SEC/LBM)	ANGLE OF ATTACK	ANGLE OF ATTACK	0.000 0.000 0.0110 0.2533 0.0917	(NEGREES) (PSI)
RFORMANCE 4686. 1201. 1976. 0.6190	(LBF) (LBF-SEC/LBM)	PRESSURE RE PROCESS EFF PROCESS EFF IC ENERGY EF IC ENERGY EF LPY AT PO -	RECOVERY - SUBSONIC FFICIENCY - SUBSONIC FFICIENCY - SUBSONIC EFFICIENCY - SUBSONIC EFFICIENCY - SUBSONIC SUPERSONIC SUBSONIC	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	(RTU/LBM)
MOMENTUM AND FORCES			COMBUSTOR		
	(LBF) (LBF) (LBF) (LBF)	FUEL-AIR RATIO	100 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.995 0.742 0.742 0.7523 0.7523	
0.00 883.	(LBF) (LBF)		NOZZLE		
2000 2000 2000 2000 2000 2000 2000 200	(185) (187) (187) (187) (187)	VACUUM STREAM THRUST NOZZLE COEFFICIENT PROCESS EFFICIENCY KINETIC ENERGY EFFIC	STREAM THRUST COEFFICIENT - CS	0.8696 0.8771 0.8612	
STATIONS		Fue	FUEL INJECTORS		
NOMINAL COML LEADING EDGE		INJECTORS 1A 1B	STATION VAL 40.400 41.270 44.300	VALVE	
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## RAMJET PERFORMANCE

INLET	1		COMBUSION  0.0275  0.0275  0.0256  0.7756  0.7756  0.7756  0.7756  0.7757  0.7756		<u>v</u>	VALVE D E
1	LOW RATIO	INCEL PROCESS EFFICIENCY - SUPERSONIC INCET PROCESS EFFICIENCY - SUBSONIC KINETIC ENERGY EFFICIENCY - SUBSONIC ENTHALPY AT PO - SUPERSONIC ENTHALPY AT PO - SUBSONIC	FUEL-AIR RATIO	NOZZLE VACUUM STREAM THRUST COEFFICIENT - CS PROZZLE COEFFICIENT - CT KINETIC ENERGY EFFICIENCY	FUEL INJECTORS	10 40.400 10 40.400 10 41.270 10 20 44.300 20 20 48.745 20 20 54.035 38 56.220 44.770
	014, (LBF) 958, (LBF) 939, (LBF-SEC/LBM) 833, (LBF-SEC/LBM) 5223 4936	NCE 4. (LBF) 5. (LBF) 3. (LBF-SEC/LBM) 44	95.9 (LBF) 16.4 (LBF) 65.6 (LBF) 0.86 (LBF) 64.9, (LBF)	NO		0.2849 (IN) 0.2849 (IN) 40.400 (IN) 155.169 (IN) 75.509 (IN) 56.425 (IN) 65.025 (IN) 67.025 (IN)
ENGINE PERFORMANCE	CALCULATED THRUST	STREAM THRUST		7 77778	STATIONS	NOMINAL COWL LEADING EDGE
54	:				-	·

t = 204.25 sec.

BLOCK # 115 TIME = 204,249 MACH 5,2 PT = 300,250 TT = 2942.9
RAMJET PERFORMANCE . READING = 0095

SURMARY REPORT

FTAC 2484 31.101 130.2 6.34 0.01 2484 31,115 130.2 6.34 0.07 F IVAC 1,185 191.9 1.343 182.9 7,173 183.2 7.580 182.9 2780 41.643 147.2 2018 12.510 149.3 2668 37.707 141.3 2535 31,997 134,3 2818 38.280 149.3 2779 40,910 147.2 2691 38.375 142.6 2685 38,180 142.2 2560 32.946 135.6 2552 32.640 135.2 2534 31.960 134.2 2605 35.326 138.0 3453 3453 3265 3421 KOKTY 25.321 2562 25.321 2204 1.517 3344 2.175 0.59850 19.083 0.1245 5.170 5741 1.884 0.08040 17.824 0.8655 948 2.094 0.08040 17.824 0.8655 28.919 2560 28.919 1124 5.098 5728 1.884 0.08516 18.878 0.8655 28.919 2559 28.919 2532 0.401 1015 2.094 0.08516 18.878 0.8655 26.919 2513 28.919 1958 2.080 4074 1.935 0.62108 18.878 0.1128 1,2965 28.919 2513 1,3411 28.919 1943 2,120 4119 1,935 0,59799 18.878 0,1233 28.919 2513 28.919 2462 0.547 1346 1.965 0.59799 18.878 0.1233 28.919 2506 28.919 2051 1.825 3743 1.945 0.65965 18.878 8.1117 28.919 2506 28.919 2056 1.810 3722 1.946 0.66002 18.878 0.1117 28.919 2505 28.919 2069 1.774 3671 1.947 0.66099 18.878 0.1115 28.919 2122 1.579 3350 1.955 0.63288 18.878 0.1165 28.919 2479 28.919 2124 1.566 3327 1.955 0.63135 18.878 0.1167 28.919 2475 28.919 2132 1.536 3274 1.956 n.62890 18.878 0.1172 28.919 2474 28.919 2132 1.535 3272 1.95m n.62857 18.878 0.1173 25.430 2606 25.430 2262 1.478 3344 2.191 0.59880 19.083 0.1244 28.919 2513 28.919 1981 2.020 4002 1.935 n.65771 18.878 0.1121 28.919 2496 28.919 2110 1.646 3473 1.953 0.65449 18.878 0.1126 A/AC VEL 28.919 2559 28.919 2535 0.374 MACH MOLWT SONV 28.919 2560 28.919 1110 1.2970 1,2949 1.2948 1,3397 1.2949 1.2985 1.5323 1.3319 1.2991 1.2998 1,3009 1.3011 1,3014 1,3125 1,2985 1,3014 1.2948 745) 1.2985 1,3075 416) 778) 761) 778) 126) 778) 758) 745) 745) 408) 709) 740) 463) 740) 465) 739) 472) 733) 194 722) \$000 721) **5**02) 718) 506) 718) 206) 786) 564) 752) 530) -5.8( 123) 745) 634.8( 618.30 286.7( 618.3( 658.8( 632.2( 652.8( 372.7 376.9( 298.1 565.2 613. 553. 13. 336. 300,250 2943 0.384 513 14.287 2943 300,250 2943 V.EUU 12.891 2875 0 12 87.469 2788 14.287 2943 13.564 1669 121.078 2826 12.703 1637 19,915 1973 19.645 1951 121.076 282 79.144 77.130 0.417 14.990 102,029 17.498 97.939 18,003 20.058 77.023 20.464 64.243 100.795 80.115 20.456 WIND TUNNEL 0.000 300.2 0.000 0.4 SPIKE TIP NS 0.000 300.2 0.000 0.3 SPIKE TIP NS 4.ET UNNRSK WIND TUNNEL MBUSTOR DMBUSTOR

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	PHI	. P	40.0	40.0	6.70	6.70	9.70	0.10	0.71	0.71	9.71	0.71	0.71	0.71	9.71	6.71	6.71	0.71	0.71	6.71
	IVAC	131.0	131.0	132.4	131.7	131.7	133.9	140.4	149.6	51	154.8	157.9	161.5	172.7	172.9	173.3	173.6	174.4	175.0	176.6
-	ø	29,185	29.237	25.847	23.756	23.717	21,758	17,313	14.900	14.832	13.998	13,257	13.067	10.580	11.296	11.268	10.697	11.119	11.098	10.806
	MOMIT		2500	2526	2541	2542	2584	2709	2903	10	3605	3665	3136 1	3352 1	3356	3364	3369	3385	3396	3428 1
	A/AC	.1340	.1338	.1435	.1552	.1554	.1662	.1950	.2379	.2480	.2631	.2782	. 2969	.3679	3698	.3716	.3674	.3688	.3693	.3753
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PT =	MACH	.550	.551	.447	.323	.356	.330	.153	.129	.165	.139	.115	. 160	900	.179	.183	116	.144	.140	.115
5.2	SONV	550 179 1	2549 2178 1	2544 2214 1	2682 2380 1	2635 2321 1	2625 2522 1	2501 1	2894 2666 1	2921 . 2680 1	2975	3025 2808 1	3069	3223 3049 1	3210 3000 1	3214	3229 3046 1	3233 3042 1	3240 3053 1	3260 3087 1
9 MACH	MOLWT	25.305 25.305	25.303	25,303	22.511 22.511	22.423	22.410	22.647	22.892	22.967 22.968	23.123	23.283	23.440	24.075	24.012	24.034	24.110	24.136 24.186	24.176	24.302
204.24	GAWMA		1,3138	1,3141	1,3182	1,3229	1.5238	1.3116	1.2937	1.2901	1.2022	1.2739	1.2867	1.2496	1.2575	1.2564	1.2225	1.2209	1.2182	1.2366
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18 Se00	٩		6,151 4,488			48.144 2 16.421 1			38.269 1 17.850 1		5.907	4,537 6,500	3,360		28.930 4 12.916 3		28.914 4 14.010			
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28 31 4 4012 555.4(1515) 4013 56.8(1359) 403 58.6.4(1493) 4013 58.0(1357) 40 33 3 4 40 33 3 4 40 34 3 4 41 34 3 41 34 3 42 33 38 3 42 34 34 34 34 43 34 34 34 34 34 34 34 34 34 34 34 34 3	1.1995 24 1.2204 24 1.2226 24						B	ノにいる		,	IVAC	IVAC PHI	FIAC
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## RAMJET PERFORMANCE

INLET	ANGLE OF ATTACK		COMBUSTOR	FUEL—AIR RATIO	FUEL INJECTORS	INJECTORS STATION VALVE  1A	54.035
50 ENGINE PERFORMANCE	CALCULATED THRUST	STREAM THRUST	STORY CAR ELLINGROPE	INLET FRICTION DRAG	STATIONS	TRANSLATION	

t = 211.45 sec.

5.2 PT = 300.250 TT = 2937.1 RAMJET PERFORMANCE MACH TIME = 211,449 BLOCK = 123 READING = 0095

0 d 3 × SUFFARRAT

PHI ETAC 2497 31.641 130.7 0.29 0.07 IVAC 7.176 183.0 1.184 191.9 2787 41.710 147.2 2826 12.598 149.3 2675 37,701 141.3 2566 32,830 135.5 7.593 182.7 1.346 182.7 2611 35.268 137,9 2826 38,331 149,3 2786 40,950 147.2 2699 38.381 142.5 2692 38,183 142,2 2541 31.855 134.2 2541 31.818 134.2 2497 31,650 130.7 2558 32.516 135.1 3426 3459 3459 3267 **FOV** 28.919 2557 28.919 1123 5.096 5721 1.884 0.08541 18.933 0.8655 28.919 2527 28.919 2529 0.401 1014 2.093 0.08541 18.933 0.8655 28.919 2516 28.919 1965 2.071 4068 1.936 0.62202 18.933 0.1128 28.919 2516 28.919 1950 2.109 4113 1.936 0.59974 18.933 0.1233 20.919 2516 28.919 2464 0.548 1352 1.966 0.59974 18.933 0.1233 2508 2077 1.762 3660 1.949 0.66292 18.933 0.1115 26.919 2467 26.919 2134 1.560 3328 1.957 0.63473,18.933 0.1165 28.919 2461 28.919 2146 1.514 3248 1.958 n.63041 18.933 0.1173 25.817 2585 25.817 2184 1.556 3399 2.146 0.59925 19.106 0.1245 0.8655 0.8655 28.919 2516 28.919 1988 2.009 3995 1,936 0.65964 18.933 0.1121 26.919 2510 26.919 2059 1.813 3733 1.946 0.66158 18.933 0.1117 26.919 2509 26.919 2064 1.798 3712 1.947 0.66195 18.933 0.1117 2501 2120 1.631 3457 1.955 0.65641 18.933 0.1126 28.919 2137 1.546 3304 1.957 0.63319 18.933 0.1167 26.919 2481 28.919 2146 1.515 3250 1.958 0.63074 18.933 0.1172 25.912 2592 25.912 2234 1.521 3398 2.160 0.59955 19.106 0.1244 5.171 5734 1.884 0.08053 17.852 946 2.093 0.08053 17.852 VEL KACH 0.374 MOLWT SONV 1109 2557 2533 28.919 28.919 28.919 26.919 1.2950 1.2983 1,3392 1.2983 1.2983 1.5517 1.2989 1,3262 1.3007 1.3254 1,3063 1.2951 1,2983 1.2994 1.2988 779) 550) 723) 513) 723) 514) 751) 521) 736) 507) 725) (11) 1771 126) 411) 743) 467) 742) 470) 742) 476) 727) 2937 2878 1998 2004 2020 2761 2937 14.312 14.312 120.377 120,377 0.384 13,087 300.250 0.418 3.695 76.442 12.913 15.031 101.476 846.94 19,990 79.512 64,321 120.501 17.536 100.253 97.419 18.263 20.359 78,546 20,952 20.517 20,961 PIKE TIP NS SPIKE TIP NS WIND TUNNEL 0.000 300 0.000 0 OMBUSTOR

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IVAC	31.7	131.7	33.0	32.5	32.5	34.0	38.0	41.6	42.2	# 0° 8	7.94	49.8	64.49	164.6	65.1	65.4	4.99	67.1	169.2
	.973 1	.032	.773 1	.672 1	.842 1	.373 1	434 1	.725 1	265 1	.227	.385 1	192 1	.817 1	.925 1	631 1	.631	.750 1	.566	7.763 1
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	19.106	19.106	19.106	19.273	19.273	19.273	19.273	19.387	19.387	19.387	19.387	19.387	19.387	19.387	19.387	19.387	19.387	9.387	19.387
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	25.803	25.801 25.801	25.801	23.497	23.423	23.411	23.410	23.266	23.260	23.515	23.839	24.036	24.776	24.797 24.818	24.827	24.838	24.891	24.918	24.939 24.961
	1,3116	1,3117	1,3120	1,3155	1,3193	1.3200	1,3206	1,3217	1.3221	1,3094	1.2935	1.2993	1.2422	1.2409	1,2391	1,2385	1,2353	1.2338	1,2330
	743) 504)	742) 503)	739)	797) 562)	769) 534)	763) 524)	756) 527)	752)	748)	<b>6</b> 40)	954) 785)	1019)	1262)	1268)	1135)	1142)	1295)	1302)	1305)
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11 = 2937.1	W/W	1.2355 24.914 3120 1.2478 24.932 3031 0.760 2304 2.474 0.20041 19.387 0.3777	1,2313 25.002 3131 1,2450 25.025 3034 0.801 2431 2.473 0.20739 19.387 0.3658	0.885 2687 2.475 0.21301 19.387 0.3553	3142 2987 1.031 3080 2.478 0.20191 19.387 0.3749	1.2250 25.123 3139 1.2471 25.161 2990 1.014 3032 2.483 0.18771 19.387 0.4032	1.2111 25.081 3205 1.2314 25.137 3080 0.950 2927 2.507 0.18771 19.387 0.4032	1.2250 25.123 3139 1.3176 25.182 2208 2.890 6381 2.483 0.03907 19.387 1.9371	1.2262 25.123 3139 1.3282 25.182 2080 3.201 6659 2.483 0.02749 19.387 2.7538	1.2111 25.081 3205 1.3104 25.182 2300 2.847 6550 2.507 0.03907 19.387 1.9371	3.192 6877 2.507 0.02635 19.387 2.6728	1.1975 25.839 3281 1.3344.25.999 1694 4.140 7839 2.375 0.03924 19.387 1.9290	1.2166 25.127 3117 1.3119 25.162 2260 2.674 6098 2.497 0.03907 19.367 1.9371
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300	VEL	2304	2431	2687	3080	3032	2927	6381	6839	6550	6877	7839	8609
<u>-</u>	MACH VEL	0.760	0.801	0.885	1.031	1.014	0.950	2.890	3.201	2.847	3.192	4.140	2.674
2.5	SONV	3120 3031	3131 3034	3150 3035	3142	3139 2990	3205 3080	3139 2208	3139 2080	3205 2300		3281 1694	3117
9 MAC	GAMMA MOLWT SONV	24.914	25.002	25.120 25.152	25,128 25,167	25.123 25.161	25,081 25,137	25,123	25.123 25.182	25.081 25.182	25.081 25.182	25.839	25.127 25.162
= 211.449 MACH 5.2 PT = 300.250	GAMMA	1.2355	1.2313	1.2245 25.120 1.2415 25.152	1,2251 25,128	1.2250	1,2111	1.2250	1,2250	1.2111	1.2111 25.081 3205 1.3219 25.182 2154	1,1975	1.2268
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NEADING     00%5   BLOCK     123   TIME     211.449	VACH	5.2 PT = 300.250	TT = 2937.1			PAGE
ENGINE PERFORMANCE	•	KAMJEI PEKFOKMANCE	IRMANCE	TB INI		
CALCULATED THRUST	571. (L 420. (L 1613. (L 1186. (L 0.2938	(LBF) (LBF-SEC/LBM) (LBF-SEC/LBM)		ANGLE OF ATTACK MASS FLOW RATIO ADDITIVE DRAG COEFFICIENT LIWITING PRESSURE RECOVERY FFFICIENCY UELTA PT2 TOTAL PRESSURE RECOVERY - SUPERSONIC	0.000 0.8655 0.0110 0.2549	(DEGREES)
REGENERATIVE-COOLED ENGINE PERFO CALCULATED STREAM THRUST	PERFORMANCE 4186. (L 1952. (L 0.3555	(LBF-SEC/LBM)	TOTAL PRESSURE RECOVERY + INLET PROCESS EFFICIENCY + KINETIC ENERGY EFFICIENCY KINETIC ENERGY EFFICIENCY KINETIC ENERGY EFFICIENCY KINETIC ENERGY EFFICIENCY ENTHALPY AT PO - SUBSONIC,	SUBSONIC SUPERSONIC SUBSONIC SUPERSONIC SUPERSONIC		(RTU/LBM)
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STATIONS				FUEL INJECTORS		
NOMINAL COWL LEADING EDGE SPIKE TRANSLATION. INLET THROAT. COWL LEADING EDGE. NOZZLE SHROUD TRAILING EDGE. STRUT LEADING EDGE. STRUT LEADING EDGE. COMBUSTOR EXIT.	34.884 40.2864 40.2400 43.169 73.509 73.509 657.261 65.028 65.028		1NJECTORS 1A 1B 1C 2A 2A 3A 3A 44	STATION 40.400 41.270 44.300 46.745 66.250 56.220 44.770	<u>u</u> >	

t = 217.75 sec.

SUMPARY REPORT

FTAC 2508 30.245 131:0 6.34 0.07 2508 30.226 131.n 0.34 0.01 PHI IVAC 7.163 183.2 2681 37.871 141.5 2793 41.906 147.5 2632 38.464 149.5 2632 12,572 149,5 2793 41,112 147.4 2705 38.549 142.8 2698 38.352 142.4 2569 32,974 135.6 2562 32.676 135.2 2547 32.099 134,4 2616 35.421 138.1 2546 32.065 134.4 3261 3430 3465 3465 MOVIE 5.171 5742 1.885 0.08027 17.795 0.8655 28.919 2560 28.919 1125 5.092 5728 1.885 0.08545 18.942 0.8655 28.919 2560 28.919 2532 0.401 1015 2.094 6.08545 18.942 0.8655 25.348 2252 1.451 3239 2.176 0.60046 19.146 0.1245 28.919 2550 28.919 2536 0.372 943 2.094 0.08027 17.795 0.8655 28.919 2516 28.919 1946 2.119 4125 1.935 0.60002 18.942 0.1233 28.919 2516 28.919 2465 0.547 1348 1.966 0.60002 18.942 0.1233 28.919 2510 28.919 2055 1.824 3748 1.946 0.66189 18.942 0.1117 28.919 2510 28.919 2060 1.809 3726 1.946 0.66226 18.942 0.1117 28.919 2608 28.919 2073 1.772 3674 1.948 0.66323 18.942 0.1115 28.919 2500 28.919 2116 1.640 3471 1.954 0.65671 18.942 0.1126 26.919 2485 26.919 2129 1.570 3341 1.956 0.63502 18.942 0.1165 28.919 2137 1.532 3273 1.957 0.63103 18.942 0.1172 28.919 2479 28.919 2137 1.531 3271 1.957 0.63070 18.942 0.1173 28.919 2516. 28.919 1960 2.085 4086 1.935 0.62007 18.942 0.1128 28.919 2516 28.919 1965 2.020 4009 1.935 n.65994 18.942 0.1121 28.919 2483 28.919 2131 1.557 3319 1.956 0.63349 18.942 0.1167 2608 2288 1.416 3239 2.186 0.60078 19.146 0.1244 A/AC **4/3** MOLWT SONV MACH VEL 28.919 2560 28.919 1111 25,455 1,2949 1.2947 1.2947 1.2982 1.2302 1.2320 1.2306 1.2995 1.3266 1.3011 GAMMA 1.2982 1.2988 1.3265 1.3900 127) 759) 743) 504) 724) 416) 410) 712) 429) 465) 474) 747) 207.3 121.624 15.069 13,120 12,935 64.539

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		Ø	27.81	27.86	25,14	23.63	23.60	22.21	18,654	15.95	15,58	14.46	13.46	13.29	10.90	11.251	11.224	11.22	11.45	11,111	9.787
		MOMIM	2542	2541	2580	2603	2603	2649	2773	2949	2988	3046	3105	3176	3416	3420	3429	かのかの	3449	3461	3496
		A/AC N	.1340	338	1435	552	554	799	950	.2379	2480	631	.2782	696	3679	3690	3716	3674	. 989	693	.3753
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ě	1 × × ×	₹	5784	55883	52086	48700	48637	45487	8767	31960	30655	28896	.27325	25606	20666	20604	20460	20692	20617	20585	0.20258
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	0(1)	VEL	3208	3209	3106	3122	3123	3142	3096	3211	3271	3228	3170	3340	3394	3514	3530	3491	3576	3473	3109
	-	MACH.	6443	***	.377	308	.341	360	243	.214	•226	171.	.120	.168	.103	.150	.153	.136	.166	.121	. 980
	2	SONV	2552 2223 1	2551 2222 1,	2560 2256 1	2684 2388 1	2636 2328 1	2626 2311 1	2762 2490 1.	2904	2669 1.	2992 2752 1.	2630 1	3089 2860 1.	3250 3078 1	3245	3249 3061 1.	3255 3073 1.	3258 3068 1.	3270 3099 1.	3295 3171 0.
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	•	VOLWT	25.332 25.332	25.330 25.330	25.361 25.361	22.572 22.572	22.481	22.467	22.754 22.754	22.971 22.972	23.050 23.051	23.222	23.402	23.557	24.273	24.246	24.270	24.368	24.324	24.463	24.581
11.0	41.17	GAMMA	3356	3360	3332	3371	3428	1.3235	3089	1.2921	2882	.2987	1.2699	1.2615	1.2403	2445	2142	1.2120	1.2108	2322	.1924 .2124
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4	5	<u>-</u> :	2527 2527 1885	2525 1883	2547 1947	2481 1936	2375 2375 1826	2354	2668 2139	26 3016 2465	27 3095 2526	3268					4244 3688				4502
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COMBUSTOR			31 3				-							,		:	; :
58.755	29,727	4475	562.0(1535)	1,1948	24.562	3290				1,1948 24,562 3290							
58.755	5			1.2095	24.630	3197	0.840	2686	2.569	0.20130	19.472	0.3777	3530	8.402	8.402 181.4 A.70 0.79	A. 70.	2,79
COMBUSTOR	0	ŝ	<b>1</b>	•	1			!			)		)			•	•
60.765	30.602	4467	2(1532)	1,1956	1.1956 24.577	3287					•						
50.765	20.025	4170	3(1415)	1.2107	24.645	3192	0.852	2720	5,565	3192 0.852 2720 2.565 0.20830 19.472 6.3656	19.472	0.3658	4518	A. A. O. O. O. T. A. 70 0 70	180	70.	20
COMBUSTOR	0	0		•				1									
62.185	31,104	4514	1(1548)		24.647	3294			÷								
52.185	19,031	4173	4(1414)	1.2090 24.732	24.732		0.920	2931	2.564	3185 0.920 2931 2.564 6.21395 19.472 6.3553	19.472	0.3554	1506	CO O OF 8 1 081 347 9 305F	180	700	60
COMBUSTOR	0	4	~			}	•								• • • • •		90.
649.49	•	4474	0(15	1.1938	24.633	3283					•						
649.49	15,386	4027	2(13	58) 1,2173 24,730	24.730	3139	1.056	3316	2.566	3139 1.056 3316 2.566 0.20280 19.472 0.3749	19.472	0.3749	34.85	3485 10.452 178.0 A.70 0.81	178.0	100	181
COMBUSTOR	0	42	•	•	• • •	) )							3		100		•
65.025	27,151	6944	2(15	1,1931	24.631	3281											
65.025	14.502	4004	6(13	61) 1.2162 24.729 3141	24.729	3141	1.044	3277	2.571	3141 1.044 3277 2.571 0.18853 19.472 0.4032	19.472	0.4032	34.81	TART 9-602 178 8 6 70 0 81	178	06.0	4
COMBUSTOR	REGEN	4	1	, ,													•
	27.151	4623		1.1827	24.560	\$327			-								
55.028	15,028	4883	413.7(1438)	1.2027 24.683 3198	24.683	3198	1.016	3251	2.591	3198 1.016 3251 2.591 0.18853 19.472 0.4032	19.472	6.4032	45.10	1419 9 404 180 7 A 70 0 BI	. 08.	706	9
NOZZLE A	لوا	<b>4</b>		· ·	1		•	•						7			•
87.261	27,151		2(15	1,1931	24.631	3281											
87.261	0.792		.56	85) 1.2981 24.800 2398	24.800		2.846	6824	2.571	2.846 6824 2.571 0.03925 10.472 1.9371	10.472	1.9371	4503	440 0 04 0 1 6 0 0 4 1 1 1 1 1 0 1 0 1 1	2 686		•
MOZZLE PL		2	38 4	•	) 1 1 1 1 1								9		200		
87.261	27,151	6944	2(15	1.1931	24.631	3281											
87.261	0.419	1905	1 ( 5	81) 1.3108 24.800 2238	24.800		3.217	7198	2.571	3.217 7198 2.571 0.02543 19.479 9.9899	19.472	9.9492	4677	S. Aus Dung B. TO D. B.	0.040	700	
NOZZLE A	E REGEN	9	3	1				•						?	7		
87.261	27,151	4623	.8(1592)	1.1827	24.560	3327				1,1827 24,560 3327							
87.261	0.631	2365	-342.0( 740)	1.2922	24.800	2475	2.810	6956	2,591	20050-0	19.472	1.9372	46.99	IN O OF A W THE CASE A	947 4	06.	9
NOZZLE P	O. REGEN	47		•			1	1							•		•
87.261	27,151	4623			24.560	3327				1.1827 24.560 3327							
87.261	0.419	2020	-462.0( 620)		24.800	2300	3.207	7374	2.591	0.02458	19.472	3.0935	4796	2.817 246 1 A 70 0 A1	P. 946	700	8
FICTIVE C	OMBUSTR	67					•		•								
65.025	121,624	4930			25.168	3390				1,1801 25,168 3390							
	0.419	1571	-831.6( 463)		25.453	2014	4.106	8267	2.457	0.03636	19.472	2.0912	5228	4.671	4.671 268.5 6.70 1.00	1 02.8	00
FICTIVE	DZZLE	99	0 19														
87.261	18.692	4413	\$12.2(1509)	1.1916	24.628	3258											
87.261	0.948	<b>E</b> 470	-304.6( 777)	1.2882	24.800	2526	2.531	6393	2.597	77) 1.2882 24.800 2526 2.531 6393 2.597 0.03925 19.472 1.9371	19.472	1.9371	4338	4538 3.899 222.8 8.70 0.81	222.8	0.70	.81

READING = 0095 BLOCK = 130 TIME = 217,749 MACH 5.2 PT = 300,000 TT = 2944.1

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PAGE 4	P-08/P10 P.000 0.000	1.450E-02	8.917E-03 1.220E-02 1.832E-02	2.605E=02 3.021E=02 3.612E=02	4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00	1.375E-02 1.375E-02 1.49E-02	1.482E-02 1.486E-02 1.657E-02	4 - 6 - 6 - 6 - 6 - 6 - 6 - 6 - 6 - 6 -	5.790E=02 6.426E=02 6.426E=02	6.040E-02 6.040E-02 6.063E-02 6.063E-02 5.500E-02	5.2896 + 0.2	6.55000 6.55000 6.55000 6.55000 6.55000 6.55000 6.55000 6.55000 6.55000 6.55000 6.55000 6.55000 6.55000 6.55000
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	P-18/P10 3,533E-03 3,533E-03 6,167E-03	1.017E-02 1.023E-02 1.024E-02	1.049E+02 1.045E+02 1.176E+02	1.103E-02 1.417E-02 2.230E-02	3.931E-02 4.014E-02 4.586E-02	5.00 00 00 00 00 00 00 00 00 00 00 00 00	7.327E+02 7.446E-02 7.736E-02	6.369E+02	6.35 6.35 6.35 6.35 6.35 6.35 6.35 6.35	6.070E-02 6.068E-02 5.937E-02 6.063E-02	5.289F.02 5.419F.02 5.550F.02 5.060F.02	4.5336 4.5336 5.5336 5.5636 6.5636 6.5636 6.5736 5.3446 5.3446
	P-18/P .527E .527E	319E 323E 323E	505E 473E 411E	.085E .014E .595E	. 251E . 251E . 187E	364E 533E 667E	327E 327E 534E	. 711E	3020	00000000000000000000000000000000000000	.782E .875E .969E .618E	3.099E 01 3.245E 01 4.424E 01 4.690E 01 4.774E 01 3.668E 01
944.1	,,,,,,,	. 60 4 FF O O O O O O O O O O O O O O O O O	000	.743E 0 .048E 0 .851E 0	0000	0000	0000		9668 9668 9668 9668 9668 9669	275E 0 276E 0 343E 0 521E 0	. 451E 0 . 946E 0 . 044E 0 . 167E 0 . 209E 0	3.244E 3.244E 3.245E 3.200E 3.402E 3.5402E 3.5402E 0.3470E 4.200E 0.3470E
.000 TT = 29	0000	000000000000000000000000000000000000000	666	222	9 2 2 2 2	1.634E 1.724E 1.890E	37.50	2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	5.212E	# # # # # # # # # # # # # # # # # # #		-8.274E 02 -8.326E 02 -9.646E 02 -9.095E 02 -9.707E 02 -1.090E 03 -1.299E 03
PT = 300.0	0	8888	-3.013E -3.052E -3.127E	-3.226E -3.432E -3.432E	-3.608E -3.617E -3.774E	-4.951E -4.038E -4.212E	-4.639E -4.673E -4.757E	-6-4-70E	14.555 14.555 14.66 14.66	18.924E 19.207E 19.207E	-1.116E -1.150E -1.224E -1.244E	
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= 130 TIM	000	0.000 4.0000 4.0000 0.0000	2.675E 0 3.660E 0 5.497E 0	7.816E 0 9.062E 0 1.084E 0	1.180E 0 1.182E 0 1.254E 0 1.357E 0	4.125E 0 4.171E 0 4.257E 0	4.456E 0 4.456E 0 4.471E 0	1.342E 1.342E 1.472E 1.473E	1.737E 0 1.739E 0 1.987E 0 1.987E 0	1.00 C C C C C C C C C C C C C C C C C C	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1.418E 01 1.403E 01 1.403E 01 1.403E 01 1.600E 01 1.969E 01 2.902E 01 1.903E 01
0095 BLOCK	P-18 1.060E 0 1.060E 0	3.030E 0 3.072E 0 4.163E	3.148E 0	3.307E 0 4.232E 0 6.690E 0	1.204E 0	1.411E 0 1.482E 0 1.706E 0	20 1986 0 20 1986 0 20 1981 0 10 1981 0	1.911E 0 1.976E 0 2.102E 0	1.906E 0 1.908E 0 1.789E 0 2.789E 0	1.821E 0 1.820E 0 1.781E 0 1.619E 0	1.5887E 0 1.668E 0 1.518E 0 1.445E 0	1.403E 01 1.403E 01 1.403E 01 1.600E 01 1.969E 01 1.903E 01 1.903E 01
READING =	(ABS 981E- 836E 070E	508E 516E 517E	583E 606E 648E	701E 729E 803E 831E	8756 8786 9016 9296	978E 000E 040E	124E 134E 150E	#06E #31E #78E	625E 730E 731E 811E	874E 928E 069E	6224 6224 6224 6226 6236 6336 6336 6336	5.642E 01 5.650E 01 5.471E 01 5.773E 01 5.875E 01 6.218E 01

TT = 2944.1

## RAMJET PERFORMANCE

INET	OF ATTACK  LOW RATIO	PROCESS EFFICIENCY - SUPERSONIC PROCESS EFFICIENCY - SUPERSONIC IC ENERGY EFFICIENCY - SUPERSONIC PY AI PO - SUPERSONIC PY AI PO - SUBSONIC	COMBUSTOR	FUEL—AIR RATIO	FUEL INJECTORS	INJECTORS STATION VALVE  1A 40.400  1B 41.270	24 46.250 E 5.250 3.8 56.220 E 56.220 E 44.770
C ENGINE PERFORMANCE	CALCULATED THRUST	STREAM THRUST	MOMENTUM AND FORCES	INLET FRICTION DRAG	STATIONS	NI CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTO	73.809 56.425 65.025 65.025

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PLOCK B 142 TIVE B 220,049 MACH 5,2 PI B 500,250 TI B 2944,3 RAMJET PERFORMANCE

ETAC 2766 26,056 144,6 0.52 0.24 2691 39,937 141.0 0.22 0.00 2633 36.089 137.9 0.22 0.15 27,02 26.719 141.5 0.22 0.48 2732 26.166 143.1 0.22 0.57 2733 26.132 143.1 0.22 0.58 2794 43.161 146.7 0.14 0.07 2700 40.199 141.4 0.22 0.03 2674 38.871 140.0 0.22 0.00 2714 26,550 142,2 0.22 0.92 2699 40.153 141.4 0.22 0.01 n L IVAC 7.612 162.9 2795 41.889 147.4 1.179 192.7 1.349 182.9 7.172 183.2 2033 36,455 149,5 2833 12,607 149,5 O 3468 3468 5265 5453 アニア 28,919 1125 5,092 5728 1,865 0,08552 16,958 0,8655 28.919 2520 28.919 2532 0.401.1015 2.093 0.08552 18.958 0.8655 20.919 2517 28.919 1963 2.079 4081 1.936 0.62060 18.958 0.1120 28.919 2517 28.919 1950 2.114 4121 1.936 0.60051 18.958 0.1233 24.307 2808 24.308, 2610 1.062 2773 2.506 0.60472 19.271 0.1244 28.919 2560 28.919 1111 5.170 5742 1.885 0.08037 17.816 0.8655 2466 0.548 1351 1.968 0.60051 18,958 0.1233 20.492 2582 26.492 2097 1.646 5877 2.093 0.6672} 19.091 0.1117 26.455 2569 26.455 2079 1.863 3873 2.087 0.66710 19.091 0.1117 2567 2082 1.849 3650 2.087 0.66747 19.091 0.1117 26.449 2565 26.449 2111 1.772 3742 2.087 0.66845 19.091 0.1115 27.042 2735 27.043 2552 1.053 2686 2.137 0.64002 19.091 0.1165 27.166 2761 27.168 2569 1.022 2645 2.141 0.63566 19.091 0.1173 944 Z.095 U.U8U37 17.816 0.8655 2621 2281 1.599 3509 2.112 0.66188 19.091 0.1126 27.086 2745 27.090 2566 1.043 2676 2.139 0.63847 19.091 0.1167 27.163 2760 27.165 2566 1.023 2647 2.141 0.63600 19.091 0.1172 27.388 2573 27.388 1994 2.098 4187 2.038 0.66338 19.041 0.1121 A / A C ۲ ۲ æ C: **√**6 > a 4 1 1 26,919 2560 26,919 2516 0,372 H A C 3 MULMT SONV 26.919 26.450 26.630 26.919. 1.3966 1.2947 1.4933 1.3949 1,2962 1.2982 1.3007 1.3410 1.3066 1,2831 1,3040 1.3067 1,2613 1.2962 1.2995 1.2947 1.4966 936) 1.2786 800) 1.2932 937) 1.2785 801) 1.2931 SAMAS 7493 766) 468) 763) 127) 4117 177) 4765 469 770) 759) 418) 748) 3.5 3.5 9097 125 748) 653.2( 635.4( 597.46 457.3 459.3 460. 14.350 2944 300.250 2944 14.350 2944 2.946 2876 3.604 167 4.843 1649 PINE TAP NO 300.250 121.135 121,135 87,916 19.125 86,326 64.539 101,275 07,376 72,335 37,144 72.624 88.632 13,995 74.508 19.097 37.669 30.676 11.017 15,873 72.461 14,217 72,602 13,961 コンススコン ロマーマ BUSTOR BUSTOR USTOR

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	IVAC	9.0	46.7	97	•	0 8	53.5	53.3	•	-	•	:	79.7	77.6	1.00	•	0.00	91.1		•	91.6	91.6	98.5	193.0
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	A/AC	0.1245	0.1340	25 K 1 0	:	0.1435	0.1552	0.1354	0-1062				000000	0.2631	0.2782	•	* <b>9 6 7</b> 0	0.3679	0.460		0.3716	0.3674	0.3688	0.3695
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250 1	ø	2.306	2,322	2,321		2,336	2.500	2.501	2.513				2,581	2.592	2.601	•	•••	2.649	2.634		2.635	2.659	2,659	2.658
300	VEL	2774	2903	2903	:	2926	3194	3107	751	; ;			7007	0777	4140	. ;	7/70	4504	0957	•	4570	4269	4315	4332
<u> </u>	MACH	1.062	1.089	0.60		1.074	1,185	1,165	1.234	•	•	•	1.036	1.453	1.432	. ;	7 ·	1,331	1.511	•	1,513	1.313	1,331	1.337
5.8	80×	2809	2870	2668	2923	2726	2950	2931	2991	3078	9120	31.00	2847	3220 2889	3250	3278	1181	3158	3335	3338	3021	3438	3438	3438
9 HACH	MOL*1	24.309	24.528 24.530	24.523	24,723	24.726	22.144	22.146	22,282	88.808	22.662	22.762	12.776	22.916	23.025	23,161	109063	23.917	23.466	33.484	23.578	24.192	24.194	24,196
228.54	GAMAD	3078	3000	2002	2755	.2010	.2936	.2035	2882	2752	2892	2556	. 2669	2804	2397	2310	7007.	4207	2535	2069	.2525	.1502	1503	.1504
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	BUOILE				FUEL INJECTORS			
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t = 289.75 sec.

The AIM nozzle pressures appear to be excessively high.

READING = 0095 BLOCK = 210 TIME = 289.749 MACH 5.2 PT = 308.250 TT = 2893.1

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	I		GAMMA	VOLWT	SONV	KACH	VEL	s	4 / ¥	2	A/AC	40414	ø	IVAC	PHI	ETAC
	637.8	764)	1.2965	26.919	2539	5.171	5685	1.877	0.08388	18.595	0.8655	3374	7.411	181.4		
<b>79</b> 10	637.8(	764)	1,2964	28.919	2539	0.371	932	2.086	0.08388	18.595	0.8655	3561		191.5		
2	4.	764) 124)	1.2965	26.919	2539	5.087	5670	1.877	0.08964	19.873	0.8655	3599	7.899	181.1		
	37.	764)	1.2964	28.919	2539 2511	0.401	1008	2.086	0.08964	19.673	0.8655	3599	1.404	181.1		
2795 1531	608.3( 250.6(	738) 380)	1.2996	28.919	2499	2.247	4231	1.918	0.64794	19.873	0.1120	2973 4	45,525	149.6		
<b>10 N</b>	0.00 45	738)	1.2996	28.919	2499	2.276	4260	1.918	n.62949	19.873	0.1233	3008	41.678	151.4		
2683	578.2	735)	1,2996	28.919	2643	0.525	1267	1.957	0.62949	19.673	0.1233	3006	12,593	151.4		
795 574	608.3( 262.0(	735)	1.2996	28.919	1907	2.183	4162	1.918	0.69236	19.873	0.1121	2972	44.785	149.6		
26 26 26 26	276.	731)	1.3000	28.919	2493	2.093	4052	1.922	0.69440	19.873	0.1117	2929	43.726	147.4		
2779 1630	603.7( 277.3(	731)	1,3001	28.919	2492	2.084	4045	1.922	0.69479	19.873	0.1117	2925 4	3.638	147.2		
2777	90.	730)	1.3402	26.919	1947	2.062	*10#	1.923	0.69580	19.873	0.1115	2914	#0#°E#	146.6		
	597.4( 287.7(	724)	1.3395	28.919	1960	2.008	3937	1.926	0.68896	19.873	0.1126	2882 4	2.148	145.0		
<b></b>	87.	715)	1.3018	28.919	2469	1.984	3683	1.927	0.66621	19.673	0.1165	2853	40.205	143.6		
279	96. 87.	713)	1.3020	26.919	2467 1959	1.974	3867	1.927	0.66460	10.873	0.1167	2846	39.940	143.2		
2710 2710 1666	583.1( 287.0(	710)	1,3023	26.919	2463	1.965	3849	1.927	n.66202	19.873	0.1172	2837	39.603	142.A		
. 6.9.	86.	710) 416)	1,3023	28.919 28.919	2463	1.965	3849	1.927	n.66167	19.873	0.1173	2837	39,581	142.A		
2 £ .	593.6(	862)	1.3007	24.783	2466	1.199	2956 2	2.241	N.63229	20.150	0.1244	2828 2	29.044	140.4 8	0 77.	.17
16	5	863)	1,3005	24.786 24.786	2710	1.196	2952	2,241	0.63197	20.150	0.1245	2829 2	28.992	140.4 0	0 44	0.17

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0.31	0.30	0.41	0.16	0.16	0.18	0.32	8 <b>†</b> • 0	74.0	0.50	0.53	0.56	0.76	0.65	0.66	0.75	0.75	0.70	0.53
44.0	44.0	4	0.85	6.63	8.85	8.85	9.86	9.86	9.86	9.86	99.0	9.86			98.	9.86	9.86	.86
6.4.	44.7	48.9	49.6	49.6	2.9	ç	E - 2	73.6	76.8	79.6	82.8		91.3	91.6	91.9	95.6	93.1	94.1
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2806 2645	2805 2643	2869 2711	2902	2902 2660	2920 2628	3087 2862	3208 2952	3238	3263	3278 2995	3296 2998	3398	3349	3351 3040		3391 3150	3373 3090	3275
25.073	25.068	25.286 25.288	21.908	21.910	91,958	22.391	22.681	22.797	22.934	2.982	23.079	23.650 23.808	33.362	53.373	53.640	23.629	23.513 23.639	23.006
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2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242   2.242	36.534 2713 497.45 623) 1.3002 55.074 2645 0.055 2547 2.287 0.58018 20.135 0.1348   2918 23.240 1444 6 0.44 0.0	38-334 2713   457-47 (873)   1.2073   25.074   2665   0.65   2547   2.247   0.56013   20.150   0.1340   2918   23.240   144.6   0.44   0.44   0.44   0.44   0.44   0.44   0.44   0.44   0.44   0.44   0.44   0.44   0.45   0.45   0.45   0.45   0.45   0.45   0.45   0.45   0.45   0.45   0.45   0.45   0.45   0.45   0.45   0.45   0.45   0.45   0.45   0.45   0.45   0.45   0.45   0.45   0.45   0.45   0.45   0.45   0.45   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NE = 289.749 MACH 5.2	KOLET SONV	•	23,306		23.868	24.090		24.020	24.273	1	24.051	24.299					23.988	24.348		24.104	24.703		24.104	24.706		1.1487 23.988 3467	24.701		23.988	24.705		1,1649 24,339	24.817		24.309	24.706
: 289.74	GAMPA		1.2143		1.1708	1.2005		1.1598	69) 1,1785 24,273	 	74) 1,1578 24,051	1.1739	•	1,1526	30) 1,1639 24,354		1.1487	16) 1.1624 24.348		1.1526	36) 1,2637 24,703		1.1526	1.2810		1.1487	1.2572					1,1649	1.3097		1.1693	1.3085
TIME			533)	:	(1724)	(1468)		(1772)	(1569)			(1586)		(1790)	(1630)		(1830)	(1616)		.0(1746)	•		7	~		(1820)			.3(1830)	•		.0(1873)	( 523)	_	9(1831)	10360
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9 2600	a.		40,537	•	36.070	14.025		35,973	16.294		33.694		0	31,085	16,102	REGEN	-,	12,676		31,085	0.995	_	31.085	0.437	REGEN	31,089	1.038	PO REGEN	31.085	0.437	COMBUSTR	147.481	0.437	ZZLE	131,505	0.000
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Ŋ	0	.220E 0	-5.039	9		-446E	-1.156E	1.070E	.838E	4.019F-02	7956	Ç
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٦,	0	.418E 0	-5.627	5.6	1.1	.037E	2 -1.814E	1.257E	4.045E 01	5.728E-02	.248E 0	Ġ
٦.	0	.418E 0	-9.629	۳.		.042E	2 -1.818E	1.259E	4.058E 01	5.746E-02	248E	Ğ
Ŋ	0	.414E 0	-5.951	۳.		465	2 -2.223E	1.362E	-200E	7.364F-02	240E 0	589F-0
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۳,	0	.286E 0	-6.341	•	<b>%</b>	.073E	2 -3.905E	1.697E	261E (	6.035E-02	3446	0
r.	0	1499E 0	-6,381	1.0	S	6.213	2 -4.070E	1.727E	405E	6.237E-02	. 433E	0
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	P-08/PT0	5.224F-02	5.223F-02	5.210F=02	2 145,00	0.0615100	1.5665	1.1035-02	0 100 P	6.732F=03	0.1165-03	1.760F=09	1.7545-02	1.723F-02	1.722F=02	0000	0.000	0000	000	00000	00000
	P-08/PS0	3.689E 01	1.688F 01	3.685F 01	1.506F 01	10000	1.106F 01	7.789F nn	6.602F 00	4.754F 00	6.437F 00	1.243F 01	1.23AF 01	1.216F 01	1.216F 01	0.800	0.00	0.00	0.000	0.00	0.00
	P-18/PT0	5.2236-02	5.2235-02	4.903F-02	2.251F-02	1.664F=02	9.895E-03	8.0945-03	6.569F-03	6.313E-03	6.196F-03	1.222F-02	1.2815-02	1.2635-02	1.263E-02	1.231E-02	1.450E-02	2.198E-02	2.378E-02	2.402E-02	2.402E-02
	P-18/PS0	3.688E 01	3.688E 01	3.463E 01	1.589F 01	1.175F 01	6.987E 00	5.716E 00	4.639E 00	4.458E 00	4.376E 00	8.632E 00	_	8.921E 00	_	8.694E 00	1.024E 01	1.552E 01	1.679E 01	1.696E 01	1.696E 01
	CAWALL	4.337E 03	4.342E 03	4.368E 03	4.583E 03	4.665F 03	4.760E 03	4.848E 03	4.922E 03	5.036E 03	5.088E 03	5.273E 03	5.290E 03	5.374E 03	5.375E 03	5.427E 03	5.525E 03	5.630E 03	5.684E 03	5.707E 03	5.707E 03
	HO-0	3 -1.501E 03	3 -1,503E 03	3 -1.513E 03	3 -1.580E 03	3 -1.601E 03	3 -1.624E 03	3 -1.645E 03	3 -1.663E 03	3 -1.686E 03	3 -1.695E 03	13 -1.727E 03	3 -1.730E 03	3 -1.750E 03	3 -1.750E 03	3 -1.791E 03	3 -1.865E 03	3 -1.865E 03	3 -1.865E 03	3 -1.865E 03	3 -1.865E 03
	0-1B	03 -1.407E 0	03 -1,409E 0	03 -1.417E 0	03 -1.468E 0	03 -1.482E 0	03 -1,494E 0	03 -1,504E 0	03 -1.511E n	03 -1.522E 0	03 -1.527E 0	•	03 -1.544E 0	03	3	03	3	03	S	03	03 -1,723E 0
	X09	02 -2.908E	02 -2,912E	02 -2,929E	02 -3.048E	02 -3.082E	03 -3,118E	03 -3.149E	03 -3,174E	03 -3.208E			03 -3.274E	03	03 -3,302E	03 -3,356E	03 -3,457E	03 -3,493E	03 -3.528E	03 -3,538E	03 -3.588E
	POA	7.097E	7.097E	7.097E	8.34SE	9.609£	1.093E	1.180E	~	1.309E	_	_		_		1.777E	1.943E	2.103E	2.340E	2.517E	2.517E
	P-08	1.610E 01	1.610E 01	1.609E 01	6.575E 00	_	4.827E 00	_	_	_	_	5.425E 00	8.406E	5.310E	5.309E		0	0000	00000	00000	0.000
	P-18	1.610E 01	1.610E 01	1.511E 01	6.937E ·00	5.129E 00	3.050E 00	2.495E 00	2.025E 00	1.946E 00	1.910E 00	3.768E 00		3.894E 00	3.894E 00		4.470E 00	6.775E 00	7.330E 00	7.405E 00	7.40SE 00
-	XABS	6.502E 01	6,506E 01	6.526E 01	6.692E 01	6.759E 01	6.836E 01	6.908E 01	6.969E 01	7.064E 01	7.107E 01	7.260E 01	7.27SE 01	7.350E 01	7.351E 01	7.483E 01	7.76BE 01	8.158E OI	8.439E 01	8.725E 01	8.726E 01
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FT = 308.250 TT = 2093.1 READING = 0095 BLOCK = 210 TIME = 289,749 MACH 5,2

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RAMJET PERFORMANCE	TR INI	ANGLE OF ATTACK	INCEL PROCESS EFFICIENCY - SUPERSONIC 0.9113 INCET PROCESS EFFICIENCY - SUBSONIC 0.9164 KINETIC ENERGY EFFICIENCY - SUPERSONIC 0.9189 KINETIC ENERGY EFFICIENCY - SUBSONIC 17.86 (RTU/LBM) ENTHALPY AT PO - SUPERSONIC 17.86 (RTU/LBM)	COMBUSTOR	FUEL-AIR RATIO	IENCY	INJECTORS STATION VALVE 1A 40.400 1B 41.270	
RARUET PI	ENGINE PERFORMANCE	CALCULATED THRUST	STREAM THRUST	MOMENTUM AND FORCES	FRICTION DRAGE		NOMINAL COML LEADING EDGE	73.509 87.261 56.425 65.025

t = 310.45 sec.

TVAC PHT ETAC 5825 28.622 115.8 0.34 0.07 4966 10,908 156.6 5087 1.933 160.5 5114 11.226 196.5 5113 2.065 156.5 4198 62.774 128.5 4855 58,151 130,2 4255 19.073 130.2 4196 62.168 120.4 4019 57.483 123.6 3879 49,991 118,7 3849 48,826 117.8 4073 58.470 124.7 4063 58.160 124.X 3958 54.256 121.1 3694.50.579.119.2 3849 48,772 117.8 1-29-75 Peg. conetal KOW TE 28.919 2246 28.919 948 5.170 4908 1.780 0.14300 31.702 0.8655 717 971) 1.3143 20.919 2246 886) 1.3201 20.919 2220 0.392 870 1.985 0.14300 31.702 0.8655 971) 1.3182 28.919 2246 91) 1.3985 28.919 955 5.132 4983 1.780 0.14738 32.671 n.R655 971) 1,3163 28,919 2246 998) 1,3202 28,919 2218 6,406 902 1,985 0,14738 32,671 0,4655 556) 1.3261 28.919 2220 305) 1.3635 28.919 1709 2.077 3548 1.629 1.10462 32.671 0.1120 20,919 2220 20,919 1684 2,147 3616 1,829 1,03491 32,671 0,1233 26.919 2220 26.919 2171 0.546 1186 1.860 1.03491 32.671 0.1233 28.919 2202 28.919 1860 1.598 2971 1.852 1.09528 32.671 0.1165 25.454 2337 25.454 2230 0.797 1777 2.072 1.03622 33.722 0.1244 28.919 2220 28.919 1720 2.045 3514 1.829 1.13877 32.671 0.1121 28.919 2217 26.919 1787 1.844 3296 1.840 1.14162 32.671 0.1117 28.919 2216 28.919 1792 1.828 3277 1.841 1.16227 32.671 0.1117 28.919 2216 28.919 1805 1.792 3235 1.843 1.14394 32.671 0.1115 28.919 ZZII 28.919 1642 1.673 3052 1.808 1.13209 32.671 0.1126 28,919 2201 28,919 1866 1,577 2942 1,853 1,09264 32,671 0,1167 1,3217 28,919 2197 1,3473 28,919 1875 1,539 2887 1,854 1,08840 32,671 0,1172 28.919 2197 26.919 1875 1.538 2885 1.854 1.08783 32.671 0.1173 1.3319 25.346 2203 1.3392 25.346 2171 0.817 1774 2.055 1.03571 33.022 0.1245 ¥ / 3 PACH VEL MULKT BONV 571) 1.31#2 ; 1.3203 1.3215 1.3201 1.3201 1,3203 1.3204 1.3217 1.3261 1.3214 A 7 7 A 7 556) 1,3201 295) 1,3659 551) 1,3207 361) 1,3505 413.6( 542) 247.3( 376) 10 21 422.1( 669) 359.0( 546) 556) 100 554) **53**4) **33**9) 553) 345) 545) 372) 526) 926) 246) 369) 543) 376) 427.2( 427.21 485.20 427.26 425.1( 422.01 610.00 413.76 415.6 442.50 208.20 178.66 .37.90 142.5( 426.2( 00.00 80.4( 210.40 215.7( 232.10 242.96 399.16 427.2( 424.7 16.473 1208 21.047 2235 1.000 416.249 2225 10 0.610 380 DO. 184,612 2172 30.598 1518 93,936 2109 18.936 2168 20.714 1245 00 117.175 2172 00 96.630 2072 .410 184.617 2172 21.664 1264 0 155,423 2165 153.509 2164 11.500 149.144 2163 2.460 134.512 2153 1.065 122,670 2135 25.680 1.310 120.555 26.450 29.604 65.29 25.366 20.696 29.390 CT PROFIE X S Y Z Z C IND TUNNEL 312

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359.21 512)

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e	63	20.67	21.86g	22.602	22.677	23.481	26.641	28.311	87.736	27.436	27.356	26.474	21.138	21.072	22.991	165112	21.891	22,819	25.356
707	7985	3979	4156	4309	4312	24075	<b>6</b> 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	<b>\$22</b> 0	\$20	5363	5467	5559	3786	5791	2003	0.00	9031	5845	5874
A/AC	1.1340	A.1 238	0.1435	0.1552	0.1554	0.1662	0.1950	0.8379	0.2450	1898.0	G.2782	0496.0	0.1679	0.40.0	0.1716	0.1674	0.3688	0.1693	f.1793
7	33,622	33,022	33,022	33.352	33,352	55.352	33.332	33,470	31.470	33.470	31.470	31.470	31.670	38.470	55.470	31.470	33.470	33.479	33.470
¥/1	0.96216	0.963AB	0.39838	0.83902	0.83793	0.78367	0.66790	98698.0	0.52690	0.49667	0.4694	0.44013	0.35521	0.35415	0.35166	0.35566	0.35436	0.35342	0.34821
0	9	2,048	2.076	2,253	2.253	2.286	2,351	2,393	2.400	3.406	2.409	2.415	2.453	2.433	2.434	2.451	2.450	2.441	2.392
بر د د ح	1393	1393	1546	1738	1701	1928	2567	3316	3387	3554	3734	3671	3829	4192	4207	3008	3975	4150	9897
į	0.635	n.635	0.659	0.734	0.734	0.760	0.968	1.228	1.245	1.306	1.381	1.430	1.324	1.542	1.547	1.358	1.390	1,490	1,929
> 2	264	2263	2355	2467	2469	2501	2616	2022	2078	2000	2704	3031	3181	2718	3062	3148	3146	3118	2071
	25.330 25.330	25,328 25,328	25,528	22.954	22,957	23.172	23,722	24.044	24.133	24.217	24.261	24.344	20.856	24,557	24.550	24.848	24.839	24.708	24.159
41145	<b>FT PM</b>	1,3332	1.3238	1.3285	1.3285	1.3170	1.2003	1.2718	1.2676	1.2617	1.2617	1.2860	1.2596	1.2074	1.2814	1.2615	1.2532	1.2383	1.2660
	563) 925)	562)	621)	615)	677)	797)	954)	1091)	1120)	1146)	1154)	1183)	1340)	1206)	1244)	1345)	1341)	1299)	1114)
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ETA	0.80	0.87	0.91	0.90	0.90	0.90	0.90	0.90	0.90	0.90	1.00	0
PH	8.51	9.51	8.51	6.51	0.51	0.51	6.51	6.51	6.51	9.51	15.0	ī
IVAC	164.5	163.7	163.0	161.7	161.5	162.5	208.0	214.7	211.5	218.8	232.9	9
Œ	11.512	13.190	14.654	16.449	15,139	12.025	6.427	4.387	6.524	4.364	7.469	8 0
MONTH	5499	5474	5450	5406	5399	5433	6955	7180	7071	7316	1787	4652
	7775.0	3656	,3553	3749	.4032	.4032	.9371	9 <b>6</b> 64	1.9371	925001	.9550	.9371
	33.439	53.439	33.439 C	33.439	33.439 (	33.439	1. 624.88	53.439 2	53.439 2	33.439 3	53.439 1	1.054.63
M/A	.34568	. 35771	.36740	.34825	.32376	.32376	.06740	1.04372	0,06740	.04270	.06678	1225) 1.2341 26.026 3019 597) 1.3067 26.062 2260 2.530 5717 2.341 A.06740 33.434 1.4371 4652 R ARB .00 C A E: C CC
so.	2.351 n	2.354 0	2.354 n	2.357 0	2.363 0	2.375 0	2.363 0	2,363 0	2.375 0	2.375 0	2.253 0	2.391.0
VEL	2143	2373	2602	3039	3009	2390	<b>613</b> 6	<b>645</b> 8	6259	6877	7197	5717
MACH	.736	.810	888	.059	.046	.802	. 895	.279	.872	.275	.242	530
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LWT S	769 2 778 2	986	042 3	038 3	027 3	013 3	062 2	027	013 3	013 3	290 3 329 1	026 3
A 5	3 25. 1 25.	8 25. 0 25.	1 26. 9 26.	3 26. 6 26.	3 26. 4 26.	7 26. 6 26.	3 26. 1 26.	3 26. 7 26.	7 26. 1 26.	7 26. 0 26.	5 26. 3 26.	1 26. 7 26.
GAMM	1.246	1.237	1.233	1.234	1.254	1.240	1.234	1.234	1.514	1.528	1.229	1.834
	1182) 1097)	1228) 1125)	1252) 1130)	1243)	1240)				1284) 541)	1264) 452)	1316) 310)	1225) 597)
I	393.36	387.7( 275.1(	388.7( 248.4( 34 84		375.0( 194.1(	426.2( 312.1(	378.0( -377.5(	375.0( 456.5(	426.2( -349.2( 40		375.01 -660.1( 61 0	359.7( -293.8(
<b>⊢</b> ₩	3736	3871	3 D =	23.2		#030 3750	3908 1787 45	3908 1527 46	4030 1876 47	4030 1592 67	4129 1125 68	2049
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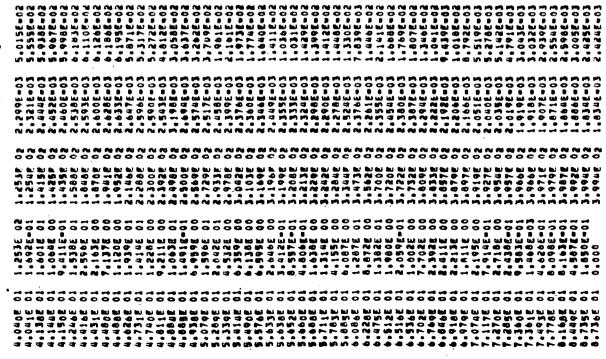
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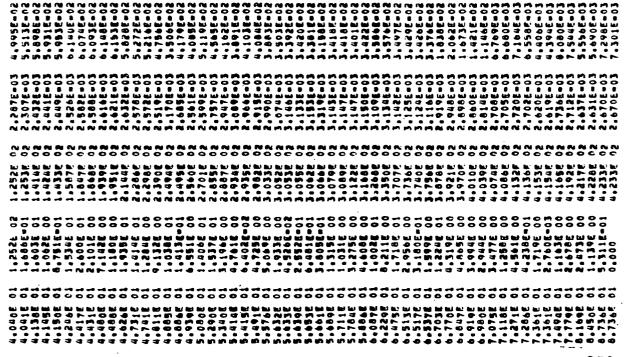
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<b>1</b>		70	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	•	ר ט	-	D		7	Ľ			901	•		
416.499 22	76.75	576)	1.3181	28,859	2256	3		9		2	•	ŭ	70			
7 .00.0		_	. 3 400	٥		<b>D</b>	^ ! ·	70/1	9	36.36	011940 2	60 60	7.1.1	-) 6.1		
22,437 22	447.30	576)	.3161	26.859	2256		;					•	1			
40.136 616 HRDAT 5	9 7	60				0.407	906	796.	0.15642	36.56	9118	5015	<b>5.20</b>	157.0		
172.231 217	29.10	598)	1,3203	26,859	2225											٠
·20,388 126	181.20	103	.3628	. 658		2.043	3522	1.835	1.05953	32,522	2 0.1097	4133	63,362	127.1		
172,231 217	489.1	(6)	3203	85	2225											
20.143 126	80.10	309)	1,3630	20.058	1721	2.051	3530	1,835	1.05237	52,52	2 0,1207	4190	57,724	126.6		
*	4			0												
95.697 207	000		2026.1	24.850	2134	1	1220	1.841	1.04217	13.62	~	9	-			
9	, in							-		36136		•				
173.065 21	429.1	558)	1,3203	26.859	2225	,										
45.848 131 0	194.7	24	13505	6.65	737	1.949	3425	1.035	1.15746	32.52	2 0,1097	4132	61.602	127.0		
143,326 21	C 920	(8)	.3206	28.859	2220											
28.263 144	227.00	•	1.3522	20.05	1632 1	.724	3150	1.846	1.15692	32,52	2 0,1098	3987	\$6.789	122.6		
08 0 10	<b>S</b>	į		, (							,					
571 759 82	70.07	3500	10261	70000	6660											
			•	2		108	3138	1.847	1.15799	32.52	2 0.1096	3976	50.460	122.3		
0 11	3															
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61 ACT 0	, de 1. e	<u>.</u>	7166.			, 0	2150	1.00	1.15765	36.96	2 0,1097	3468	56.138	122.0		
125,025 215	422,8(	592)	.3211	620	2214											
32.240 153	388.00	81)		20.050	1991	1.549	2923 1	1.854	1.14675	32.52	2 0,1107	1869	.52,091	110.0		
21 0 212.540 211	4 416.85	(40	A 1 C 1		4066											
33.710 157	263.70	6	7.7645	20.858	1912	1.447	2768	1.859	1.10365	32.522	2 0.1150	3791	47.471	116.6		
71 0	. S						,	•		•		•	•	):  -		
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35,199 160	5 270.8(	600		20.858	1951	1.343	2684	1.860	1.09925	32,52	2 0,1155	3754	45,646	115.4		
01 0 0 0 ° 8		441	155	3	4000											
35,370 160	8 271.7(	401)	1.3430	20.03	1929	1.386	2673	1.860	1.09783	32.52	2 0.1157	1750	45.604	9 6 1 1		
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2 2	240.46	(075	1,3226	28,859	2012	1	,	4	,			;	•	;		
91 0	11 S			D	, u	108.1	/ (0)	7007	1.05050	36.36	< 0,1625	27.24	44.741		-	
99,705 210	0 407.50	537)	1,3230	28,859	2188											
8.201 153	380.85	80)	.3471	26.058		1.466	2801 1	. 965	0.96382	32,522	2 0.1317	3782	41.950	116.3		

TIME # 165,940 NACH 5.2 PT # 418,499 TT # 2240.5

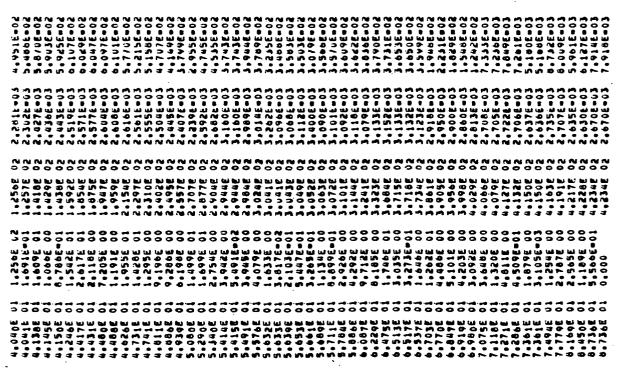
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61	ъл. Э. Т.	;	4 - E	HO.	z	HACH	VEL	ø	<b>4</b>		A/AC	3	G	IVAC	g I	ETAC
3 7 1	~ 6	536) 378)	1,3230	20.059	1680	3 · 7 · 1	2816 1	.664	16956.0	52.52	0,1327	3789	41,903	116.5		
3.0	5.4(	534)	1,3232	28.459	2184	1.601	2950 1	0 1 9 9 • 1	.69754	32.522	0.1415	3842	41.142	110.1		
32		533)	1,3235	28.859	2161	1,715	3088 1	862	.81707	32,522	0 -1554	3904	39.206	120.0		
J =		531)	1,3236	26.459	2179	1.789	3171 1	.862	0.76415	32,522	0,1662	2943	37.059	121.3		
9 7 7	•••	526)	1.3240	28,659	2173	;			į	•						
244	200	547) 456)	1,3211	26,778	2205	1.050	2141 1	9 9 9 9 9	. 53563	32.52	0.1950	1 to 0 to 0 to 0 to 0 to 0 to 0 to 0 to	35.010 17.616	125.6	20.0	. 0
2779	<b>400</b>	546)	1.3213	26.778	2203	0.902	1873 1	0 669	.51374	32.634	0.2480	4840	•	:	<b>~</b>	•
) W F	7.	800) 738)	1.3016	25.271	2611	0.700	1762 2	.215 0	.49082	33.051	0.2629	9697	13,593	140.5	0 244 0	36
3 19 4	===	801) 738)	1.3015	25.473	2612	0.10	1762 2	.215 0	57067	33.051	0.2631	4638	13.582	140.3	0 99 0	34
	10.8 55.6 5	848)	1.3047	25,429	2564	9.0	1772 2	.228 0	.46579	53.051	0.2782	4795		45.1	3	
とりだべ	3 N	901)	1,2868	25.614	2727	1.00.0	1767 2	. 242 0	.43752	33,051	0.2949	0.67	12.012	150.4	0 24.0	16.
	<b>36.5</b> 0	1098)	1.2852	22.649	2950	0,591	1704 2	0 767.	,35538	33.467	0.3677	5708	9.412	170.6	0.87 0	.35
2 - W K	76.55 76.55 76.55	1029)	1,2850	22,652	2951	0.591	1705 2	0 767.	.35518	33.467	0.3679	5711	9.410	170.0	0.87 0	. 25
3 - 14	36.2( 70.8(	1110)	1,2784	22.782	3000	9.618	1809 2	.505	. 35419	33,467	0.3689	5722	956.6	171.0 (	0.87 0	98.
9 4 4 6	52.50	1116)	1.2773	22.806	3007	\$ t 9 . 0	1608 2	.507 0	.35164	33.407	0.3716	5749	9.880	171.8	0.67 0	0
3 77 7	55.1.C	1013	1,2849	22,762	2991	0.601	1759 2	. 502 0	,35551	33.467	0.3675	5764	9.716	178.2 (	0.07 0	34
, , ,,,	23.00	1132)	1,2754	22,845	3020	0.607	1792 2	. 508 0	.35453	33.467	0.3686	2810	9.676	173.6	0.67	14
	2.3 2.3 2.3 2.3	11611	1.2714	22.928	3046	. e i S	1831 2	.513 0	15367	33,467	0,3695	S # 55	10.066	174.0	0 48.0	3 3 .
,	29.2( 56.4(	1230)	1,2617	23.116	3104	0,60	1910 2	. 524 0	.34819	33.407	0.3753	5937	10.334	177.4	0.67 0	3

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	IVAC PHI	•		0.67	•		0.87	•		0.87			0.87	•		0.87			0.87			0.87	•		0.87			0.67			0.87	•		0.87
	IVAC			179.4	•		177.9	•		176.7	•		194.3			177.2	•		228.8			235.3			230.2			236.9			270.7			214.5
	3			0.830			3.495			5.432			8.676	•		5.897			7.116			4.986 235.3 0.87 0.72	•		7.156			4.976	•		7.119	•		777.9
	NO NO N			5003 10.816 179.4 0.87 0.56			5955 13,495 177.9 0.87 0.67	•		5913 15.432 176.7 0.87 0.72			6504 18.676 194.3 0.87 1.00			5930 15,897 177,2 0,87 0,72	•		7657 7,116 228,8 0,87 0,72	• .		7874			7703 7,156 230,2 0,87 0,72			1927 4.976 236.9 0.87 0.72	1		9056 7,119 270,7 0,87 1,00	•		7179 6,444 214,5 0,87 0,72
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U • 3	E		2509 23,320 3158	53.467		2293 23,702 3244	33.467	,	2217 23,834 3267	33.467	•	1682 24,983 3388	33.467	•	2190 23.426 3282	33.467	•	1217 23.634 3267	33.467	•	2217 23.634 3267	33.467	ı		2,996 6826 2,558 0,06745 33,467 1,9371		140 23,626 3282	33.467		1797 24,676 3427	33.467	,		.2994 25.496 2456 2.503 6147 2.595 0.06745 55.467 1.9371
65,940 KACH 5.2 Pl # 418.499 TI # 2240.3	<b>4/</b> x			0.34597			0.35601			0.36771	•		0.36771	•		0.36771	•		0.06745			0.04523			0.06745			0.04483	,		0.05507			5029000
1 661	ø			2.535			. 550			2,553			2.556			955.3			1.553			2.553			955.7			558			1.447			2.593
418.	VEL			2012			2425			2701	•		3266			2782			6789			7094			6026			7142	•		6316			6147
<b>n</b>	MACH VEL 8			169			.770			.856			000	;		.879			900			.356			966	•		354			190			505
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F.ACH	NAMA MOLMI SUNV	ı	3,320	3.527		3.702	3.723		3.834	3.865		14.983	97.77		3.626	3.862		3.834	3.896		3,634	3.896		1190 23.626 3282	3.896		3.826	3.896		4.676	296.4		3.635	969.5
165,946	A M M D		1.2509 2	1.2566		1,2293 2	1.2410								-			1.2217	_			1.3268			1.3131 2		1.2190 2	-			1,3155 2		1.2216	1.2994
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e xoole	-	38	3740	5548	39	780#	3618	0 7	4189	3868	7	6597	9677	62	4234		•	69	1867 .	-,	4189	1619	68	7530	• 0061	97	4234	1044	9 99	<b>₹</b> 761	- 6291	9 69	2	2230
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-	200.	007	205	,		300		562	550	87.1	.775	907	262	1 1	300	200		990	967	956	325	. 362	220	362	55	0 0	4 6	2 4	192	.312	549	7	765	1.5396	906	751	9	166		7	6/	950	950	179	28.	. 163	0110			
	<b>:</b>	40			• -	<b>.</b>	• -	: 5	70	<b>∹</b>	<b>3</b>	3	<del>-</del> :	<b>→</b> .	<b>-</b> -	• -		70	5	7	<b>₹</b>	5	3	<b>.</b>			• -	 0	=	5	<b>-</b>	3 6	• •	70	<b>.</b>	• •		٦ 0	<b>.</b>	• ~	70	10	=	3	<b></b>	<b>:</b>	<b>?</b> ?	• 1	•	
80	<u>.</u>	1034	1706		1000	4500		5945	.606E	. 648E	701E	740E	. 00 J	27.0	8 4 5 t	3000	3072	950E	989E	000E	30 # O E	0416	1385	1456	30E	1977		4006	4886	. 626E	. 731E	7	1 60 50	939E	90806	140E	414	415E	7 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	6306	633E	. 6 3 9 E	6535	900 E	4040	7115	3797.	.087E	2306	



t = 172.24 sec.

READING # 0096 BLOCK # 76 TIME # 172,240 MACH 5.2 PT # 418,499 TT # 2259.8

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					<b>3</b>	∢ 7 2 .	<b>&gt;</b>	<u>د</u> د	# O							
<b>a</b>	I		GAMEA	1300	NÜS	MACH	VEL	S	٧/-	*	A/AC	HUY T	•	IVAC	H H	ETAC.
7 TUNNEL 100 418,499 22 100 0.587 3	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	576)	1.3161	26,859	2255	5,170	6267	1.782	0.14319	29.778	0.6119	3 0 0	10.969	157.3		
PIKE TIP NS 20060 22000 0000 2000 2000 2000 2000 2	C C C C C C C C C C C C C C C C C C C		3182	8 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	- M- M-		617	89	1631	29.77	0.811	5037	9	100		
170 TUNNEL 00000000000000000000000000000000000	147 147 185	46)	3986	6.839 6.858	255		~	.78	.1566	32.57	0.811	5112	2.			
PIKE TIP N8 0.600 22.462 224 0.600 20.161 218	447.16		3201	650	. 10 00	0.407	6		.1506	32,5	0,81	5115	. 50	•		
5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	189	100			2225	2.045		1.635	1.05951	32	0.1097	4140		127.1		
0.400 172.540 217 0.400 20.158 126	180.1	356)	1,3630	28.659	1721	2.051	3530	1.635	1.05353	32,571	0.1207	4197	37.800	126.9		
NTEL DANKER 0.400 117.418 21 0.400 95.824 20	2 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	526)	1,3203	26.859	2225	0.561	1220	1,061	1.05353	32.571	0.1207	4197	19.967	120.0		
0-410 173-400 21 0-410 23-860 13	194011	598) 324)	1,3203	28.859	1757	086	50 50 50	2635	15874	12.57	1001.0	6139	04	127.1		
DMBUGTOR 0 9	2 2 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	555)	1,3206	28,859	2221	727		1.840	.1582	32.5		3668		2 2		
10445 142.137 21 10445 142.137 21 10445 20.586 14	2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	555)	1.3207	26.659	2220	1.711	3143	1.847	1.15867	32.571	0.1098	1965	36.586	122.3		
1.500 140.661 21 1.500 28.947 14	426.1 ( 230.9 (	360)	1,3207	26,859	1841	80	3125	1.847	1.16059	32.571	0.1096	3976	50.364	122.1		
No. 400 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS. 707 NAS.	251.4(	552)	1.3211	26.859	2215	1.554	2930	1.654	1.14971	32,571	0.1106	3678	52,350	119.1		
12.002 112.003 21 4.163 113.003 21	417.1(	502)	1.3218	28.859	1911	1.054	2778	1.658	1.10479	32,571	0,1151	3801	47.687	116.7		
4.310 112.255 213 4.310 112.255 213 4.310 34.667 156	264.3	546)	1,3218	28,859	1914	1.442	2760	1.859	1.10419	32,571	0.1152	3793	47.362	116.5		
4.000 109.136.23 4.000 35.054.16	2118.00	399)	1,3433	28.859	1920	1,399	2693	1.860	1.10061	32,571	0.1155	5764	90.00	115.6		
200 100 00 215 200 100 00 215 200 100 00 100 00 100 00 100 00 100 100	416.76	544)	1,3221	28,859	1927	1,392	2662	1.860	1:09955	32.571	0.1157	3759	45.638	115.4		
6.266 101.696 23 6.266 101.696 23 6.266 33.253 15	268.6 268.6 268.6	540)	1,3226	28,859	2194	1.388	2667	1,863	1.03745	32,571	0.1226	3744	43.006	115.0		
7-310 100-217 21 7-310 28-100 15	250-16	557)	1,3229	26.459	2189	1,492	2810	1.862	0.96500	32,571	0.1318	3793	42.157	110.4		

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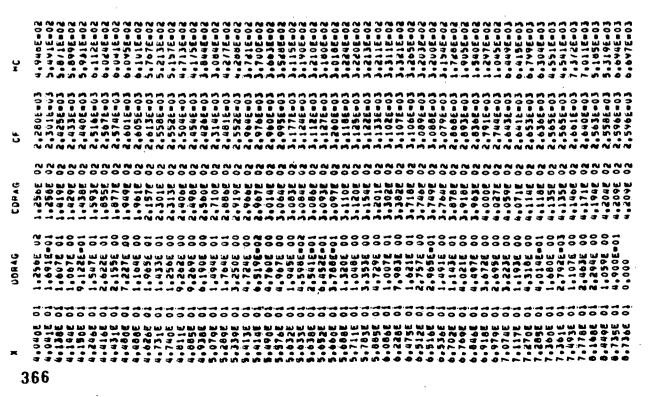
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	IVAC	116.6	118.2	119.8	120.7		130.5	132.7	133.7	133.6	137.3	-	57.	•	. ag		. 5	•	161.1	163.4
	3	590-27	41,223	940.08	37.270	3.70	21.501	19.039	17.195	17.175	15.764	14.585	1.43	77		98.1	11.599		11.073	11.502
	RUVIR	3709	3650	2005	3931	920	4265	4336	6097	0 1 7 7	4527	1997	9	152		281	2	. 62	5357	5431
	A/AC	1327	. 1415	.1554	1662	.195	. 2379	. 2480	.2020	.2631	.2782	.2950		747	368	175	ņ	.368	.3694	.3753
•		32.571 0	12.571 0	12.571 0	12.571 0	2,571 0	2.683 0	32.683 0	32.964 0	2.964 0	2.964 0	32.964 0	3,244 0	22.244	3.244	3.244	3.244 0	3.244 0	3.244 0	33,244 0
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11 66		.868	.862 0	. 662	.664 0.	.663 0.	.0 769.	.897 0.	.150 0.	.151 0.	.161 0.	.172 0.	.365 0.		368 0	.370	.368 0.	.371 0.	.372 0.	2.377 0.
418.4	VEL .	2827 1	2952 : 1	3071 1	3134 1	3331 1	2579 1	2361 1	2 0 2 2	2289 2	2163 2	2151 2	2085 2	2086	139	2134 2	2113	2124 2	2138 2	2140
5 P1	HACH	1.505	1 1.602	2. 6 1.700	1.755	1,941	1.318	1,195	0.021	0.050	0.871	9.836	0.7	0.7		0.750	9,142	0.742	0.743	16.757
ě.	80N	2188	2185	218	2180	4174	2205	2203	2556	2596	2644	2695	2919	2919	293	2941	2941	29562	2968	2994
O MAC	HOLE	26.659	26.654	28.858	26,859	26.659	28.779	26.779	26.615	26.617	26.772	26.953	24.666	24.671	24.925	24,949	24.944	25.006	25.056	25.165 25.171
172.24	GAMA	1.3230	1,3232	1.3234	1,3835	1.3240	1.3211	1,3213	1.2944	1.2943	1.2861	1.2507	1.2693	1.2692	• •	1.2654	1,2656	1.2628	1,2604	1.2553
11×6 =		( 537)	( 535) ( 361)	( 533)	( 532)	( 529)	( 546)	( 546)	C 804)	( 804)	( 845)	( 892)	(1041)	(1072)	1001)	(1000)	(1045)	(1113)	(1128)	(1189)
* 7	E,	407.34 268.0	405. 231.	20 4 6 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	# 0 # 0 # 0 # 0 # 0 # 0 # 0 # 0 # 0 # 0	1000.7	200	2000	4 4 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6		407	404°2	410.1	418.	8 417.6 826.4	417.3		£ 18	, ki	
BLOCK	<b>-</b> -	2101	2002	2088	2064	2072	777	225	27.56	2768	200	3078	3357	3359	360	3 E E E E	1500	3460	3523	3615
9600	<b>a</b> .	100.241	23,778	19.946	95.113	871.61 13.149	75.014	71.057	32.308	52.285	31.045	49.866 38.518	45.967	45.972 32.864	45.756 32.273	45.646 32.316	46.345 33.030	46.527	33.271	35.500
EADING .	101040	7 * 4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0				0 4 6 U 8 T						5.760	6.320 6.320 6.320	0 - 8 - 8 - 9 - 9 - 9 - 9 - 9 - 9 - 9 - 9	0 MBUD 10 6 MGS 6 MGS	5.525 5.525 5.535			7.11.7	7.635
Œ	•	362	) <b>(</b>		) t t (			<b></b>		) W W C	3 GP GP (			n av av	UMM	O IN IÑ Ó	) Primit		າ <b>ເ</b> ນ ເນ ເ	. w w

DING .	9600	BLOCK	1,6	11×E #	172,24	IO MAC	2.5		418	4 667	172,240 mACH 5.2 PT # 418,499 TT # 2239.8	e.						•	PAGE
•	٩	-	x		GAMA	GAMMA MOLMT BONV	> 200		MACH VEL 8	80	<b>4/</b> #		A/AC	1011	3	IVAC	IVAC PHI ETAC	ETAC	
BUSTOR	•	26	31 4																
658	608.97	3714	0.80%	(1193)	1.2495	25.286	3020			,	1,2499 25,286 3020	1		•	•	1	;		
	33.450	3470	313.2	(1105)	1,2593	25.295	2931	0.743	2178	2,380	0.54366	33.244	0.3777	2500	2446 11.632 165.0 0.59 0.73	102.0	<b>2</b>	0.73	
BUSTOR	0	20	32		;	:	•												
.865	47,358	~	400.6(12)	(1235)	1,2419	25.447	3051				1,2419 25,447 5051		,					į	
,865	31.425	3538	202.6	(1126)	1,2543	25,461	2944	0,825	2430	2,384	0.35562	33.244	0.3650	2449	5449 13.430 163.9 0.59 0.79	163.9	0.50	6.40	
BUSTOR	0		33													-			
285	47.946	_	395.5(1246)	(1246)		25.498	3058				2399 25,498 3058								
265	29.906	3524	259.7	(1120)		25.514	2935	0.888	2607	2,303	0.36526	33.244	0.3553	9178	5416 14.799 162.9 0.59 0.81	162.9	0.59	18.0	
TC THRO	1 A 7		34 202	•				•								,			
	50.114	4283	395.6(1340)	(1390)		25.988	3151				.2120 25.988 3151								
	29.906	3909	234.1	(1252)	1.2295	26.038	3029	0.936	2942	2.390	0.36526	33.244	0.3553	5659	5659 16.135 170.2 0.59 1.00	170.2	0.59	00.1	
<b>40</b> 4	REGEN	7	35 21	• •	•			•	1				•						
285	979.67	3986	445.2(1	(1290)	1.2338	25,487	3098				2336 25,487 3098								
285	26,268	3547	266.7	(1129)	1.2528	25.513	2943	1.010	2472	2.396	0.36526	33.244	0.3553	2448	5462 16.671 164.3 0.59 0.81	164.3	0.59	0.61	
ZLE AL			36		,							1							
190	47.946	3847	395.5	(1240)	1.2399	25.498	3050				2804 28,498 3058								
. 191	1.077	1664	-389.3	( 493)	1.3261	25.526	2073	3.023	6267	2.303	0.06700	33.244	1.9371	7010	7010 6.526 210.9 0.59 0.61	210.9	0.54	19.0	
34 312;	_	77	37 4	•	•								•						
196	47.946			(1240)	1.2399	25.496	3058				.2399 25.498 3058							,	
198	0.669	1478	-447.6(	(425)	1.3364	25,526	1961	3,312	6499	2,383	0.04854	33.244	2.6737	7169	4,900 215.7 0.59 0.61	215.7	0.59	19.0	
ZZLE AE	REGEN		36 4																
1961	47.946		2000	(1800)	1,2330	25,487	3098												
198	1.153	1745	-363.4	(605 )	1,3221	25.526	2120	3,001	6361	2.396	0.06700	33.244	1.9371	7125	7125 6.624 214.5 0.59 0.81	214.3	05.0	191	
SLE PO	REGEN	7	39	,															
.361	976.60	3966	449.2	(1290)	1,2338	25,487	3098				. 2556 25.487 3098								
	699.0	1539	-426.5(	(404)	1.3329	25.526	1999	3.308	6612	2.396	0.04745	33.244	2,7356	7361	7301 4.875 219.6 0.59 0.81	219.6	0.59	0.61	
u	COMBUSTR	9											•					ı- •	
	72,540	4309	305.5	(1400)	1,2213	26,017	3171			•	.2213 26,017 3171								
205	0.669	1299	0.00	( 383)	1,3450	26.079	1796	4.103	7370	2.296	0.06608	33.244	1.9643	7952	7952 7,568 239,2 0,59 1,00	239.2	0.0	00.1	
TIVE NOZ	~	64	62 0																
361	52.449		361.5	(1213)	1.2412	55,499	3024				1,2412 25,499 3024							•	
361	1.469	2031	-270.6	( 602)	1.3094	25.526	2276	2,071	9624	2.423	0029000	33,244	1.9371	6536	6536 5.857 196.7 0.59 0.81	196.7	65.0	3.81	

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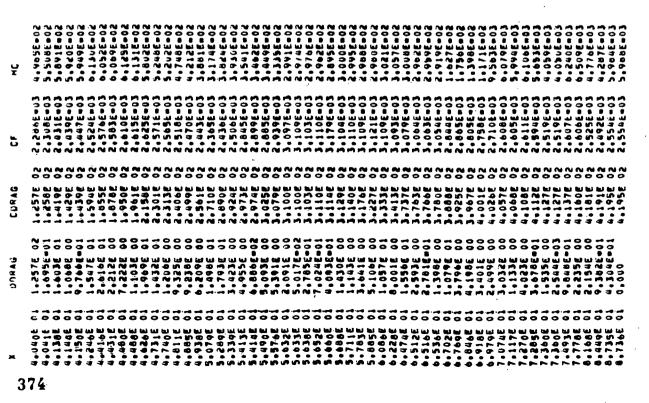
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	AVAC		0.3777			0.3650			0,3553			0.3553			0.3553			1,9371			2,5613			1.9371			2,6303			1.7309		1	1,9371
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80.340 MACH 5.2 PT # 416.749 TT # 2241.2	< \ z		241 26.541 2831 0.835 2365 2.290 0.34208 33.092 0.377		,	2616 26,575 2620 0,886 2499 2,288 0,35399 33,092 0,3650		2490 26,557 293A	0.36358		2406 26,726 2974	0.36358			2580 26,564 2852 0,927 2645 2,500 0,56358 33,092 0,3553		2490 26,557 2938	0.06670		2490 26,557 2918	0.05044			2028 3,005 6085 2,300 0.06670 33,092 1,9371			1921 3,280 6299 2,300 0.04912 33,092 2,6303			1623 26.753 1632 4.147 6767 2.190 0.07447 33.092 1.7349		2498 26,557 2910	0.06670
7 447	ø		2,290	 		2.288			2.286			2,286			2.300			2.286			2.286			2.300			2.300			2.190			2.330
416	VEL		2365			2499			2579			2726			2645			9979			6196			6092			6589			6767			5326
<u>.</u>	MACH VEL S		648			9980			916.0			296.0			156.0			1.031			3.284	•		800.5			1.260			1.147			2,426
5.2	SONV	9	2831		2943	2820		2938	2806		2974	2834		2984	2882		2938	1973		2938	1878		2984	2025		2984	1951		2962	1632		2910	2194
TARE D	NAME HOLKT BONY		20.541	•	26,564	26.575		26,557	26.568		26.726	26.744		26.548	26,564		26.557	26.574		26.597	20.574		2425 26,548 2964	26.574		2425 26.548 2984	26.574		26.735	26,753		20.557	26.574
-	W M M C		::	:	-			-	-		-	-		-	1.2580		1.2490	1.3325		1.2490	1.3416		1.2425	1.3276		1.2425	1.3375		-	-		٠	1.3134
TIME .		•	0 2 8 3	•	136)	010)	•	130)	008)		1773	(070)		1178)	(600)		11253	432)		1125)	386)		1110)	450)		178)	406)	•	1803	263)		106)	554)
1 65 1	I	31 4	291.3(1028	32 3	397,5(1	272.6()	33 2	393,6(113	260.6(1005)	34 202	393.6()	245.1	35 21	446.4(1	306.6(1049	36 4	393.6(11	-320.9(	37 4	393.6(1125)	-366.9(	30 4	446.4(1178)	-293.7(	30 4	446.4(1178)	346.7(	0 19	393.661	521,6	0	~	-198.76
9 <b>7</b> 00k	•-	38	3565	29	3707	3370	9				3833	3437	<b>7</b>	3827	3496	Ę,	3690	1961	7	3690	1404	S	3627	1651	9	3827	1474	9	1961	1052	•	3620	1959
8 9600			26.575	2		27,750	æ	45.311	8	THOAT	47.312	27.300	UP REGEN	45.311	27.122	۸Ę	45.311	1,012	<b>.</b>		0.668		45.311	1.052		_		œ	171.509	0.668	NOZZLE	22.937	1 . 4 2 7
READING		FBUB'S	56.65	BUSTO	8	60.861	BUSTO	62.291			_	62.281	JS T	62.28	62.29	MOZZLE	87.387	67.357	MOZZLE	87.357	87,387	372ZON	67.357	87.157	372 ZON	87,357	87.357	FICTIVE					

100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100		0	404 204 304	<b>*</b> 00	1.0	0 ÷	CAMALL	P=18/F8	14/81-4		9
	_	9	5.489E	20.0	00.	00	. 470E-U	10ZE 0	.3556-0	ě	30.
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1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,	_	9	2,3326	30°0 8	3	ê	0.3850	.780E 0	.630£-0	ĕ	00
Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colored   Colo	_	8	4.747	20.00	00	00	9008	TABLE D	0175-0	ĕ	
1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997   1997	_	0 9860	-5.498F	2 0.00	00	0	ANNE	1125		0776	4406
100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100	~	0.0518	4000	2000							
	•	2046	. F. B. D. F.								
100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100   100	•				0000		• 1 / KE U	0 40/C.	/ [	900	. 238690
No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No. 10.   No.	•		107000	2130.75	4 44.041E		ט אאנני	O BOOK O	• 3656 • C	. SESE O	.0096.00
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10.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00				1000000 V	360000	0 31604E 0	0 2/00	9000	. 3746.0	.727E 0	.787E-U
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1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00   1.00		417E 0	.6.366E	2 .4.688E	2 -1.5266	2 -1.162F 0	1145		061600	4176	
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\$\begin{array}{c} 0.0 = -0.036 & 0.3 = -0.026 & 0.2 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3 = -0.036 & 0.3	_	0 3797	<b>3</b> 59.64	2 -5.377E	2 -3.672E	0 3005.1- 5	253E 0	.533E 0	0405-0	2046 0	3.10E-0
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2.611E 01 =5.635E 02 =1.747E 03 =1.002E 03 =7.653E 03 3.904E 01 6.235E=02 3.907E 01 6.335E=02 3.904E 01 6.335E=02 3.904E 01 6.335E=02 3.904E 01 6.335E=02 3.904E 01 6.335E=02 3.904E 01 6.335E=02 3.904E 01 6.335E=02 3.904E 01 6.335E=02 3.904E 01 6.335E=02 3.904E 01 6.336E=02 3.904E 01 6.336E=02 3.904E 01 6.336E=02 3.904E 01 6.336E=02 3.904E 01 6.336E=02 3.904E 01 6.336E=02 3.904E 01 6.336E=02 3.904E 01 6.336E=02 3.904E 01 6.336E=02 3.904E 01 6.336E=02 3.904E 01 6.336E=02 3.904E 01 6.336E=02 3.904E 01 6.336E=02 3.904E 01 6.336E=02 3.904E 01 6.336E=02 3.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E 01 6.336E=02 4.904E=02 4.904E=02 4.904E=02 4.904E=02 4.904E=02 4.904E=02 4.904E=02 4.904E=02 4.904E=02 4.904E=02 4.904E=02 4.904E=02 4.904E=02 4.	_	· Book o	*6.826E	2 .1.682E	3 .9.700E	2 .7.117E 0	BS6E C	10 M C	1125		
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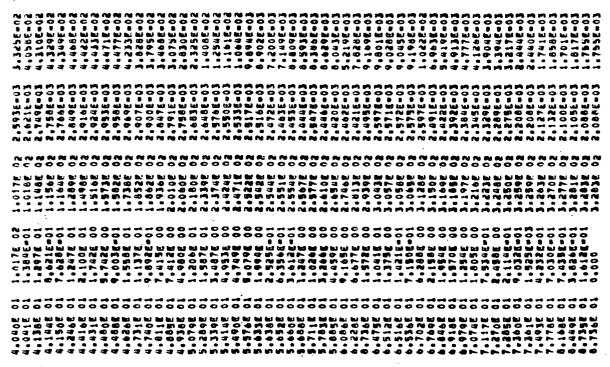
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Fuel flow measurement malfunction for 1B indicates no fuel flow from injector 1B. However, 1B manifold pressure indicates flow rates about as planned, similar to 1A. The performance program used fuel flow from 1A only.

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	P I	ı		010			0.10	•		01.0			010			010			0.10			0.10			0.10			0.10	•		0.10
	IVAC			120.4			125.6			125.0			129.9			4.5.4	,		141.6			150.0			146.7			166.0			140.0
	œ			4119 21. 420 120.4 0.10 0.00			4101 19.318 125.6 0.10 0.00			4044 11.778 125.0 0.10 0.00			4240 17.242 129.9 0.10 0.00			ubel 4.476 145.4 0.10 0.00			4628 5.429 141.8 0.10 0.00			4847 4.675 150.0 6.10 0.00			4855 5,390 148,7 0,10 0,00	•		5418 6435 166.0 0.10 1.00	•		4.377
	TCF 1			4119			4101	•		4507			1 0727			- 202		•	4628			1641			4855			5418			4596 4.377 140.8 0.10 0.00
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1 667	Ø			0 757.0			1.955 0			1.959 C			1.984 0			1.959 0			1.959 0			1.984 0			1.984 0			1.920 0			1.964 0
417.	4 1	ı		3754			3657			3620			3511			4380			4500			4573			0150			5139			1821
ā	11 A C 11			217.2			2.245	! •		2,251			1.905			3.450			3,431			3.586			3,421			4.260			3,503
5.6	SONV		1912	1536		2179	1594		2179	1008		2122	1787		2179	1198		2179	1253		2272	1275		2272	1318		5399	1201		2159	1222
1) A C 0	1.0.4		5/0004	27.004		27,603	27.602		21,002	210015		27.002	27.802		20802	27.80.75		27.802	208.12		27.002	27.006		27.802	27,602		28,365	20.564		27.602	27.802
264,04	4 1 4 1		1,3279	1.3810		1.3261	1.3781		1.3261	1.3769	•	1,3216	1.3610	; ;	1,3261	1.3982		1.3281	1.3969		1,3214	1.3962		1.3216	1.3947		1.3042	1.3944		1,3296	1.3977
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BLOCK # 178, 1	I	51 21	393.71	114.1	32 21	392.91	125.76	33 21	394.7	130.40	7 75	446.6(	200.3	35 4	392.7(	73.5	36 4	344.76	23.2(	37 4	446.6(	26.6(	78 4	7440.00	40.2	58	392.7(	-135.1(	29 0	361.5(	15.2(
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B BNID		<b>BUSTUR</b>						BUSTOR	127	127	BUSTOR	127	127	SLE AL	363	363	ZLE PU	363	363	SLE AE	363	363	SLE PO	363	363	TIVE CO	127 1	127	TIVE NO	363	363

35
.000 -44.707E 01 0.
.000 -2.343E 32 0.0
.000 =4.762E UZ U.
-048F 60 -55 NT F 62 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
.338E 00 -5.616E 02 0.
.375E 00 -5.837E UZ -2.1/
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.162E 01 -6.243E 02 -2.7
422E 01 = 6.421E UZ = 2.9
.01/E 0] .0.464E 02 .3.5. .735E 01 .7.324E 02 .5.6
9E 01 -7.759E UZ -5.8
.952E O1 =7.922E U2 =3.9
7**** 20 37:07*0* 10 300***
*425E 00 =8-707E UZ =4-6
-423E 00 -8.851E 02 -4.7
-403F 00 -1.07 E UN -5.9
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-100E 01 -1-25SE 03 -9-4
CONTROL OF STREET OF STREET
-632E O1 -1-164E O3 -1-1
.227E 01 -9.913E 02 -1.
.106E 01 -9.050E 02 -1.
7 1 20 30 1 1 1 0 0 0 100 50 50 50 50 50 50 50 50 50 50 50 50 5
.606E 00 =7.714E 02 -1.4
-700E 00 -7-514E 04 -1-4
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.555E 00 -6.852E 02 -1.5
*498E 00 =6.638E 02 =1.5
. 300E 00 =6.794E 02 =1.5
.478E 00 -6.761E UZ -1.5
-030E 00 -0-634E 02 -1-5
-/12E 00 -6-564E 02 -1.
- 10/6 00 80-30/8 02 81-
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173F OG =6.562F OF =1.
104F 00 404F0 00 4146

READING & 0096 BLOCK & 178 TIVE & 264.040 MACH 5.2' PI



t = 274.84 sec.

Injector 1B fuel flow measurement
malfunctioned,

READING B 0096 BLOCK & 140 TIVE & 274,840 MACH 5.2 Pt & 417,244 IT = 2221.4
RAMJET PERFURMANCE

TREPUBL REPUBL

ETAC								0.07	0.01	0.00	00.0	0.00	0.14	9.05	00.0	00.0	00.0	0.11
T i								0.20	0.0	0.20	0.40	0.0	0.20	0 • 60	0.20	0.40	0.20	0.60
IVAC	150.0	166.8	156.3	150.3	125.9	127.0	127.6	125.2	119.7	119.3	119.0	115.4	113.4	113.5	114.0	112.6	114.8	114.6
مي	344.0	1.844	.611	2.185	.743	65#*9	970.	£74.	565	160	.632	506.7	685	,352	.931	7.847	108.	42,756
¥ + 40×	4679 10	€ 967	2048 11	8405	4068 61	4128 50	4128 20	4067 64	3690 57	3876 57	3865 56	5747 5	3685 49	\$6/95	3659 47	3657 47	3666 45	3730 42
ž.												~					. 4	
AIAC	0.8118	0.8118	0.8116	0.8118	0.1097	0.1207	0.1207	0.1097	0.1098	0.1096	0.1097	0.1107	0.1150	0.1150	0.1155	0.1157	0.1225	0.1317
	878	# Z	562	8	536	548	244	2 0	60	997	9 9 7	987	487	40	999	Ø 90	•	
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4 / 4	.14370	.14570	.15534	.15534	1.06350	.04516	.0451	.15620	.15565	1.15673	1.15636	. 14549	1.10245	10246	20860.	1.09664	1.05522	0.96277
	0	O NJ	9	۰ م		-	~	-	~	~	67 1,	~		2 1.1	~	-	<b>~</b>	
Ś	1.78	1.48	1.78	9.0	1.838	1.836	1.86	1.973	1.968	1.96	2.96	1.98	2,003	1.98	1.979	1.97	1.97	1.447
VEL	8067	825	2697	706	3456	3476	1234	3586	3205	3179	3151	3253	2900	2081	2809	2818	2816	2858
Y ACT	5,170	0.5/1	5.074	104.0	1.984	2.004	995.0	1.986	1.706	1.691	1.670	1.758	1.437	1.076	1.457	1.438	1.450	1.434
3.4C	440	4247	2247	2247	2221	2221	2221	2308	2275	2271	22/0	2265	2321	2265	2254 1955	2252 1953	1942	1993
₩6L#1	9444	28.859	28,659	26.659	28,859	28,859	26,859	20.676	26.811	26,801	26.800	26.799	26,947	26,621	26,803	66.800	26,799	20.917
6 A 14 5 A	.3187 2	.3204 8	3167	1.5188		.3617	1.3206	3224	1,3257 2	3262	.3262	3266 6	1.3205 2	3203	1.3273	1.3275	.3260	1,3229
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	571)	571) 557)	571)	571)		556) 315)		598) 341)	577)	574)	574) 375)	571)	440)	571)	564)	56.3) 4(6)	559) 401)	590)
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-	2222 374	2222	386 386	4 2622 2164	5 2169 1293	2169 1283	2169	8178 1295	2106	2046 1405	2094	2084 1356	2211 1645	1522	2063	2059	.0.10	2152
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IVAC	115.1	•		119.1		0			125.2		125.6		136.1		120.0	į		ž	•	4		9.861		20.0		29.1	•	200		29.4		
	288	3 0 4		643	4	0	56.1	n >	217	•	916		. 536		335	•	2	4	2	454		427	•	540	•	633 1		372 1		371 1		
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30/0	1581.	.1415		.1554	44.	<b>3</b> 001•			.2379		.2480		.2631		.2782				90		•	.3716		.3675	•	.3686		1695		.3/53		
	0 497	0 997		0 407	4	9	44		597 0		597 0		597 0		547	604		597		607		547 0		597 0		0 46		97 0		0 / 6		•
•	2	32.		52.	2	2	2		32.		32.		2		7	42		. 2		2		32.		32.		32.5		32.5	•	32.5		
. Y/.	9.45592	0.09050		0.61617	C1447-0	700	25 0 S 0 0 0		0.53502		0.51316		0.46572		0.45743	0.41152		0.34595		80000		0.34250		0.34627		0.34531		94446	:	0.53914		
م	5 10 20	470		416	440		20		500		497		800		<b>9</b>	700		0.52		410	<b>,</b>	015		021		013		008		500		
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) ¥ ¥	1. ah	1.47		1.50	1.67	•	1.80	•	2.15		2.18		2.25	-	2.	2,15	•	2.24		2.43		2.46		2.30		2.40		2,42		2,20		
> ℃ Ø	2247	2237	2233	1865	2231		2320		1684	2	1662	2218	40	2216	701	2215		2253		2220		1560	1166	159	7	1559	i	1573	ŕ	1626	2211	9
	26,817	200.02	26.800	٥	26.799		27.009	•	26.686	۰	50.654	26.650	064.42	50.049	730.07	26.649		26.732		26.661	•	26.651	26-684	20.00		26.054	4	26.650	7	50.049	6	074
₹ Σ ₹ 9	1,3276	1,3265	1.3268	1,3564	1,3290		1.3197		1.160	3301	1.3762	1.3305	. 1770	.3306	**	1.3812		1.3268		1,3302		1.3837	1200	1.3807		1.3837	4011	1.3828		1.3740	1,3310	4.01
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POING .	9600 ×	# COC*	196	TINE R		De 90	7. X.	<u>a</u>	417.	F 317	274. Rub cach Sec Placificay II a cetto	<i>5</i> •						•	PAGE
	٩	-	I		4440	SAMPA NOLET SONV PACH VEL S	SONV	7 A T	V E.	ø	4 4	•	A/AC PUPIP G	7	ى	IVAC	PH	IVAC PHI PIAC	
MEUSTO	2					1			•							•	•		
.287	05.718	2273	341.46		1.5127	45.67	***			-	\$25.7 JULY 05.00 JULY 05.00								
.287	0000				1.3405	20.454	1454	1,405	4621	۲۰۰۰۶	C. 55415	54.547	6451.0	4213	4215 1r.545 129.2 U.cl 0,28	124.2	12.0	9240	
MBUSTO.	3												,				•		
.751	40.576				1.5128	27,055	2384				1.512A 27.055 2384								
.751	10.290				1.3385	27.055	2035	1.554	3175	4.011	0.53948	12.547	57/50	4203	4203 16.741 126.9 0.21 0.36	126.9	0.21	0.36	
FBUS TO	2						1								•		1	•	
.127	42.235				1.5199	76000	2318												
.127	7.785				1.5527	20.090	1897	1.707	3.553	450.5	1.3527 20.090 1897 1.707 3353 2.059 0.31561 32.597 0.4032	14.547	0.4052	4202	4202 15.447 128.9 0.21 0.22	128.9	0.41	0.22	
FBUS TO	R REGEN						,		<b>1</b>			•			•				
.127	42.238			634)	1.3165	20.897	2365				3165 20.897 2365								
.127	8.165				1.3460	26.896	1990	1.758	3389	2.072	0.31501	32.597	0.4034	4217	4277 16.622 131.2 0.21 0.22	131.2	0.21	0.22	
372Z	AE				•		·												
.363	42.235				1.3199	26.097	2318				1.3199 26.897 2318								
.363	0.581				1.3929	26.096	1351	3.400	1007	450.5	0.06570	12.597	1.9371	2567	4952 4.700 151.9 0.21 0.22	151.4	0.21	5.2%	
. 3722	00												•			•		•	
.363	42.235				1.3149	46.897	2318				3149 40.897 2318								
.363	. 0.657				1.3919	20.096	1374	3,325	4567	2.059	0.07118	32.597	1.7880	4928	4928 5.052 151.2 0.21 0.22	151.2	0.21	0.22	
272Z	AE MEGEN											) )	•				;		
.363	42.235				1,3165	26.897	2365				1,3165 26,897 2365								
. 163	0.605				1,3911	26,496	1392	3,375	4697	2.072	0.06570	32.547	1.9371	2060	5060 4.796 155.2 0.21 0.22	155.2	0.21	0.22	
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, 363	42.235				1,3165	26.897	2365												
.163	0.657				1.3964	20.00	1007	3,320	4673	2.072	1.1964 26.496 1407 3.320 4673 2.072 0.06931 32.597 1.8363	32.597	1.8363	8008	5043 5.033 154.7 0.21 0.22	154.7	0.21	0.22	
CIIVE	COMBUSTR												) }						
.127	163,093				1,2824	27.796	2635				1,2824 27,796 2635								
.127	C. 657				1.3851	27.797	1367	4.213	5760	450.5	0.09016	32,547	1.4116	6073	6073 6.U71 186.3 0.21 1.0U	186.3	0.21	1.00	
CTIVE	37220N												•		,			•	
.363	24.873			610)	1,3195	20.096	2324						1,3105 20.606 2324						
. 163	0.780				1.3843	26.096	1816	2.805	4345	2.100	0.06570	32.597	1.9371	4787	4.434	146.9	0.21	0.22	•

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## RAMJET PERFURMANCE

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PRADING B 0097 BLOCK B 29 71KE B 135.714	7 0 1	5.2 PT # #10.750	11 # 2096.6			9 A G E
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t = 156.41 sec.

MEADING 8 0097 BLOCK 8 52 TIME 8 156 414 MACH 5.2 PT 8 209.750 TT 8 2180.0

IVAC PHI ETAC 2599 1.055 154.9 5.840 155.0 0.484 154.0 5.714 154.9 2146 32.468 127.9 2174 30.021 129.6 2174 9.591 129.6 2145 34.158 127.9 2082 30.322 124.1 1950 25.940 118.0 1989 25.856 118.5 2017 25.781 120.2 2077 30.617 125.8 2067 29.676 123.2 2021 28,167 120.5 1990 26,385 118.6 1986 26.210 118.3 1980 25.944 118.0 2518 7364 2599 FORTE 2228 939 5.170 4857 1.822 0.07340 16.247 0.8643 28.036 2228 20.036 2202 0.392 862 2.027 0.07540 16.247 0.8643 28.837 2228 28.836 946 5.129 4851 1.822 0.07579 10.778 0.8643 20.036 228 2200 0.407 096 2.027 0.07579 10.778 0.8643 28.836 2197 26.836 1644 2.203 3624 1.865 0.53302 16.778 0.1229 28.836 2197 28.836 2150 0.534 1156 1.900 0.53302 16.778 0:1229 28.836 2191 28.836 1743 1.906 3321 1.876 0.58751 16.778 0.1115 20.036 2191 20.036 1746 1.891 3504 1.877 0.58843 16.778 0.1113 28.436 2190 28.436 1758 1.859 3267 1.878 0.58842 16.778 0.1113 28.636 2163 28.636 1796 1.734 3111 1.884 0.58261 16.778 0.1124 28.436 2173 28.436 1810 1.666 3014 1.868 0.36330 16.778 0.1163 20.036 2171 20.036 1812 1.650 3000 1.668 0.56226 16.778 0.1165 28.836 2169 28.836 1813 1.649 2982 1.888 0.55978 16.778 0.1170 28.836 1813 1.645 2982 1.888 0.55979 16.778 0.1170 28.636 2165 28.636 1796 1.667 3029 1.667 0.54929 16.778 0.1193 24.036 2162 28.030 1757 1.790 3146 1.083 0.52753 10.778 0.1242 28.636 2197 28.636 1667 2.137 3563 1.865 0.56777 16.778 0.1117 24.836 2197 28.836 1679 2.102 3530 1.865 0.58625 16.778 0.1117 AIAC GAMPA MOLET SONV BACH 28.637 959) 1,3203 89) 1,3982 542) 1,3225 288) 1,3685 1,3242 542) 1.3225 293) 1.3673 1.3230 1.3244 1.3248 1,1225 1.3259 1.3230 1,3231 1.3235 1.3243 1.3246 1,3246 543) 1.3204 542) 1.3225 545) 542 536) **537**) **32**4) 526) 523) 526) 534) 527) 525) \$25) 348) 849) (65) 394.36 216.2 430.3 216.9 218.4 115.4 14.2 217. 397. 12 99.080 211) 10.050 1178 209.750 2180 10.725 4180 209.750 218 TIME ON GILL D 9.014 1 40.18 10.725 9.629 63.638 4.160 54.279 13.406 82.126 12.422 19.891 71.225 65.153 64.519 63.654 14.162 12.268 12.721 13.649 70000 511.71 JSTOR

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,	0	25.219	25.210	24.419	5	\$0.20	19.111	12,339	8.313	7.846	7.850	7.658	7.996	6.847	5.024	5.014	5.633	5.552	5.002	20 20 40 30
	7 - 7 - 7	9502	802B	2043	90	8602	2128	2238	2472	2533	2608	5609	2693	2796	3164	3165	3192	3207	3216	3243
	34/4	0.1335	0.1335	0.1432	4	0.1554	0.1062	0.1950	0.2379	0.2480	0.2629	0.2631	0.2782	0.2966	0.3676	0.3679	0.3691	0.3715	0.3675	0.3688
. 0.	ĸ	16.778	16.778	16.778			17.016	17.016	17.128	17.128	17.224	17.224	17.224	17.224	17.320	17.320	17.320	17.320	17.320	17.320
1 m 218	4/4	0.49076	62044.0	0.45736		27.5	0.39983	0.34076	0.28112	0.26964	0.25579	0.2559	0.24170	0.22670	0.18394	0.18381	0.18523	0.18201	0.18402	0.18338
1,750 7	•	1.678	1.678	1.674	5	2.166	2.180	2.257	2.302	2.310	2.423	2.423	2.445	2.449	2.577	2.577	2.596	2.596	2.022	2.621
1 = 609	כא יפּנ	45 3507	47 3308	83 3436	u	0505 50	46 3076	64 2330	51 -1903	UB 1872	45 1976	26 1978	56 2129	80 1944	78 1758	77 1758	8791 EÉ	.648 1963	25 1749	15 1717
S. A. P	BONV HAC		2157		٠		2343	2416 0.9	2696	2734 2646 0.7	2819 2724 0.7	4841 4725 0.7	2918	2938 2856 0.6	5100 5041 0.57	3100 3041 0.57	3189	3191	3361 3328 0.5	3361 3330 0,5
£ 04 £	HOLWT 80	8.636 215' 8.636 170	8.636 21 8.636 16	6.636 215 6.636 164	4.365 23	24.366 230	24,432 23	4.936 23	5.041 26	25.147 27	747	23.750 c6	4.034 29	14.10d 29	3.094 51	3.095 31 3.096 30	3,422 31	3.435 31	4.436.53	4.436 53
156.414	GAHHA	3654 26	.3254 24	3757 2	3345 24	.3345 24	3312 2.	3008 2	3003 2	2953 2	2895 23 2967 23	2896	2757 2	2764 2	2658 2	2589 2	2461 2	2391 2	1595 20	.1597 24
1776	-	5193 1.	\$19) 1 301) 1	517) 1	584) 1	584) 1	417) 1	770) 1	871) 1 799) 1	963) 1	958) 1	959) 1	1056) 1	1078) 1	1230) 1	1229) 1	1350) 1	1354) 1	1702) 1	1702) 1
5.5	1	189.6( 171.3(	389.	387	26.	16 2 413.90	412.	407. 299.	397.	395.	402. 324.	402. 324.	* ~ ~ ~	395.8(	#00# #38.6C	330°56	3 17 1	399.6( 322.8(	, , , , , , , , , , , , , , , , , , ,	398.5( 339.6(
BLOCK		1263	2037	2029	1957	23 1958 1371	# Q 3 ·	4 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	2635	2933	2944	2948	3226	3091	3563	3542	1966	3674 3698	4768 4668	3 4
1600	<b>a</b> .	70.486	70.523	74.105	48.597	46.539 12.187	11.77	35.67	33.44	35.07	31.970	31.95	31.025	30.79	24.22	29.22	28.73	26.72	24.16	24.55
REACING .			7.819	6 110 6 110 6 110	90.0	COMBUSTOR 48.769 48.769		7000												0000

READING # 0097 BLOCK # 52 TIME # 156.414 MACH 5.2 PT # 209.750 TT # 2180.0 ...

	•	-	Ľ	GAMPA	GAMPA MOLWT SONV	SONV	HACI	MACH VEL	ø	4/2	3	A / A C	えことつよ	c	IVAC	IVAC Pri ETAC	ETAC
_	O 0	<b>9</b>	51 21			•					•						
7.025		4787	397.0(1701)	1.1547	24.439	1361											
•	24.003		329.8(1658)	1.1630	24.304	5324	455.0	2401	4.620	1.1850 24.204 3324 0.554 1842 4.850 0.18508 17.320 0.1854	17.320	4565.0	1263	3265 Section 1881 185.4 Section	180.4	0.0	1.00
COMBUSTO	0		32 21			•	•					•					<b>.</b>
87.749	28.536	4763	394.9(1700)	1.1599	200002	3359											
57.749	22.250	4637	299.8(1619)	1.1647	24.532	3308	0.659	2182	2.620	1.1647 24.532 3368 0.659 2182 2.620 0.18019 17.320 0.1753	17.320	15/1-0	1111	1313 6.109 191.3 0.90 1.03	191.3	0.00	1.00
COMBUSTO	Œ	7	33 21							•							•
59.769	26.990	4760	391,1(1698)	1.1603	24.440	3358											
56.769	-		315,7(1650)	1.1640	24.519	5318	0.585	1943	2.018	1.1640 24.519 3318 0.585 1943 2.618 0.17904 17.320 0.1777	17,320	1111	3349	00.1 09.0 4.891 S04.2 PARE	193.4	0	4.00
COFBUSTO	<b>6</b> 22		34 21		• •	•	•			•	) 	•					•
60.779		4771	183.2(1694)	1.1610	24.468	3356											
60.179	21.675		267.8(1619)	1.1673	24,560	3293	0.730	7072	2.615	1.1673 24.566 3293 0.730 2404 2.615 0.18527 17.320 0.1650	17.320	0.1650	6320	3320 6.921 191.7 0.90 1.00	191.7	00.0	1.00
00.00.00	Œ		35 400			•				•			1		•		•
65.199	29.907	4	377.4(1692)	1.1616	24.469	1354											
65.199	17.587		179-5(1560)	1.1740	24.043	3246	0.970	3147	2.613	1.1740 24.043 3246 0.970 3147 2.013 0.19030 17.320 0.1553	17.320	1561.0	5025	00-1-00-0 6-001-001-6 50-55	196.5	00.0	0.0
COMBUSTO	œ		~			,		-									•
65.199	29,907			1.1583	24.409	3374				•							
65.199	13.475	7567		1.1709	1.1709 24.673	5213	1.196	3651	2.623	5213 1-196 3651 2-623 0-19030 17-320 0-1553	17,320	1551.0	3.500	3300 11.189 190.5 0.00 1.00	100.5	00.00	00.1
37220N	1 F		37 4				•	•						•			
67.475	29,907	4765	377.4(1669)	1.1616	54.469	1354											
87.275	0.729		96.00	1.4786	1.4786 24.905	2510	3.940	7329	2.613	2,940 7329 2,613 0,03491 17,320 1,9372	17.320	1.9372	4307	4307 3.976 248.7 0.90 1.0u	748.7	00.0	00.1
N022LE	3°	4				•			• • • •				•				
17.275	29.907	*	377.4(1669)	1.1616	24.469	3354											
67.279	0.311	2041	-849.2( 636)	1.2951	1.2951 24.905 2297	2297	3.411	7835	2.613	3.411 7835 2.613 0.01922 17.320 3.4182	17.320	3.4182	4000	00.1 00.0 7.050.7 0.04	250.7	00.0	00.
NOZZLE	AE REGEN	4					•				1		•				
87.275	49.907	4856		1.1583	1.1583 24.409 5374	5374					•						
87.275	0.747	2550	•	1.2756	24.905	2548	2,900	7391	2.623	2,900 7391 2,623 0,03491 17,320 1,9373	17.320	1.9373	6757	4349 4.09 251.1 0.90 1.00	251.1	06.0	0001
MOZZLE	PU REGEN		# 0#					,					)			:	•
87.875	29.907			1.1583	54.409	3374											
. 67.275	0.311			1.2926	1.2926 24,905	2328	3.403	7922	2.623	3.403 7922 2.623 0.01689 17.320 3.5804	17.320	3.5804	0757	4549 2.125 262.7 0.40 1.00	262.7	0.40	000
FICTIVE	COMBUSTR		29	1				I			•		· •			:	
65.199	99.080	3	377.4(1731)	1.1745	24.582	3400					•				-		
2	0.311	1533	1621-7( 463)	1.3209	1.3209 24.405	2010	4.162	8367	2.516	4.164 8367 2.516 0.02733 17.320 2.4742	17.320	2.4742	4701	00-1.00-0 0-112 055-1	271.4	. 00 0	00-1
FICTIVE	NOZZLE		0 79				•	•	· · · · · · · · · · · · · · · · · · ·	) )			:				
87.275	14.418	-	J	1.1576	24.454	5304											
~	1.023	3019	-467.9( 994)	1.2569	34.900	2753	2,323	6395	2.662	1.2569 24,900 2753 2,323 6395 2,662 0,03491 17,320 1,9371	17,320	1.9371	3950	3950 3.469 228.1 0.90 1.00	226.1	0.00	00.1

REPRODUCIBILITY OF THE 7.665E 7.162E 7.665E 6.477E 2180.0 209.750 -7.007E -7.384E -8.012E . = 5.2 # 156.414 -4.8136 9.768 -3.08 .3.66 717 BLOCK 1000 000000000000000000 . READING

PEACING .	1600	1	BLOCK .		7176	\$	717	3 4 5	5.2	• . •	= 204.75u	150	=	2160.0	Q ,		•				•	PAGE 5
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0 3995.0	-	399E	1 10	399£	5	•	~	-1.800E	6	-9.553	E 02		29E	~	3682.	50	4.5036	<b>?</b>	6.669E=U2	4.503E	70	6.669E=U2
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.250 IT	s	1.876	1.876	1.872	1.870		1.865	1.930	1.939	2.173	2.173	2,175	2,194	2.356	2.356	2,363	2.362	2.378	2,376	
210.	VEL	3305	3306	3421	3517		5727	3082	2726	2873	2876	3088	2442	2031	2022	2170	1112	1830	1617	
PT =	MACH	.952	426.	2.077	2.188		2.471	1.673	1.413	1.208	1.209	1.314	0.954	.727	0.724	0.770	0.749	0.615	0.541	
5.2	SONV	2152 1693 1	2152 1692 1	2149	2146		£139 1508 2	2211	2209 1929	2608	2579 1	2616 2350 1	2705 2559 (	2880 2792 0	2791	2915 2618 (	2910	3030 2976 0	3030 2988 (	3030
4 MACH	MOLWI	28.836 28.836	28.836	28.836 28.836	28.836		28,836	28.687	28.687	27.182 27.183	27.183 27.184	27.217	27.534	25.761	25.756 25.759	25.895 25.902	25.878	26.437	26.43A 26.450	26.438
: 182.514	GAMMA	1.3258	1.3258	1,3260	1.3262	3263 3764	1.3267	1.3203	1.3205	1.2884	1.2884	1.2871	1.2738	1,2642	1.2648	1,2574	1.2584	1.2267	1.2269	1.2270
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3.1	3	0.701 2074 2.376 0.17994 17.296 0.3753	0.554 1654 2.373 n.17880 17.296 0.3777	0.672 1987 2.371 0.18502 17.296 0.3650	17.2	17.2	17.2	3.016 6240 2.369 0.03486 17.296 1.9371	3.371 6518 2.369 8.02339 17.296 2.8877	2.995 6326 2.381 0.03486 17.296 1.9371	3.367 6626 2.381 0.02289 17.296 2.9504	4.297 7007 2.264 0.03610 17.296 1.8704	17.2
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PT =	MACH, VEL	.701	. 534	.672	.911	•000	<b>.9</b> 40	.016	.371	.995	.367	.297	.531
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## RAMJET PERFORMANCE

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ETAC																		
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IVAC	154.4	158.8	154.3	154.3	127.5	129.2	129.2	127.5	123.8	123.5	122.9	120.2	118.3	118.1	117.8	117.8	118.4	120.1
ø	5,563	0,985	5,754	1.064		30.273	9.665	32.432	30,581	30.475	30.132	28,397	26.594	26.420	26.162	26,158	26.096	26.035
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<b>4/8</b>	.07397	.07397	.07662	07662	57220	.53864	.53884	59265	59392	.59465	.59484	0.58897	.56945	.56840	.56589	.56590	55529	53309
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S	1.820	2.025	1.820	2.025	1.863	1.863	1.698	1.863	1.674	1.675	1.876	1.683	1.886	1.887	1.887	1.887	1,085	1.882
VEL	4839	857	4833	893	3558	3615	1154	3521	3313	3297	3260	3102	3005	1667	2975	2974	3024	3143
MACH	.170	.390	.125	.407	.143	.207	. 538	2.104	.907	.892	.859	1.731	.662	.653	.642	.642	.685	.790
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GAMMA	1,3208	1.3209	1.3208	1.3209	1.3230	1.3230	1.3230	1.3679	1.3234	1.3234	1.3234	1.3239	1.3245	1.3246	1.3244	1.3248	1,3250	1,3252
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7.485E 01	7.0				1.288E		-1.893E	03	-1.002E	3	3.912E		5.426E	03	_		.895E-03	0.000	00.0	0
7.770E 01	7.2				1.347E		-2.057E	03	-1.022E	3	1.035E		5.52SE	20	4.117E 0	9	.136E-03	0.000	00.0	o
8.160E 01	7:7				1.399E	03	-2.074E	0	-1.039E	S	1.035E	03	5.630E	03	3.718E 0	0	.541E-03	00000	00000	0
8.441E 01	7				1.427E	03	-2.088E	S	-1.053E	03	1.03SE	03	5.684E	03	4.309E 0	9 0	.421E-03	0.00	00.0	0
8.727E 01	8°7 1		00000	_	1.466E	S	-2.114E	03	-1.080E	03	-1.035E	03	5.707E	03	6.000E 0	9 00	8.9426-03	0.000	0.000	
8.727E 01	1.8				1.466E	03	-2,114E	03	-1.080E	03	1.035E	03	5.707E	03			.947E-03	0000		

# RAMJET PERFORMANCE

			SUPERSONIC 0.9218 SUBERSONIC 0.9268 SUBSONIC 0.8908 SUBSONIC 0.8908	OR	0.7310: 0.6854		- CS 0.9389		VALVE	ա <b>ա</b>
ANCE	INIET	LOW RATIO	INCET PROCESS EFFICIENCY - SUBSONIC KINETIC ENERGY EFFICIENCY - SUBSONIC KINETIC ENERGY EFFICIENCY - SUBSONIC ENTHALPY AT PO - SUPERSONIC ENTHALPY AT PO - SUBSONIC	COMBUSTOR	EQUIVALENCE RATIO	NOZZLE	VACUUM STREAM THRUST COEFFICIENT - CS NOZZLE COEFFICIENT - CT	FUEL INJECTORS	INJECTORS STATION 1A 40.400 1B 41.284 1C 44.300 2A 48.759	2C 46.250 3A 54.049 3B 56.234 4 44.784
RAMJET PERFORMANCE		(LRF) (LRF-SEC/LBM) (LRF-SEC/LBM)	(LBF) (LBF) (LBF-SEC/LBM)		(18F) (18F) (18F)		(LBF) (LBF) (LBF) (LBF)	·	2222	( ( ( ( ( ( ( ( ( ( ( ( ( ( ( ( ( ( (
	ENGINE PERFORMANCE	IC IMPULSE	REGENERATIVE-COOLED ENGINE PERFORMANCE CALCULATED 3780.  ST	MOMENTUM AND FORCES		*	AAL FRICTION DRAG	STATIONS		
4	466	CALCULATED THRUST MEASURED THRUST CALCULATED SPECIFIC MEASURED SPECIFIC CALCULATED THRUST MEASURED THRUST	REGENERATIVE-COOLED ENGINE CALCULATED STREAM THRUST	-	TOO ST	NOZZLE MOMENTUM CHANGI NOZZLE PRESSURE INTEG	EXTERNAL FRICTION DRAG EXTERNAL PRESSURE INTEGRAL TOTAL STRUT DRAG CAVITY FORCE CALCULATED LOAD CELL FORCE FUEL VACUUM SPECIFIC IMPULSE -137.8.		NOMINAL COWL LEADING EDGESPIKE TRANSLATIONINLET THROATCOWL LEADING EDGE	NOZZLE PLUG TRAILING EDGE

t = 224.81 sec.

-	<u>-</u>	r		GAMMA	VOL*T	SONV	MACH	VEL	s	W/W	3	A/AC	MOM IN	ø	IVAC	PHI	ETAC
100 210	.750 21.	1 0 4 66 426.4 64 -41.8	( 555)	1.3208	28.837	2221 936 5	5.170	4840 1	.820	0.07412	16.408	0.8643	2534	5.575			
01 01 19 19 19	.825 21		( 541)	1.3208	28.836	2221 2196 0	0.390	857 2	.025	n.07412	16.408	0.8643	2606	0.987	158.9		
0.000 210 0.000 0	0.314 3		( 555)	1.3902	28.837	2221 943 5	.125	4834 1	0 029.1	.07678	16.997	0.8643	2623	5.768	154.3		٠
	9.717 211	4 10.	( 555)	1.3208	28.836	2221 2194 0	0.407	893 2	0 420.	.07678	16.997	0.8643	2623	1.066	154.3		
2	.019 1162		( 537) ( 284)	1.3695	28.836	2189 1656 2	.151	3862 1	862 0	.57337	16.997	0.1117	2168 3	32.879	127.6		
001 004 04	030 112		( 276)	1,3231	28.836 28.836	2189 1634	2,215	3619 1	1.662 0	.53996	16.997	0.1229	2196 3	30,369	129.2		
#0.400 50. #0.400 50. #0.400 50.	202	7 0 4 01 408.0( 07 381.5(	( 937) ( 511)	1.3231	28.836 28.836	2143 0	0.537	11511	0 768.1	.53996	16.997	0.1229		661			
		159.8	( 837)	1.5231	28.836	2189 1669 2	.112	3526 1	662 0	.59388	16.997	0.111.7	2168 3	32.542 1	127.5		
<b>3</b> 24	.641 20 .264 12	184.6	( 834) ( 314)	1.3238	28.836 28.836	2183 1732 1	916	3321 1	n 878.	.59515	16.997	0.1115	2105 3	30.715 1	23		
£ 63 12 €	~ ~		( 533) ( 31 <b>5)</b>	1,3236	28.836	2183 1737 1	.903	3304 1	673 0	.59609	16.997	0.1113	2100 3	30.610 1	ື້		
18 81 12 12			( 320)	1.3236	28.836	2182 1747 1	.871	3268 1	.875	n.59608	16.997 (	0.1113	2089 3	30.272 1	o,		
22 13	.591 2073 .820 1361		( \$29)	1.3241	28.836	2175 1784 1	.745	3114 1	681 0	.59020	16.997 (	0.1124	2043 2	28.565 1	120.2	•	
<b>9</b> 61		394.0	( 523)	1.3249	28.836	2165 1797 1	.681	3022 1	884 0	.57063	16.997	0.1163	2013 2	26.796 1	118.4		
\$9.4 •		293.3	( 522)	1.3250	28.836 28.836	2163 1799 1	.672	3008 1	684 0	.56958	16.997	0.1165	2008	26.628 1	118.2		
		212.7	( 542)	1,3251	26.836	2161 1800 1	.663	2994 1	.885	0.56706	16.997	0.1170	2003 2	26.385 1	17.9		
		291.9	( 521)	1,3251	28.836	2161 1800 1	.663	2994 1	.885	0.56707	16.997	0.1170	2003.20	6.381 1	17.9		
	.013 2036 .269 1355	290.1	( 519)	1.3254	28.836	2158 1761 1	.710	3046 1	.883 n	.55644	16.997	0.1193	2014 2	26.341 1	18.5		
68 11		368.3	( 518)	1.3256_	28.836 28.836	2155 1741 1	.819	3167 1	.879	0.53419	16.997	0.1242	2044 2	26.288 1	120.3		

READING =	7600	BLOCK	= 128	TIME =	= 224.8	814 MACH	5.2	PT =	210	.750 T	TT = 21 <b>6</b> 6	6.						PAGE	6F 2	
	. a.		±		GAMMA	<b>MOLWT</b>	SONV	MACH	VEL	s	W/W	*	A/AC	KONTH	ø	IVAC	PHI	ETAC		
COMBUSTOR 47.310 47.310	73,122 9,619	2022 1202	12 385.8( 164.6(	515)	1.3259	28.836 28.836	2150	1,677	600	, A74	40714	7.00.41	1 to 1 to 1 to 1 to 1 to 1 to 1 to 1 to	, Ago	704	000				
UST0	73.161		13 385 164	515)	1.3259	28.836 28.836	2150 1682				0.49692	16.997				122.A				
30STO	76.409 8.149		<b>→</b> •	513)	1.3262	28.836 28.836	2147 1635	2.107	3445	1.670	0.46331-16	16.997	0.1432	2119	24.807	124.7				
7697	78.637 6.899	7 2010 7 2010 9 1069	777	\$11)	1.3264	28.836 28.836	2144 1592	2.227	3546	1.867	0.42702	16.997	0.1554	2148 2	23,532	126.4				
0	80.238 6.052		٠ .	510)	1.3265	28.836	2141 1559-2	320	3618 1	1.865	1.39937	16.997	0.1662	2169 2	22,453	127.6				
ō ′	00.2		<b>=</b> "	506)	1.3271	28.836	2134 1427	2.717	3877	1.847	0.34037	16.997	0.1950	2248 2	20.507	132.3				
ō ?	44.954 19.100		=	546)	1.3210	28.687 28.687	2201 1992	1.195	2380	1.934	0.28079	17.108	0.2379	2429 1	10.384	142.0	0.03 1	00.		
2 9	40.613	2 2 10 2 2 10 3 1813	- ,	844) 460)	1,3213	28.687	2198 2046 (	0.999	2045	1.940	0.26932	17.108	0.2480	2481	8.559	145.0	0.03 1	00.		
5	31.075		393	897)	1,2863	25.695	2718 2627 (	0.724	1903	2.280	0.25716	17.316	0.2629	2533	7.607	146.3	0.45	\$0°		
	31.069 22.413	2 2 2 5 9 6 9 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	393	897) 826)	1.2863	25.697	2718 2628	0.724	1902 2	2.280	0.25696	17.316	0.2631	2534	7,597	146.4	0.45 0	<b>.</b> 10.		
54.819 54.819	30.693 22.900		380	934)	1.2806	25.829 25.830	2757 2677	0.686	1835 2	2.288	0.24300	17.316	0.2782	2620	6.931	151.3	0.450	. 09•		
55.760 55.760	30.532		886 836 830	450)	1.2781	25.894 25.895	27.73 2706	0.624	1688	2,291	0.22792	17.316	0.2966	2728	5.977	157.5 (	0.45 0	.63		
56.234 56.234 56.234	29.118 24.472		407.7( 362.8(	1029)	1.2867	22.801 22.801	2913	0.524	1506	2.524	0.18612	17.525	0.3676	3121	4.338	178.1	0.86 0	.36		
56.244 56.244 56.244	29,119	3024	407.6(	1028)	1.2968	22.800 22.800	2913 2861	0.523	1498	2.524	n.18599	17.525	0.3679	3123	4.329	178.2	0.86 0	.36		
56. New 95. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No. 10. No	28.499 22.972		#07.4(	1174)	1,2665	23.185	3049	0.589	1759	2.553	P.18540	17.525	0.3691	3130	5.068	178.6	0.86.0	80 <b>≱</b>		
900	28.497	0.00	) 6° 90#	1178)	1.2659	23.198	3052	0.584	1748	2.554	n.18417	17.525	0.3715	3145	5.002	179.5	0.86.0	89 3*		
519 519 519	29.457		406.6(	1050)	1.2839	22.858	2934	0.523	1507 2	2.527	n.18620	17.525	0.3675	3154	4.360	180.0 (	0.86 0	<b>8</b> .		
799	29.689 25,100		405.36	1054)	1,2833	22.872	2938 2869	0.515	1489 2	2.527	0.18555	17.525	0.3688	3182	4.294	181.6	0.86 0	0.38		
7.025	29.505		351.1	1153)	1.2696	23.134 23.136	3030 2975	0.550	1637 2	2.546	0.18523	17.525	0.3694	3202	4.713	182.7	0,860	94.0		

o_																												
	IVAC PHI ETAC	9	60	0.62		9	20.0		66.0		,	66.0		96			00			66.0		6	7.0			90.1		66.0
	PHI	a d		98.0		40			98.0		3	98.0		.86			, 86 .			3.86		,	98.		90			98.6
	IVAC	5,799 185.6 0.46 0.40	•	5.208 187.7 0.86 0.62		4.750 186.0 0 86 0 83			9.183 184.6 0.86 0.99		,	3546 10.63/ 183.0 0.86 0.99		3.952 244.5 0.86 0.99	•		2.344 255.4 0.86 0.90	2		3.968 245.6 0.86 0.99		,	66.0 08.0 0.0c2 0cc.3			3.020 208.3 U.86 1.U		3,424 223,8 0,86 0,99
		7662	•	208 1		150 17	3		183 16		7	) (		152 24	•		44			168 24		90 01	200		70			24 25
	<b>(3)</b>								9.1		•	2																
	NEWON	3254		3289		3260			3235			34.00		4285			4473	•		4305		6000	***		1000			3923
	A/AC	0.3753		17775.0		0.3650			0.3553		1667			1.9372			3.4909			1.9373		7.51A6			0.496E	2		1.9371
	£	525		.525		.525	1		.525		700	000		.525			. 525	 		. 525		5.25	3		505			. 525
6.2		17	,	17		17	;		17			-		17			17			17		17	•		1,	•		17
= 21	W/A	.18232		.18116		.18747			.19255		10056	77.		.03532			09610.			.03532		01945			.02820			.03532
Ę		80 10		72.0		91 0			96		=	•		96			9.0					10	•		70			210
.750	S	2.5		2.5		2.5	•		2.5		•	j		2.5			2.5			2		2.6	•		9			2.0
- 210	VEI	2047		1650		2317			3069		142A			7200			7697			7229		77.37			8275			6237
P G	MACH	0.649		0.595		0.722			0.951		1.068			2.903			3.391			2.094		3.388			4.176			2,267
5.5	SONY	3216 3152	3168	3110	3279	3209		3330	3226		100 E		3330	2481		3330	2270		3340	2642	3340	2284	1	3380	1901	1	3287	2751
= 224.814 MACH 5.2 PT = 210.750 TT = 2186.2	GAMMA MOLWT SONY MACH VEI S	1,2269 23,841 3216 1,2361 23,859 3152 0,649 2047 2,583 n,18232 17,525 0,3753	23.640	1.2462 23.649 3110 0.595 1850 2.572 0.18116 17.525 0.3777	24.228	1.2117 24.274 3209 0.722 2317 2.591 0.18747 17.525 0.3650		24.630	1.1813 24.781 3226 0.951 3069 2.596 n.19255 17.525 0.3553	\$07.46	1.1831 24.796 3209 1.068 3428 2 601 A.18954 13 525 A 3554	) : : :	24.630	1.2820 24.992 2481 2.903 7200 2.596 0.03532 17.525 1.9372		1,1671 24,630 3330	24.993		24.605	1.400/ 24.792 2498 2.894 7229 2.601 0.03532 17.525 1.9373	1.1653 24.605 3340	24.993	•	1,1791 24,763 3380	25.041		24.504	1,2580 24,987 2751 2,267 6237 2,651 0,03532 17,525 1,9371
24.81	AVMA	226 <b>9</b> 2361	2410	2485	2002	2117		1671	1813	1651	1831	:	1671	2820	-	1671	2986	i	1653	1007	1653	2974		1791	3241		1612	2580
11	9			=	-	-		-i	<u>-</u>	-	: -	•		<u>.</u>		<u>-</u>	<b>:</b>		<b>.</b>	:	-	<u>.</u>		-	-			<del>.</del>
TINE		1404	1330	1268	1525	1438		\$ 100 m	1524	444	504	,	1645	763		384.6(1645	<b>6</b> 16		9		9991	625		1700	447		354.4(1613	786
	ď	401.9(140)	2 4 398.0(133	329.7(1268	390.2(152)	282,9(143	N)	384.6(1654	.96.4(1524	406.011666	171.2(1504	3	29.	÷.	t	<b>.</b>	ř	3	406.0(166	ว์ ส	406.0(166	77.	0	384.6(170	č	0	3	~
= 128	I	401.9(1404	388	329	3 39 90	282	すり	384	96 T	404	171	95	384.6(1645	-651	37	384	-799.3( 61	9	900	10 00 00 00 00 00 00 00 00 00 00 00 00 0	406	-790.2( 62	3	384	-983.9(	29	354	6.224-
BLOCK =	<b>⊢</b> ₩	4042	. 4486 3844	3686	4365			4708	0604		4341			-			'n		4737		~	2021	89	s	1494	69	4604	
	=													.732									STR		<b>*</b>		13.427	
600	<b>Q</b>	28.698 22.250	29.	23,587	29.073			28.729	AFGEN	28.729	15,106	Į.,	28,729	0	֝֟ ֖֖֡	28.729		REGEN	62/ 97		28,729	0.314	COMBUSTR	100.886	0	NOZZLE		<b>:</b>
اا	TOR		A TOR	2	5	_	ZO Z		100		_	¥	-		2	· ~		¥.	•	Po			Ç				٠.	•
READING = 0097	CCMBUSTOR	57.749	58.769	58.769	60.179	60.179	COMBUST	62.199	COMBIS	62.199	62.199	NOZZLE	87.27	87.275	NOZZLE	87.275	07.27	NOZZLE	A7 278	NOZZLE	87.278	87.275	FICTIVE	62.199	65.199	FICTIVE	87.275	2/20/0
	,	<b>=</b> 0																										

AGE 4	08/PT0	00	00	00	00	50E+0	45E+0	55E-0	715-0	115-0	100	75-0	37E-0	77E=0	30F-0	16E-0	17E-0	72E-0	0-361	37E-0	10 E	4.3E+0	31E-0	35F = 0	11.0	4 SE = 0	19F-0	745-0	35E+0	33E-0	35E-0	14E-0	36E-0	39E-0	300		75-0	37E-0	3E-0	3E-0	11E-0	3E-0	54E=0	37E-0	36E-0	315-0	2 C L 2 C C C C C C C C C C C C C C C C	20110	1010	100	100	56F-0	95	46-0	19E-0	
<b>a</b> .	PS0 P-	ċ	<u>-</u>	0	0.0	00 1.4	00 1.4	00 1.1	0			10	0.1	01 4.1	01 4.6	01 4.5	5.4	01 5.0	0.1	01 3.6	1.00	00	9-1	3.5		10	9.1	01 2.5	01 4.6	01 5.3	01 6.7	01 6.6	01 8.9	01 7.5	010		100	010	01 7.3	0.6 9.0	01 1.0	01 10	01 10	01 1.0	101	101	10							10	01 8.1	
	4	3.0.0	3 0.0	3	2 0.0	2 9.7	2 9.6	7.8	,		-	2	2.0	2	2	( )	87	2.5	2.5			6	2 1.0	2	-	2		5	2.1	10.00	- A	2.	2.0	יני מו			, ,		2	6.0	6.9	1.7.1	7.1	7.2	9°.		•		1			7.0		9.9	 	
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	P-18/PS	.277E 0	.277E 0	.044E O	.852E 0	.933E 0	.938E 0	.244E 0	OURF	.910E	OFOF O	.857E 0	.002E 0	.524E 0	0 1600	0 3469°	.773E 0	.116E 0	.095E 0	.081E 0	172E 0	.234E 0	.833E 0	BUBE D	172F 0	.269E 0	.481E 0	.296E 0	.246E 0	.381E 0	.665E 0	.669E 0	.123E 0	.561E 0	2.754E 01	91010	0456	.595E 0	.961E 0	.082E 0	.984E 0	.135E 0	.137E 0	.292E 0	.625E 0	7045 0	0 30E 0	9146	9045	9925	7765	<b>C</b>	511F 0	.806E 0	5.469E 01	
2.9	CAWALL	.470E-0	.634E 0	.053£ 0	.804E n	.847E 0	.850E 0	.218E 0	.521F 0	.738F 0	1746 0	734E 0	0555	.843E 0	.018F 0	0.0655	.071E 0	.095E 0	.129E 0	. 151E 0	.186F 0	.210E 0	.257E 0	.258F 0	362F 0	3706 0	.387E 0	.502E 0	.698E 0	.726E 0	.785E 0	.786E 0	.874E 0	.965E 0	2.093E 03	1956	277F 0	344E 0	.521E 0	.786E 0	.851E 0	.946E	.947E 0	.043E U	.100E	2002	2165 0	234F 0	2445	280F 0	1005	4025 0	532F 0	.790E 0	.972E 0	
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#154 422 E	<b>♥</b> 0	2.648E-01	2.377E 01	1.042E 02	2,151E 02	2.491E 02	2.492E 02	2.533E 02	9.593F 02	2.635E 02	2.700F 03	782F 02	2.836E 02	3.105E 02	3.227E 02	3.433E 02	3.455E 02	3.540E 02	3.636E 02	3.648E 02	3.814E 02	925E 02	4.147E 02	152E 02	4.701F 02	4.744E 02	339E 02	5.206E 02	5.364E 02	386E 02	395E 02	5.396E 02	220E 02	4.538E 02	-4.349E 02	3.959F 02	523E 02	3.37RE 02	501E 02	916E 01	822E 00	384E 01	998E 01	3/6E 02	783E 02	74.75	1135 02	173F 02	073F 02	398E 02	639F 02	272E 02	303E 02	355E 02	355E 02	
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P-CB/PT0	6.598E-02	6.361E-02	6.336E-02	6.210E-02	2.325E-02	6.014E-03	1.014E-02	1.400E-02	1.113E-02	6.667E-03	6.589E-03	6.311E-03	6.129E-03	5.219E-03	5.215E+03	0000	00000	0.000	000.0	0000	0000
P-OP/PS0	4.42RE 01	4.269E 01	4.252E 01	4.167E 01	1.560E 01	4.036E 00	6.804E 00	9.393E 00	7.470E 00	4.474E 00	4.421E 00	4.235E 00	4.113E 00	3.503E 00	3.499E 00	000.0	000.0	00000	0.00	00000	000.0
P-18/PT0	6.598E-02	5.789E-02	5.789E-02	5.461E-02	2.740E-02	2.079E-02	1.3195-02	1.144E-02	9.964E-03	6.845E-03	5.4336-03	4.309E-03	4.199E-03	5.6116-03	5.618E-03	8.114E-03	6.406E-03	5.575E-03	6.501E-03	9.751E-03	9.758E-03
P-IB/PS0	4.428E 01	3.885E 01	3.885E 01	3.665E 01	1.839E 01	1.395E 01	8.852E 00	7.680E 00	6.687E 00	4.593E 00	3.646E 00	2.892E 00	2.818E 00	3.765E 00	3.770E 00	5.445E 00	4.299E 00	3.741E 00	4.362E 00	6.543E 00	6.548E 00
CAWALL	4.289E 03	4.337£ 03	4.342E 03	4.368E 03	4.583E 03	_	4.760E 03	4.848£ 03	_		5.088£ 03		<b>306</b> 2	5.374E 03	-		5.525E 03		5.684E 03		5.707E 03
10-0	-8.348E 02 -	-0.466E 02	-8.479£ 02	-8.538E 02	-9.021E 02	-9.230E 02	-9.513E 02	-9.839E U2	-1.0ngE 03	-1.029E 03	-1.033E 03	_	-1.059E 03	-1.077E 03	-1.07AE 03	-1,116E 03	-8.871E 02	-8.871E 02	-8.871E 02	-8.871E 02	-8.471E 02
0-1B	-9.366E 02	-9.519E U2	-9.535E 02	_	18E	-1.036E 03	-1.053E 03		_	-1.096E 03	-1.103E 03	-1,125E 63	-1.127E 03	-1.136E 03	-1,136E 03		-1,171E 03	-	-1,209E 03	-1.241E (13	-1.241E 03
¥00	-1.771E 03	-1,799E 03	-1.801E 03	-1.815E 03	•	7		-2.052E 03	-2.088E 03	-		-			ı			-2.079E 03	-2.096E 03		-2,128E 03
FOA	8.855E 02		8.855E 02	8,855E 02	9.841E 02	1.067E 03	1.144E 03	1.212E 03	1.265E 03	1.324E 05	1.343E 03	1.399E 03	1.404E 03	1.442E 03	1.444E 03	1.475E 03	1.536E 03	1.590E 03	1.618E 03	1.660E 03	1.660E 03
P-08	1,390E 01	1,341E 01	1,335E 01	1,309E 01	4.9UOE 00	1.267E 00	2,137E 00	2.950E 00	2,346E 00	1.405E 00	1.389E 00	1.330E .00	1.292E 00	1,100E 00	1,099E 00	00000	000.0	0.0.0	000.0	0.000	ċ
P-16	1.390E 01	1.220E 01	1.220E 01	1.151E 01	5.775E 00	4.381E 00	2.780E 00	2.412E 00	2.100E 00	1.443E 00	1.145E 00	9.082E-01	8.850E-01	1.182E 00	1.184E 00	1.710€ 00	1.350E 00	1.175E 00	1.370E 00	2.055E 00	2.056E 00
XABS	6.466F 01	6.504E 01	6.508F 01	6.528E 01	6.694F 01	6.761E 01	6.838E 01	6.910E 01	6.971E 01	7,066E 01	7,109E 01	7.262E 01	7.277E 01	7,352E 01	7,352E 01	7.485E 01	7.770E 01	8.160E 01	8.441E 01	8.727E 01	8.727E 01

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CDRAG CF hC 2.459E 02 3.177E-03 0.738E-03

DDRAG

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READING = 0097 BLOCK = 128 TIME = 224,814 MACH 5,2 PT = 210,750 TT = 2166,2

# RAMJET FERFORMANCE

	(DEGREES)	(RTU/LBM)							
	0.8643 0.0011 0.0111 0.0111 0.01283 0.0128	0.9243 0.8890 -23.54 -7.07		0.0253 0.862 0.987 0.9091 0.6899		0.9154 0.8420 0.8602 0.8002		N.	
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	ANGLE OF ATTACK ADDITIVE DRAG COEFFICIENT LIMITING PRESSURE RECOVERY EFFICIENCY UELTA PTZ TOTAL PRESSURE RECOVERY - SUPERSONIC INLET PROCESS EFFICIENCY - SUBSONIC. INLET PROCESS EFFICIENCY - SUBSONIC.	25.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00		FUEL-AIR RATIO		VACUUM STREAM THRUST COEFF NOZZLE COEFFICIENT - CT PROCESS EFFICIENCY KINETIC ENERGY EFFICIENCY.	FUEL INJECTORS	STATION 40.400 41.284 44.300 48.759 46.250	54.049 56.234 44.784
	ANGLE OF ATTAC MASS FLOW RATI ADDITIVE DRAG LIMITING PRESSU JOHN PRESSURE TOTAL PRESSURE INLET PROCESS	KINETIC ENE KINETIC ENE ENTHALPY AT ENTHALPY AT		FUEL-AIR RATIO EQUIVALENCE RATIO COMBUSTOR EFFE RATI COMBUSTOR EFFECTIVE INJECTOR DISCHARGE		VACUUM STREAM THRU NOZZLE COEFICIENT PROCESS EFFICIENCY KINETIC ENERGY EFF		INJECTORS 1A 1B 1C 2A 2C	Ab a
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ENGINE PERFORMANCE		STREAN THRUST	MOMENTUM AND FORCES	-	NOZZLE PRESSURE INTEGRAL	•	STATIONS	::::::	
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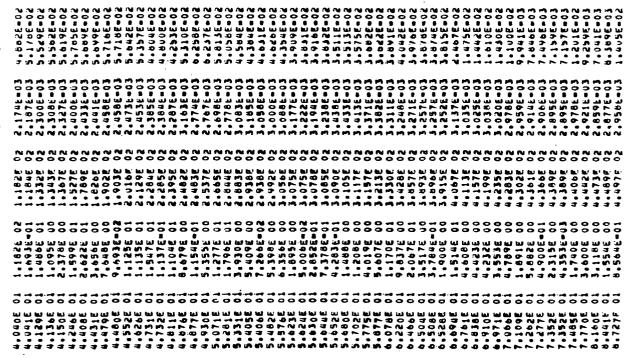
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READING .	Œ	9816-0	0 74.6	0 8000				20100	7000		6486	7016	7316 0	.803E 0	.833E 0	875E 0	0 2000	3106			0000	.046E 0	0416 0	189E 0	1366 0	1001	0 Maca.		4707 0	0 3084	5926 0	0 265 0		0116	.876E 0	0 1 2 6		20160	. 331E 0	0 3507°		0 17 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	6216	0 3450	.630E 0	. 644E 0	.6526 0	0 2000	7786	4746	0795	

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	F-18/PIO	8.076F-02	263k=0	5.630Em02	5.6305.642	5.307E-02	2.629E=02	2.003E-02	1.2036-02	1.121E-02	9.8326-03	7.075t-03	5.847E=03	4.4301-03	4.293E-03	5.9485-03	5.957E-03	8.8656-03	6.2115-03	4466-03	5.8396-03	1.139t-02	1.1406-02
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PEADING 8 0097 BLOCK 8 180 TIME 8 271.614 MACH 5.2 PT 8 4/6.994 TF 8 2225.0

4.426E 02 2.877£+03 1.556E+02

EADING # 0097 BLOCK # 180 TIME # 271,614	MACH 5.2 PT # 416.999	99 TT # 2223.6	
	RANGEL PERSONEANCE	FORFANCE	
ENGINE PERFORMANCE		INLET	
ALCULATED THAUST	2340, (LBF) 4606, (LBF) 3102, (LBF=SEC/LBM) 3442, (LBF=SEC/LBM) 0,7961	ANGLE OF ATTACK	0.000 0.000 0.00111 0.0000 0.1409 0.1409 0.1409 0.1409
REGENERATIVE COLCOLEO ENGINE PERFORMANCE CALCOLATEO THRUST	T707. (LBF) 2419. (LBF) 3190. (LBF-8EC/LBM)	INCEL PROCESS EFFICIENCY = SCOOPS STREET PROCESS EFFICIENCY = SCOOPS STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STREET STR	1113 120 120 120 120 120 130 130 130 130 130 130 130 130 130 13
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2/27/75-

READING = 0097 BLOCK = 207 TIME = 295.914 MACH 5.2 PT = 417.249 TT = 2221.4
RAMJET PERFORMANCE

ETAC																		
PHI																		
IVAC	156.6	163.0	156.4	156.4	62	131.2	131.2	129.5	125.7	13	124.7	122.0	120.2	119,9	19.4	119.4	118.9	119.3
œ	996	.903	.508	123	032	742	.207	.120	.416	. 673	458	. 979	8 2 2	.114	335 1	.306 1	948	49,453 1
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KOMTK	4987	5191	5236	5236	4336	4391	4391	4335	4206	4196	4174	4083	4623	4014	3995	3995	3980	3992
A/AC	8645	8645	8645	8645	111	1229	.1229	.1118	1114	1115	1113	1124	1164	1165	1176	1171	1193	0.1243
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3	31.838	31.838	33.470	33.470		33.470	33.470	33.470	33.470	33.470	33.470	33.470	33.470	33.470	33.470	33.470	33.470	33.470
⋖	4379	379	5117	5117	211	285	285	898	278	218	377	16222	2312	134	585	639	09537	163
3	0.1	0.14	7.	0.15	1.11211	1.06285	1.06285	1.16898	1.17278	1.1721	1.17377	1.16	1.12	1.121	1.11685	1.1163	1.09	1.05163
s	1,780	1.984	1.780	1.984	•	1.821	1.857	1.821	1.833	1.834	1.835	1.842	1.845	1.845	1.846	1.846	1.847	1.648
VEL	4908	852.	4899	906		3677	1163	3585	3370	3353	3314	3155	3062	3048	3015	3015	2993	3026
MACH	.170	0.383	5.107	1.407	.175	.223	.536	.122	.918	.903	.869	.740	.677	199•	179.	119.	630	1.660
SONV	2248 949 5	2223 (	9248	2248	2217 1671 2	2217 1654 2	2217 2170 0	2217 1689 2	2213 1757 1	2212 1762 1	2211 1773 1	2206 1814 1	2196 1827 1	2194 1829 1	2192 1634 1	2192 1834 1	2188 1836 1	2185 1823 1
KOLWI	28.837	28.836	28.837	28.836	28.837	28.837	26.836	28.837	28.836	28.836 28.836	28.836	28.837	28.836	28.836	28.836	28.836	28.836	28.836 28.836
	28	28			82 82 82 83				28	28	82			28	28	28. 28.		28 28
GAMMA	1.3983	1.3189	1.3189	1,3189	1.3211	1.3211	1,3211	1,3211	1.3214	1,3214	1.3215	1,3219	1,3226	1.3227	1.3229	1.3229	1,3232	1.3234
	90)	571) 557)	92)	571)	66	853) 283)	\$53) 526)	553)	324)	550)	331)	547)	3541	540)	5591	\$36) 357)	358)	535)
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_	249	612	.249 .631	612	409	300	<b>⇒</b> →	.317	45 88 88 89 80 80 80 80 80 80 80 80 80 80 80 80 80	.151 .822	638 478	.596 .813	.539	291	.453 640	36.0 6.35.0 6.05.0	.357	.942
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ETAC							00.1	90.1	0.56	0.56	1970	9.4	0.47	4	<b>.</b>			0.53	•
<b>1</b>							0.02	05	38	0.38	38	. 88		0.74	7	7	.74	0.74	
IVAC	120.6	120.7	22.2	23.6	24.6	128.7	-	8.04	-	42.2					, 4		æ		l i
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A/AC	.1335	1336	0.1433	.1554	.1662	1.1950	.2379	.2480	.2629	.2631	.2782	.296	.3676	.3679		.371	.3675	.3688	
3	0 064.	.470 0	.470	.470 0	.470 0	.470 0	.582 0	.582.0	0 986.	.934 0	.934 0	.934 0	.285 0	285 0	. n	ري د	285 0	.285 0	
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E / A	n.978e	1876.0	0.91208	0.84088	n.7864	0.6702	0.5511	0.5286	0.50394	0.5035	0.47618	0.44658	0.3641	0.36387		•	0.36420	ñ.36300	
'n	.847	.847	. 846	. 846	9#8.	.838	984	. 68	.192	.192	.201	.211	.426	.426	443	442	.430	.433	
VE 1.	3128 1	3129 1	3233 1	3324 1	3388 1	3632 1	2399 1	2143 1	2011 2	2010 2	1946 2	1880 2	1764 2	1763 2	1943 2	م.	1795 2	1804 2	
MACH	.749	.750	.845	.933	666	.279	•210	.058	.778	.778	.738	.697	.607	.607	•654	.650	.611	.611	
NOS	2181 1789 1	2161 1788 1	2178 1752 1	2175 1720 1	2173 1695 1	2167 1594 2	2197 1983 1	2195 2026 1	2687 2584 0	2688 2584 0	2730 2638 U	2779 2697 0	2972 2906 0	2972 2906 0	3043 2969 0	2976 0	3001 2935 0	3018 2952 0	104
VOL1.1	28.836 28.836	28.836	28.836 28.836	28.836	28.836 28.836	28.836	28.760	28.760 28.760	26.206	26.208	26.351	26.529	23.870	23.872	24.107	24.128	3.965	24.025	101
GAWN.A	.3237	3237 2	3239 2	3241.2	3242 2	.3247	3219 2	.3221	.2956 2	.2956 2	2815	2741 2	2725	2725	.2606 2	2595 2	2679 2	2650 2710	256
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م ت	21.066- 22.934	21.071 22.905	21,664 19,796	20.686 17.051	9.40	31,337	0 84.048 35.000	77.855 39.233	8.43	8.42	1.05	0 56,685 41,931	3.31	3,31 2,38	0 52.556 10.366	2.47	3.78	4.07	0 53.95a
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	ETAC	6.72	0.71	0.85	0.93	1.00	66.0	0.93	0.93	0.93	0.93	1.00	0.93
	PHI	0.74	0.74	0.74	0.74	0.74	0.74	0.74 0.93	9.74	97.0		9.14	9.74
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	ø	6099 11.803 177.9 0.74 0.72	6164 11.197 179.8 0.74	6114 13,782 178,3 0,74	6071 16.859 177.1 0.74 0.93	6269 17.947 182.8 0.74 1.00	6695 18.399 177.8 0.74 0.93	7.364 231.9	4.746 240.1 8.74 0.93	7.419 233.8	4.729 242.4 6.74	7.480 257.0 0.74 1.00	6.604 215.8 0.74 0.93
÷	MINON	6609	6164	6114	6071	6929	6695	7950	8234	8616	8311	8811	7398
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3	5	34,285	34.285	34.285	34.285	34.285	34.285	34.285	34.285	34.285	34.285	34.285	34.285
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PT = 417.249	VEL	2129	2033	2418	2880	306n	3143	6858	7245	6069	7312	7934	6150
	MACH	0.690	0.659	0.771	0.916	0.970	1.000	2.960	3.383	2.947	3.380	4.213	2.456
5.2	SONV	3160	3151	3223	3256		3274 3141	3256 2317	3256 2142		3274	3316 1883	3210
914 MACH	MOLWT SONV	24.592 24.606	24.560 3151 24.572 3082	24.950 3223 24.985 3137	25.172 3256 25.240,3142	25.346 3282 25.445 3162	25.152 25.237	25.172	25.172	25.152 3274 25.309 2344	25.152 3274 25.309 2163	25.410	25.179
295.	GANMA	1,2346	1.2369	1.2143	1.2006	1.1893	1.1967	1.2006	1,2006	1.1967	1.1967	1.2025	1.2008
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# READING = 0097 BLOCK = 207 TIME = 295,914 MACH 5,2 PT = 417,249 TT = 2221,4

# RAMJET PERFORMANCE

INET	OF ATTACK  LOW RATIO	PRESSURE RECOVERY PROCESS EFFICIENCY PROCESS EFFICIENCY IC ENERGY EFFICIENC ENERGY EFFICIENCY AT PO = SUBSONI	COMBUSTOR	FUEL-AIR RATIO	FUEL INJECTORS	INJECTORS STATION VALVE	
FORMANCE	2547. (LBF) 2547. (LBF) 2929. (LBF-SEC/LBM) 3539. (LBF-SEC/LBM) 0.7153	F F F F F F F F F F F F F F F F F F F		117.3 (LBF) -953.9 (LBF) 218.8 (LBF) 140.12 (LBF) 1734. (LBF) 1734. (LBF) 1734. (LBF) 1734. (LBF) 1734. (LBF) 1734. (LBF) 1736. (LBF) 1736. (LBF) 1736. (LBF) 1736. (LBF) 1736. (LBF) 1736. (LBF) 1736. (LBF) 1736. (LBF) 1736. (LBF) 1736. (LBF) 1736. (LBF) 1736. (LBF) 1736. (LBF) 1736. (LBF) 1736. (LBF) 1736. (LBF) 1736. (LBF) 1736. (LBF) 1736. (LBF)	SNS		0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0
ENGINE PERFORMANCE	CALCULATED THRUST	REGENERATIVE-COOLED ENGINE  STREAM THRUST	CAR MITTARACE	INLET FRICTION DRAG.  INLET MOMENTUM CHANGE.  COMBUSTOR FRICTION DRAG.  COMBUSTOR STRUT DRAG.  COMBUSTOR MOMENTUM CHANGE.  NOZZLE STRUT DRAG.  NOZZLE STRUT DRAG.  NOZZLE PRESSURE INTEGRAL.  EXTERNAL PRESSURE INTEGRAL.  TOTAL EXTERNAL DRAG.  CAVITY FORCE.  CALCULATED LOAD CELL FORCE.  FUEL VACUUM SPECIFIC IMPULSE -152.8.	STATIONS	NOMINAL COWL LEADING EDGESPIKE TRANSLATION	COWL LEADING EDGE

Reading 97

t = 317.51 sec.

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READING # 0097 BLUCK # 231 TIME # 317,514 CACA 5.2. PL # LIB.499 TI # 2214,5

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٧/.	5.00 P	0.4620	0.9157	200000		0.7895	0.6729	0.5533	4	>	0.5071	7005.0		0.4791	4	3 3 3 •	9.3672		. 366.	9,44,0		0.3652	1,43	•	0.5661	
ĸ	1.001	1.641	1.8.1	1.64		1.642	1.827	1.885			2.227	2,227		2,239		× × × ×	2.504		2,503	165.0	•	5.55	4	•	2.516	
ب خ م	3100	31,16	3226	3.542		3436	3746	2129	4	D	1 / 88	1788		1776	7	00/	1669		1669	1845	•	1843	1721		1754	
H. J. M. H.	<b>ددر.</b> ۱	1.736	1.840	1.952		2.044	2.461	1.046	•	•	0.685	685		0.665	7		0.565		. 567	3		909.0	. 44.0		0.500	
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4.11.4.7	, 525H	3258 3564	.3240	3242	1.3243	.3247		1,3219	1.5221	. 2927	1.2989	1.2926		1.2913	1.2760	) <b>.</b>	.2828	1.2779	1747.	.2651	2639	6642.	.2716		.2725	2574
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	504	U 4 4 (		, , ,	<i>J</i>		y, U	ימיניטי	תני העניט	<sub>.</sub> .	J- L	r ur ur	<i></i>		יש עם	، ی	er en (	ו הו ט		יט יט <u>.</u>	U an	er C	ר <i>שירטי</i>	<i></i>		, (

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	٥	-	I	CAVA	ANDS INTUM BARKS	7400	HACH VEL	VE.	so	4/4	•	A / A C	7	3	IVAC	IVAC PHI	£ TAC	
2	2	28	31 5															
1.147	56.345	7	(464()40474)	1.8248	73.012	\$259				*E348 73.612 3259								
	2		357.9(1354)	1.2388	23.024	3188	404.0	7134	- 155*2	0.55970	30.50	6.3753	4467	6427 11.431 185.4 C.90 0.60	1.5.1	ر د .	0.66	
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8.767	57.106		444.7(1414)	_	23,58	3244				2339 23,558 3244								
8.767	44.662	38	362.9(1302)	-	23.571	3179	0.637	2024	4.546	0.35747	34,580	0.3777	9679	000 11,244 187.8 0.90 0.64	187.8	05.0	1900	
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0.777	56.693	77	436.7(157A)	-	24,044	3334												
0.177	38	42	315.8(1477)	_	24.092	3252	0.762	2480	2.541	2143 24.092 3252 0.762 2480 2.561 0.36991 34.560 6.3650	34.580	0.3650	0441	6441 14.256 186.3 0.90 0.8U	186.5	0.50	0.80	
2	2	7 7	75 75															
2.197		467	10165	1,1850	24,284	3366				1850 24,284 3366								
2.197	35.025	43	253,3(1518)	1.2006	24.383	3259	0.915	2983	2.565	0.37993	34.580	0.3553	6393	6393 17.610 184.9 0.90 0.89	184.9	06.0	9.00	
I		3	, ~															
2.197	59.720	4	Ξ	1.1662	24.523	3399				1662 24,523 3399								
2,197	35.025	454	227.8(1597)	1.1784	24.690	3285	0.971	3189	2.561	0.57993	34.580	0.3553	6616	6616 18.631 191.3 0.90 1.00	191.3	06.0	00.1	
ē	R REGEN		•	•														
2.197	56.790		413.9(164	1.1868	34.298	3358		•										
2.197	55.792			1,2020	24.389	3285	0.895	2908	2.561	.2020 24.389 3255 0.895 2908 2.561 0.37993 34.580 0.3593	34.580	0.3553	6363	6383 17,169 184.6 0,90 0,89	104.6	06.0	.89	
97220	A F.		37 4															
7.273	56.790	4671		1.1850	24.284	3366				1880 24.284 3366								
	~		*598.2( 7	1.2904	24.500	2040	2.936	7117	2.565	59690.0	34.530	1.9372	4000	6407 7.773 243.1 0.40 0.89	243.1	04.0	69.0	
	0		79 95		-		• •			•								
7.273	56,790		431,10	1,1850	24,284	3366									-			
7.273	0.632		•	1.3062	3062 24.507	2245	3,399	7630	2,565	2245 3,399 7630 2,565 0,04023 34,580 3,3559	34.580	3.3559	8744	8744 4.771 252.9 0.90 0.89	252.9	- 06.0	69.0	
0226	AE REGEN		39 4										;					
7.273	56.790	4643	5	1.1868	24.298	3358												
7.273	1.585	2254	-608.2( 716)	1,2915	2915 24,506	2430	2.943	7152	2.561	2,943 7152 2,561 0,06969 34,580 1,9372	34.580	1.9372	6374	7.746 242.2 0.90 0.89	242.2	06.0	60.0	
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7.273	\$6.790		1000	1,1868	24,298	3356												
7.273	0.632	1002	ë.	1.3071	3071 24.507 2234	2234	3.401	7597	2.561	3.401 7597 2.561 0.04049 34.580 3.3347	34.580	3.3347	8705	4.780	4,780 251,7 0,90 0,89	06.0	984	
ICTIVE	COMBUSTR		0 79															
2.197	2.48		111	1.1792	24.636	3445				1792 24.636 3445								
2.197	0.632	1566	*996.2( 473)	1.3142	24,438	2030	191.7	8451	2.463	0.05506	34.580	2,4519	0876	7.232 274.2 0.90 1.00	274.2	06.0	00.1	
ICTIVE	NOZZLE	2	•												•			
7.273	20.307	4585	403.8(1620)	1.1796	24.461	3329				1796 24.461 3329								
7.273	1.956		8	1.2708	24.508	2407	2.150	4117	2.414	0.04076	34.45	1.017	7783	4.844	336.0	00.0		

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.526E 0	2 7	_		2.501E	0	1.454E	0	-5,329E	2	-1.714E	63	1.616F C	~	4.568E U3	3.604E 0	_	5,4/3c=02	1.955E 01	6.005E=02
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1,761E 0	•	_		1.357E	0	2.005E		-3.614E	2	-1.849E		11.765E 0	~	4.665E 03	1.376E 0	_	2.090t-02	2.147£ 00	3.2596-03
. 838E 0	1. 5.1			3.92E	00	2,1524		-5.703E	6	-1.884E	50	1.819E 0	~	4.760E 03	8,997E 0		1.306E-U2	6.202E 00	9.4176-03
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.066E 0				3.725E	0	2.530L		3776°5=	3	*1.969E		-1.475E 0	~	5. U.36E 03	4.794F. 0		1.279E-03	5.890E 00	8.944E=US
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.262E 0	11			2000e	00	2.645E		-4.003E	50	-2.022c	9	2.040E 0	~	5.2736 03	3.011E 0	•	4.571t-03	3.858E 00	5.8586.03
1.277E 0		1.845E 0	00	2.230F	60	2.704E	0.5	-4.071E	20	3420.5-	50	-2.046E 0	03	5.290E 63	2.917E 0	٠ ء	4.430E=03	3.526E 00	5.354E=03
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## REPRODUCIBILITY OF THE ORIGINAL PAGE IS POOR

B 251 flet a 317,514 hath 5.2 Pl B alboagy II B 2210.5	RAMBET PERFURNANCE	NGTIVE DEFICE	### ### ##############################	THE PROCESS EFFICIENCY = GURENDILESS    INLEI PROCESS EFFICIENCY = GURENBUNICS    INLEI PROCESS EFFICIENCY = GURENBUNICS    ATARIC ENERGY EFFICIENCY = GURENBUNICS    ATARIC ENERGY EFFICIENCY = GURENBUNICS    ATARIC ENERGY EFFICIENCY = GURENBUNICS    ATARIC ENERGY EFFICIENCY = GURENBUNICS    ENTHALPY AT PO = GURENBUNI	COrbusta A.D Mineral	### ##################################	STATIONS FUEL INJECTORS	1	(21) /5(2) (21) /5(2) (21) /5(3) (21) /5(3) (21) /5(3) (21) /5(3
11HE = 317		ENGINE PEPFORMANCE		2 · · · ·	STATE OF STA		STATIONS		: : : :

Reading 97

t = 322.01 sec.

Test cell pressure was high which resulted in increased pressures in the AIM nozzle.

0. THE RESERVE OF THE						20 20	2 1.	> 0	ш Э	er E								
N ACE	-	r		GAMO	1 4 7 0 8	N YUS	MACH	٠ د د د	s	4 / 4	.<	•	747	3013	3	IVAC	0 0	ETAC
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85.0 0	7 372	139.80		1.5142	28.436	6243	5.17	1687 0	1.779	0.144	21 31.	923 0.	8643	4003	16.974	156.3		
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<b></b>	¥ ~	425.00	550	1.3210	20.030	6219	0.38	9 H 49	1,983	0.144	21 31.	923 n.	8643	5196	1.904	164.6		
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atch		•	2	1 . 36 4					000	000	• 6 6		1667		14.640	777		
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## Reading 97

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